APPENDIX C
Monterey Peninsula Water Supply Project Hydrogeologic Investigation Technical Memorandum (TM-1) –
Summary of Results – Exploratory Boreholes

Monterey Peninsula Water Supply Project Hydrogeologic Investigation

Technical Memorandum (TM1)
Summary of Results - Exploratory Boreholes

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CALIFORNIA AMERICAN WATER / RBF CONSULTING MONTEREY PENINSULA WATER SUPPLY PROJECT HYDROGEOLOGIC INVESTIGATION TECHNICAL MEMORANDUM (TM 1) SUMMARY OF RESULTS - EXPLORATORY BOREHOLES

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CALIFORNIA AMERICAN WATER / RBF CONSULTING MONTEREY PENINSULA WATER SUPPLY PROJECT HYDROGEOLOGIC INVESTIGATION TECHNICAL MEMORANDUM (TM 1) SUMMARY OF RESULTS - EXPLORATORY BOREHOLES

1.0 EXECUTIVE SUMMARY

1.1 Introduction

The investigation and findings described in this Technical Memorandum are the result of collaborative planning and discussions among the hydrogeologic experts that represent key stakeholders for groundwater use and management in the Salinas Valley and Monterey Peninsula area of central California. The Hydrogeology Working Group (HWG) consisted of the following experts: Mr. Tim Durbin and Mr. Martin Feeney (both representing the Salinas Valley Water Coalition and the Monterey County Farm Bureau), Mr. Peter Leffler (representing CalAm), and Dr. Dennis Williams (representing the CPUC CEQA Team). The HWG was formed as a result of a 2013 Settlement Agreement among parties to an ongoing CPUC-proceeding resulting from CalAm's proposed Monterey Peninsula Water Supply Project, to review and approve the scope of field investigation and development of a hydrogeologic conceptual model from which to construct the groundwater modeling tools. The names of the HWG members are presented here to indicate the general agreement among the members on the core findings of the investigative work described herein.

The work completed for this investigation was described in the Hydrogeologic Investigation Workplan (Workplan), Attachment 1, dated 18-Dec-2013. This investigation represents the first phase of field data gathering to develop a hydrogeologic conceptual model for the project area that is accepted by the stakeholders. The conceptual model will be used to refine the existing North Marina Ground Water Model (NMGWM) and construct a new focused model (CEMEX model). These models will be used to evaluate proposed project operations and impacts. Additional phases of field testing are planned and outlined in the Workplan.

Since September 2013, six exploratory boreholes were drilled at the CEMEX facility. Total borehole depth ranged from 250 feet (ft) below ground surface (bgs) to 350 ft bgs. Three of the boreholes were used to collect continuous soil cores, undisturbed soils samples, samples for mechanical grading



analysis, and geophysical logs. Two borings were used to construct isolated zones¹ for collecting water quality samples from aquifers at discrete depths and the last borehole (CX-B4) was used to collect continuous soil cores, undisturbed soils samples, samples for mechanical grading analysis, geophysical logs, and to collect water quality samples. A total of fifteen (15) aquifer zone tests have been completed at the CEMEX site. Water quality samples collected from the isolated aquifer zones were analyzed for the same suite of analytes outlined in the Workplan and included general physical, general mineral, volatile organic compounds, pesticides, tritium, and stable isotopes of oxygen and hydrogen.

Since September 2013, seven exploratory boreholes were drilled in the Moss Landing area. Six borings were drilled to a depth of 200 ft bgs. One boring (MDW-1) was drilled to a depth of 300 ft bgs. Each borehole was used to collect continuous soil cores, undisturbed soil samples, samples for mechanical grading analysis, and geophysical logs. Two isolated aquifer zones were constructed in boreholes ML-1, ML-2, ML-3, ML-4, ML-6, and PR-1 (for a total of 12 zones) to collect depth-specific groundwater quality samples. Four isolated aquifer zones were constructed to collect groundwater samples from Boring MDW-1.

1.2 Findings

1.2.1 General

- The conceptual hydrogeologic model developed from this investigation suggests that a feedwater supply system using slant wells at the CEMEX site is feasible and can utilize the Dune Sand Aquifer and underlying terrace deposits (180-Foot Equivalent Aquifer) as conduits to extract water through the seafloor beneath Monterey Bay.
- This opinion will be tested using the newly constructed CEMEX Model and the refined NMGWM
 and will be field tested using a test slant well and groundwater monitoring system as described
 in the Hydrogeologic Investigation Workplan.
- The conceptual model also indicates that the Perched "A" Aquifer between the Molera and Sandholt Road Salinas River State Beach parking lots could provide an alternative target for construction of a subsurface feedwater supply system.

1.2.2 CEMEX Area

The CEMEX facility is located on the westernmost edge of the 180/400-Foot Aquifer Subbasin of the Salinas Valley Groundwater Basin, as currently mapped by DWR (2003) and the MCWRA (2011). The findings of the investigation at CEMEX are summarized below:

¹ An isolated zone is constructed by the installation of well screen at a selected depth interval and isolating the well screen above and below using bentonite seals. Construction of isolated zones allows depth specific sampling of groundwater.



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- A significant clay layer is not present beneath the Dune Sand Aquifer at the CEMEX site at elevations commonly attributed to the Salinas Valley Aquitard (SVA), suggesting a different depositional environment than that of the 180-Foot Aquifer in the Salinas Valley. The water quality data suggests groundwater in the Dune Sand Aquifer may be in hydraulic continuity with the underlying aquifer units. The degree of hydraulic continuity will be determined by construction of aquifer specific monitoring wells and the long-term pumping test of the test slant well.
- Stratigraphic relationships and lithologic observations indicate that the aquifer system underlying the Dune Sand Aquifer consists of terrace deposits that are older than the inland 180-Foot Aquifer deposits, since they underlie the Older Dune Sand.
- The terrace deposits appear to be a distinct lithologic unit in terms of geologic history and depositional environment in the Dune Highland area and may be hydrostratigraphically equivalent to the 180-Foot Aquifer in the Salinas Valley.
- For purposes of this document, the alluvial materials encountered near the coast (in the CEMEX area) are based solely on analyses of borehole samples (and geophysical borehole logs). As of yet, no direct correlation can be made between these coastal alluvial deposits and the standard naming convention found further inland (e.g., 180-Foot Aquifer, 400-Foot Aquifer, SVA, etc). Consequently, the naming convention agreed upon by the HWG, includes the word "equivalent" since the lithologic units that make up the aquifers at CEMEX and in the Salinas Valley are chronologically different, but stratigraphically equivalent.
- As a hydrogeologic unit, the terrace deposits will be designated as the 180-Foot Equivalent (180-FTE) Aquifer. The extent of hydrostratigraphic equivalence will be evaluated through a pumping test utilizing the test slant wells and a monitoring network.
- The current interpretation of the distinctive dark greenish-gray clay found at depths ranging from 241 to 282 ft bgs at CEMEX is that it may represent a change in the depositional history and is underlain by a unit equivalent to the Aromas Sand(?)/400-Foot Aquifer.
- Both the Dune Sand Aquifer and the underlying 180-FTE Aquifer extend seaward beneath the Monterey Bay.
- Groundwater in the Dune Sand Aquifer and most of the groundwater in the 180-FTE Aquifer exhibit high concentrations of total dissolved solids (TDS), ranging from 24,000 to 32,000 mg/L, indicating a seawater source.
- Hydraulic conductivity for the Dune Sand at CEMEX ranged from an average low value of 273 ft/day to an average high value of 779 ft/day.



- Hydraulic conductivity for the Older Dune Sand at CEMEX ranged from an average low value of 136 ft/day to an average high value of 372 ft/day.
- Hydraulic conductivity of the terrace deposits that make up the 180-FTE Aquifer ranged from an average low value of 113 ft/day to an average high value of 342 ft/day.
- Hydraulic conductivity values will be further refined based on the long-term test slant well pumping test.
- Analysis of cation/anion ratios indicates that groundwater in the lower portion of 180-FTE Aquifer and in the 400-Foot Aquifer have been geochemically altered due to seawater intrusion.
- Tritium results indicate that groundwater in the lower portion of the 180-FTE Aquifer is older than groundwater in the upper portion of the 180-FTE Aquifer and the Dune Sand Aquifer.
- Analysis of oxygen and hydrogen isotopes suggests that at both the CEMEX and Moss Landing sites, saltwater from the ocean is mixing with a freshwater source that has not undergone significant evaporation (as would be expected of a surface water source).
- Hydrostratigraphic relationships indicate that slant wells drilled into the Dune Sand Aquifer and 180-FTE Aquifer will receive recharge primarily from ocean sources through vertical leakage from the sea floor and horizontal recharge from offshore subsea aquifers. This will be tested by the CEMEX and refined NMGWMs as well as field pumping tests.

1.2.3 Moss Landing Area

The Moss Landing area is located north of the mouth of the Salinas River, which overlies the westernmost edge of the 180/400-Foot Aquifer Subbasin. Borings were drilled and sampled at Moss Landing Harbor and at the Molera, Potrero Road, and Sandholt Road parking lots of Salinas River State Beach. The exploratory borings primarily penetrated fluvial sediments associated with Holocene and Late Pleistocene Salinas River deposition.

The Perched² "A" Aquifer is ascribed to the Holocene river alluvium and considered to be the hydrostratigraphic equivalent of the Dune Sand Aquifer located to the south.

• The Perched "A" Aquifer in the Moss Landing area is composed of interbedded river and floodplain deposits.

² The term Perched "A" Aquifer refers to the shallow aquifer above the Salinas Valley Aquitard. Traditionally, the term "perched" aquifer refers to a hydrogeologic condition where an aquifer is formed by groundwater being present above (perching on) an impermeable unit such as clay but with an unsaturated portion of an aquifer between the bottom of the clay and the underlying saturated portion of a lower aquifer.



- With the exception of the sediments penetrated in Boring PR-1 and MDW-1, individual sand and sand and gravel lenses do not appear to be either vertically or areally extensive in Moss Landing.
- Significant variations in TDS concentrations suggest that groundwater is mixed with seawater, and is likely present in semi-isolated lenticular deposits.
- In general, the upper isolated aquifer test zones were above a depth of 110 ft bgs. TDS concentrations ranged from 3,200 mg/L to 34,000 mg/L.
- The lower isolated aquifer zones were generally constructed at depths exceeding 150 ft bgs.
 With the exception of Zone 1 of PR-1 (190-200 feet) at 630 mg/L, the TDS concentrations ranged from 7,400 mg/L to 34,000 mg/L.
- Boring PR-1 penetrated a very permeable unit in the Perched "A" Aquifer from 54 to 139 ft bgs.
 Groundwater in this interval approximated seawater quality (i.e., 34,000 mg/L). This unit is
 interpreted to continue, but decrease in thickness southward towards Boring MDW-1. To the
 north, the unit is interbedded with fine-grained units.
- It is interpreted that the lowest portion of Boring PR-1 penetrated the SVA. Very low TDS concentrations (630 mg/L) encountered in the lowest zone in Boring PR-1 suggest that isolated zones of freshwater may exist within the 180-Foot Aquifer or that the sand unit is laterally discontinuous and may be interbedded with the SVA. In this last interpretation, Boring PR-1 did not completely penetrate the SVA.
- Hydraulic conductivity values for the permeable portion of the Perched "A" Aquifer penetrated
 in PR-1 ranged from 194 ft/day to 717 ft/day, based upon relationships between grain size
 distribution and hydraulic conductivity.
- The permeable unit between Boring PR-1 and MDW-1 represents a potential location for slant wells.
- The Moss Landing Borings (ML-1, ML-2, ML-3, ML-4, and ML-6) did not penetrate significant thicknesses of permeable deposits to produce the required feedwater supply volume for the MPWSP.



1.2.4 Refinement of NMGWM and Development of Focused CEMEX Model

The geologic and hydrogeologic data collected during this investigation was used to prepare the interpretations of hydrostratigraphic relationships in the Moss Landing and CEMEX areas. A conceptual model of the hydrostratigraphic units from the Moss Landing to CEMEX area as interpreted from data collected from this investigation is shown below on Figure 1-1

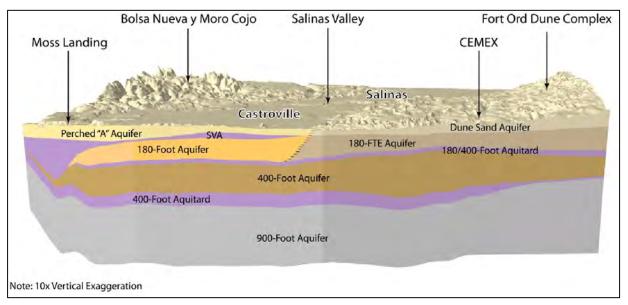


Figure 1-1. Hydrostratigraphic Model – Moss Landing to CEMEX Area

The following table provides a correlation of the geologic and hydrostratigraphic units to groundwater model layers of the Salinas Valley Integrated Groundwater and Surface Water Model (SVIGSM) and the NMGWM. In addition, the project technical advisory group described in Section 2.4 requested that a third model (a focused model) be constructed in the CEMEX area. The new focused model is designated as the CEMEX Model (CM) and will be discussed in Section 6. The model layers of the CM, as correlated to the SVIGSM and NMGWM, are also shown on Table 1-1.



Table 1-1.
Correlation of Geologic and Hydrostratigraphic with SVIGSM, NMGWM, and CM Model Layers

180/400-Foot Aquifer Subbasin			C	CEMEX Area					
Surface Geologic Units	Surface Geologic Units Map Symbol	Hydro- stratigraphic Units	Surface Geologic Units	Surface Geologic Units Map Symbol	Hydro- stratigraphic Units	SVIGSM Layer ¹	NMGWM Layer	CEMEX Model Layer	
Benthic Zone	-	Benthic Zone	-	-	Benthic Zone	Constant Head	1	1	
			Dune Sand	Qd				2	
Alluvium	Qal ²	Perched "A" Aquifer	Older Dune Sand	Qod	Dune Sand Aquifer	1a	2	3	
Older Alluvium	Qo	Salinas Valley Aquitard		1a	1a	3	5		
								6	
Older Alluvium/ Marine Terrace	Qo/Qmt	180-Foot Aquifer		Older Terrace/ Marine Terrace	Qt (Qmt?)	180-FTE Aquifer	1	4	7
Older Alluvium/ Older Alluvium Fan – Antioch	Qo/Qfa							8	
Older Alluvial Fan – Placentia	Qfp	180/400- Foot Aquitard			180/400- Foot Aquitard	2a	5	9	
Aromas Sand (undifferentiated)	Qar	400 5	Aromas Sand (undifferenciated) (?)	Qar (?)	400 5				
Aromas Sand – Eolian/Fluvial Lithofacies	Qae/Qaf	400-Foot Aquifer	,,,		400-Foot Aquifer	2	6	10	
Paso Robles	OT I Aquitaru	Foot	Paso Robles	QT	400/900- Foot Aquitard	3a	7	11	
Formation		900-Foot Aquifer	Formation		900-Foot Aquifer	3	8	12	

¹SVIGSM considers "a" layers to be aquitards (vertical hydraulic conductivity and thickness are input)



²Subsurface Holocene geologic unit not mapped at surface

2.0 INTRODUCTION

2.1 Background

The California American Water Company (CalAm) is proposing the Monterey Peninsula Water Supply Project (MPWSP, or proposed project) for the purpose of developing water supplies to replace those portions of CalAm's existing supplies that have been constrained by legal decisions regarding CalAm's diversions from the Carmel River and pumping from the Seaside Groundwater Basin. The MPWSP would include construction of a subsurface Seawater Intake System and a desalination plant with a rated capacity of 9.6 million gallons per day (MGD) or 6.4 MGD, which is approximately 10,800 acre-ft per year and 7,200 acre-ft per year, respectively.

On April 23, 2012, CalAm filed an application with the California Public Utilities Commission (CPUC) for the MPWSP (A.12-04-019), seeking a Certificate of Public Convenience and Necessity (CPCN) to construct, own, and operate a desalination facility for water supply on the Monterey Peninsula. The MPWSP application to the CPUC proposed a subsurface intake feedwater system consisting of slant wells located at the CEMEX sand mining property in Marina, CA.

In a letter dated September 26, 2012, the CPUC asked the State Water Resources Control Board (SWRCB) whether CalAm has the legal right to extract desalination feedwater for the proposed MPWSP. The CPUC requested an opinion on whether Cal-Am has a credible legal claim to extract feedwater for the proposed MPWSP in order to inform the CPUC's determination regarding the legal feasibility of the MPWSP. The SWRCB concluded in July 2013, that the conditions in the aquifer where MPWSP feedwater would be extracted could be either confined or unconfined. However, there was not enough information at that time to determine what types of conditions exist at the location of the proposed MPWSP wells. The SWRCB recommended that studies are needed to determine the extent of the Dune Sand Aquifer, the water quality and water quantity of the Dune Sand Aquifer, the extent and thickness of the Salinas Valley Aquitard, and the extent of the 180-Foot Aquifer, if present.

In August 2013, a Settlement Agreement was signed by several of the Parties associated with the CPUC proceeding. The parties agreed that CalAm and Salinas Valley Water Coalition's (SVWC) hydrogeologists would work with other experts to develop and implement a workplan for the proposed source water intake sites consistent with the study recommendations presented in SWRCB's July 2013 Review of the MPWSP.

2.2 Extracting Seawater from Subsea Aquifers for Feedwater Supply

The intake system proposed by CalAm is expected to supply a high percentage of ocean water from aquifer units that are in hydraulic continuity with the ocean floor. The feasibility of extracting seawater



from the aquifers that underlie the ocean floor using slant wells is directly dependent on the vertical and horizontal distribution of hydrostratigraphic units in the project areas and their hydraulic properties.

Previous studies have indicated that in the vicinity of the CEMEX facility, the shallow Dune Sand Aquifer may directly overlie the 180-Foot Aquifer, or may be separated from the 180-Foot Aquifer by low permeability material of the hydrostratigraphic unit designated as the Salinas Valley Aquitard (SVA). Therefore, a key aspect of the exploratory boring program at the CEMEX facility was to evaluate the presence and vertical distribution of hydrostratigraphic units. If the Dune Sand Aquifer directly overlies the 180-Foot Aquifer or an equivalent hydrostratigraphic unit (i.e., no intervening clay layer of significant thickness), and if both units are in hydraulic connection with the ocean floor, feedwater can be obtained directly from the subsea portion of both aquifers with little or no impact on the inland aquifers.

A groundwater model was developed by GEOSCIENCE in 2008 and is called the North Marina Ground Water Model (NMGWM). The NMGWM was developed based on existing data and conceptual models of the hydrogeology in the region, and has been used to evaluate several proposed projects in the area. The NMGWM is a three dimensional variable density finite difference model that uses industry standard computer codes (MODFLOW, MT3DMS and SEAWAT). Regional boundary conditions for the model are obtained from the Salinas Valley Integrated Groundwater and Surface Water Model (SVIGSM). Construction of a third model, a focused model centered at CEMEX, was requested by the Hydrogeology Working Group (HWG). The new model will have additional model layers and a finer grid size than the NMGWM. The new focused model is herein referred to as the CEMEX Model (CM). The CM will be constructed with the field data collected from this investigation. The NMGWM includes the area of the current investigation (i.e., CEMEX and Moss Landing) and will be refined (based on recent field data). Both the CM and the NMGWM will be used to support the CPUC's environmental review process, and to design a subsurface feedwater supply system.

2.3 Subsurface Intakes

Subsurface intakes are generally favored among regulatory agencies because of: (1) the natural water filtration and pretreatment provided by ocean floor sediments, which reduce the need for some treatment chemicals during the desalination process, and (2) the minimal growth of marine organisms that occurs inside the intake pipeline. The slant well subsurface intake system is also a primary consideration because the system will allow for a feedwater supply to be obtained from ocean sources (i.e., vertical leakage through the sea floor and horizontal recharge from offshore aquifers). In general, source water derived from subsurface wells requires significantly less filtration when compared to raw seawater. Subsurface wells are also generally considered a low-impact technology with respect to impingement and entrainment.



The subsurface intake site proposed by CalAm is located at the CEMEX property in Marina. Alternative intake sites have been proposed in the Moss Landing area. Therefore, this technical memorandum addresses the potential feasibility of subsurface intakes in both areas.

Figure 1 is a general location map for the current study. Figure 2 shows the locations of borings completed in both the CEMEX and the Moss Landing areas. Area maps specific to CEMEX facility and the Moss Landing area are shown in Figures 3 and 4, respectively.

2.4 Formation of Hydrogeology Working Group and Formation of the Hydrogeologic Investigation Workplan

As noted earlier, the Settlement Agreement laid the ground work for a collaborative effort by recognized experts in geology, hydrogeology and modeling, representing stakeholders of groundwater use and management in the project area. This led to the development of the Hydrogeology Working Group³ (HWG). The HWG first met on April 25, 2013, to discuss conceptual models and to form a collaborative plan of investigation to assess the hydrogeologic conditions in the project area. As with any collaborative group, individual opinions need to be evaluated against actual field data and testing to arrive at a conceptual model that reflects a common understanding at the areas of concern. A draft workplan was prepared which provides a phased approach to progressively investigate the hydrogeology and the potential effects to aquifers from the use of subsurface slant wells for obtaining feedwater supply. The draft workplan was submitted to the HWG on August 2, 2013, for review and comment. The final workplan incorporated comments and recommendations by members of the HWG, covered the investigative steps needed to evaluate the project impacts, and was submitted to the HWG on December 18, 2013. This final workplan became the hydrogeology investigation roadmap.

2.5 Project Documents

2.5.1 Hydrogeologic Investigation Workplan

The process adopted by the HWG for the workplan consists of on-going steps of data collection and analysis. The data collected from this initial phase of investigation will be used to construct the CM and to refine the NMGWM. Each subsequent step of data collection will be followed by refinement of the CM and NMGWM, which are the tools being developed to evaluate the short- and long-term hydrogeologic impacts in the project area from operation of the MPWSP. Each step of data gathering will be preceded by an update of the workplan as appropriate, describing the proposed work and

³ The HWG participants include: Tim Durbin and Martin Feeney (representing the Salinas Valley Water Coalition and the Monterey County Farm Bureau), Peter Leffler (representing CalAm), and Dennis Williams (representing the CPUC CEQA Team).



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desired outcomes. Results will be documented by a technical memorandum describing the methods of data collection, findings and recommendations, and the results of the model refinements.

The MPWSP Hydrogeologic Investigation Workplan (HWP) is the main working document for all exploratory, testing, and modeling work, including:

- Attachment 1 Technical Specifications Exploratory Boreholes
- Attachment 2 Technical Specifications Test Slant Well
- Attachment 3 Technical Specifications Monitoring Wells
- Attachment 4 Technical Specifications Long Term Pumping Test and Monitoring Program
- Attachment 5 Technical Specifications Full Scale Slant Well Field

As such, the HWP is a "living document" which will be modified as appropriate as the project progresses.

To date, technical specifications for the boreholes (Attachment 1) was submitted to the HWG for review and comment, forming the basis for the current investigation. Preliminary Technical Specifications (Attachment 1 of the Hydrogeologic Investigation Report) for the test slant well and two monitoring wells were prepared and submitted to Cal Am for planning purposes. Subsequently, it was decided by CalAm to prepare separate technical specifications for the test slant well and for the monitoring wells. These documents were recently submitted for review. Therefore, after review of the findings of the current document by the HWG, the Technical Specifications for the Test Slant Well and Technical Specifications for the Monitoring Wells (Attachment 2 and Attachment 3 of the Hydrogeologic Investigation Workplan) will be updated if appropriate.

2.5.2 Hydrogeologic Investigation Report

The companion document to the Workplan will be the Hydrogeologic Investigation Report (HIR) and will include technical memorandums documenting all exploratory and testing activities as well as progressive model refinements and impacts. This document will include the following:

The Hydrogeologic Investigation Report will include a series of technical memorandum's which provide the data and analysis conducted throughout the study period including the following:

- Attachment 1 Technical Memorandum (TM) Summary of Results Exploratory Boreholes
- Attachment 2 Technical Memorandum (TM) Summary of Results Test Slant Well and Monitoring Wells
- Attachment 3 Technical Memorandum (TM) Summary of Results Long Term Pumping
 Test and Monitoring Well Program



 Attachment 4 - Technical Memorandum (TM) — Refined ground water model results following exploratory boreholes, monitoring wells, test slant well and full scale system

The current document is Attachment 1 of the Hydrogeologic Investigation Report.

2.6 Purpose and Scope

2.6.1 Purpose

As part of the Workplan, a geotechnical borehole investigation was undertaken at several sites along the Monterey coast. The purpose of the exploratory boreholes was to obtain information on the lithologic and hydraulic character of the hydrostratigraphic units and the vertical and horizontal distribution of the units. The data gathered from the boreholes will be used to update the NMGWM. The model layers will be refined using the site-specific depth and thickness information of the hydrostratigraphic units. The hydraulic properties of the units obtained from the field work and the water quality data will be used for model input. In other words, the borehole data will help to:

- Characterize the aquifer units,
- Characterize the water contained in the aquifer units (to determine if it is seawater, groundwater, or seawater intruded groundwater), and
- Determine if the Salinas Valley Aquitard (a blue clay layer) exists between the aquifer units at this location.

This technical memorandum:

- 1. Presents the results from the exploratory borings at the CEMEX facility (see Figure 2) and the Moss Landing area (see Figure 3),
- 2. Provides an interpretation of the geologic units encountered in the boreholes as they relate to the conceptual hydrogeologic model, and
- 3. Provides recommendations for refinements to the NMGWM based on the newly collected data.

2.6.2 Scope

The Moss Landing area investigation included drilling of exploratory borings at the Molera, Potrero Road, and Sandholt Road Salinas River State Beach parking lots and along Pacific Coast Highway and along Sandholt Road at Moss Landing Harbor. The CEMEX area investigation included exploratory



borings drilled on the CEMEX facility at locations approved by CEMEX. The approved scope of work for the investigation included the following:

- Drilling of sonic boreholes from depths ranging approximately 200 to 350 feet (ft) below ground surface (bgs)
- Collecting continuous soil cores from all borings
- Preparation of lithologic logs of the materials penetrated in each borehole
- Photographs of soil cores
- Geophysical borehole logs
- Construction of two groundwater quality sampling zones in each borehole in the Moss Landing area and collection of water samples from each zone
- Figures, maps, and photographs showing site locations and conditions
- Borehole destruction details
- Mechanical grading analysis
- Analysis of hydraulic conductivity using the Hazen Approximation, Krumbein-Monk, and Kozeny-Carman methods
- Laboratory vertical and horizontal permeameter testing
- Evaluation of groundwater quality conditions
- Preparation of recommendations for model layer revisions

2.6.3 Added Scope

At the initiation of this study, exploratory borings at the CEMEX facility were limited to the collection of lithologic and geophysical data only. More recently, the scope was expanded to include two additional boreholes at the CEMEX facility to collect groundwater quality samples for borings not previously sampled for groundwater quality (see Section 3.1.6). A water quality boring (CX-B1WQ) was drilled adjacent to Boring CX-B1. A second water quality boring (CX-B2WQ) was drilled near Boring CX-B2. A fourth boring (CX-B4, third water quality boring) was also drilled at CEMEX to obtain continuous core and geophysical logs for lithologic logging and to collect groundwater quality samples. The locations of the water quality borings at CEMEX are shown on Figure 2 and Figure 3. In addition, to further explore the area south of Potrero Road, an exploratory boring (MDW-1) was drilled in the Molera parking lot of Salinas River State Beach located at Monterey Dunes Way. Four isolated zones were constructed in MDW-1 to collect water quality samples.



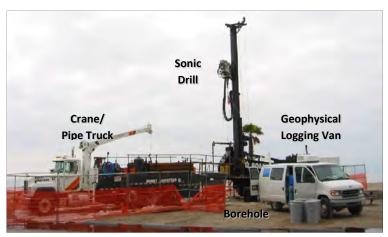
3.0 FIELD INVESTIGATION

3.1 Borehole Drilling and Sampling

3.1.1 Drilling

The sonic drilling method was used for all 13 boreholes for this investigation. All of the sonic drilling was completed by Cascade Drilling of Upland, California. Drilling commenced at the Potrero Road site in

September 2013. Sonic drilling produced continuous core samples that were minimally disturbed. The cores from all borings were logged by the field geologist, photographed, and placed in wooden core boxes. Detailed borehole logs for each borehole are provided in Appendix A1. The cores were placed in storage at the Cal Am facility in Pacific Grove, California. Sediment samples were collected of each lithologic unit encountered in



Sonic Drilling Rig and Support Equipment

the boreholes by the field geologist. Photographs of the core are provided in Appendix B. Table 3-1 below provides a summary of drilling dates for each exploratory boring.

Borehole Location **Drill Dates** PR-1 Moss Landing: SR State Beach Portrero Road Parking Lot September 20-26, 2013 ML-1 Moss Landing: SR State Beach Sandholt Road Parking Lot October 1-8, 2013 CX-B1 CEMEX October 21-26, 2013 CX-B2 **CEMEX** November 4-8, 2013 CX-B3 **CEMEX** November 9-13, 2014 ML-6 Moss Landing (MBARI) November 18-24, 2013 November 25,26 and ML-4 Moss Landing (Coast Highway) December 2-8, 2013 ML-2 Moss Landing (Del Mar Fisheries) December 9-20, 2013 ML-3 Moss Landing (Coast Highway) January 6-14, 2014 CX-B1WQ **CEMEX** February 17-26, 2014 March 4-7, 2014 CX-B2WQ **CEMEX** CX-B4 **CEMEX** March 20 - April 10, 2014 MDW-1 Moss Landing: SR State Beach Molera Parking Lot April 23-May 10, 2014

Table 3-1. Chronology of Field Investigation



3.1.2 Core Sampling

The core sampling was conducted using a 4-inch to 6-inch diameter inner casing. The core barrel is attached to small-diameter drill rods and is vibrated ahead of the outer casing collecting undisturbed formation materials as the core samples. With each 10-ft advance of the casing, the core barrel was extracted and brought to the surface to retrieve the core. Soil core samples were collected continuously during drilling of all the exploratory boreholes. Upon collection, all soil cores were placed in 6-mil polyethylene plastic sleeves measuring approximately 2 ft in length. Each bag was photographed and properly labeled in the field with the client name, boring number, sample depth interval, and date of collection. The core samples were then split longitudinally in half and visually classified (logged) in the field in accordance with the Unified Soil Classification System (USCS).





3.1.3 California-Modified Split-Spoon Sampling

Split-spoon samples were collected at specified depths from each borehole to obtain undisturbed samples of the formation materials for the purpose of estimating hydraulic conductivity using a laboratory permeameter. Samples were collected from the Dune Sand Aquifer, fine-grained aquitard

material, and coarse-grained material.

The split-spoon sampler holds three thin-walled metal (brass or stainless steel) sleeves measuring approximately 6 inches in length and 2.5 inches in diameter. The sampler was attached to a small diameter drill rod that is pushed through 18- to 24-inches of undisturbed formation material ahead of the drilling bit. Each time the split-spoon sampler is retrieved, the sampling sleeves were removed and the exposed ends were covered with Teflon® sheets, covered

Split Spoon Sampler with Brass Sleeves

with plastic caps, and taped to preserve the sample for laboratory testing. Each sleeve was marked with



the project name, borehole name, sample depth and number, and the date. The sample tubes were submitted to PTS Laboratories, Inc. of Santa Fe Springs, California under chain of custody protocol for analysis of vertical and horizontal soil hydraulic conductivity and selected soil parameters. Chain of custody forms are provided in Appendix C, along with the results of the laboratory testing.

3.1.4 Mechanical Grading Analysis

Representative samples of coarse-grained intervals were collected from core samples for mechanical grading analysis. The samples were sieved in the GEOSCIENCE soil laboratory and the grain size distribution was plotted on charts. The depth intervals at which samples were collected for mechanical grading analysis are shown on the corresponding lithologic log (see Appendix A1). Samples were sieved using U.S. Standard sieves with mesh sizes ranging from 0.0740 mm (0.0029 inches) to 9.525 mm (0.375 inches). Grain size distribution plots are provided as Appendix D. Grain size distribution was used to estimate the hydraulic conductivity; discussed in Section 3.2.3. Table 1 (attached) provides a summary of mechanical grading analysis and hydraulic conductivity estimates. Table 1 includes depth interval, lithology, geologic formation, conductivity direction, and the average hydraulic conductivity value for each sample interval. Soil types listed are based upon the results of the mechanical grading analyses.

3.1.5 Geophysical Borehole Logging

Once each borehole target depth was reached, the core barrel was removed and a 4-inch diameter PVC screen was installed within the borehole prior to removing the outer sonic casing. The PVC screen ensured that the borehole remained open during geophysical logging.

Geophysical logs were run throughout the total depth of each borehole. Each geophysical run included the following suite of logs:

- Dual Induction,
- Gamma,
- Temperature, and
- Fluid Resistivity.

<u>Dual induction logs</u> (DIL) were used to determine resistivity of formation materials by measuring conductivity adjacent to the induction tool.⁴ The induction tool focuses alternating electromagnetic



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⁴ Conductivity is measured as (mho/m) and is the inverse of resistivity.

currents into the formation, with medium and deep measurements determined by transmitter/receiver spacing. The DIL is comprised of six (6) separate measurements:

- **RILM** Resistivity, Induction Log Medium
- **RILD** Resistivity, Induction Log Deep
- CILM Conductivity, Induction Log Medium
- **CILD** Conductivity, Induction Log Deep
- SP Spontaneous Potential
- **GR** Gamma Ray

<u>Gamma ray</u> (GR) logs were used to augment and aid identification of lithologic units encountered within each borehole.

<u>A temperature log</u> measures absolute fluid temperature within a borehole. A calculated differential measurement is provided with the log, which allows detection of vertical fluid movement within a borehole, including fluid entry and exit points.

<u>Fluid resistivity logs</u> provide a measure of the resistivity of borehole fluid (in units of ohm-m) and provide a calculated differential curve. This log was used for correlation of temperature measurements, to assist in locating the presence of borehole water with higher total dissolved solids (TDS) concentrations, and to differentiate between waters from various contributing aguifer zones.

All geophysical logs are provided in Appendix E. The geophysical borehole logs and lithologic descriptions were used to determine recommended depth intervals for zone testing and to delineate the aquifer systems in the study area. The results will be used to design project monitoring wells for long-term aquifer testing.

3.1.6 Isolated Aquifer Zone Testing for Water Quality Sample Collection

Following completion of geophysical logging, the lithologic and geophysical logs were reviewed to select depth intervals that would likely yield groundwater with the lowest and highest salinity. Depth intervals selected were used to construct isolated aquifer zones for groundwater quality sampling. An isolated aquifer zone test consists of constructing a temporary well with a 10-foot well screen interval placed at the depth of the lithologic unit to be tested. A seal is constructed above and below the well screen to isolate the portion of the aquifer for water quality testing. Two depth intervals were selected for groundwater sampling zones for each Moss Landing borehole (Borings MI-1, ML-2, ML-3, ML-4, ML-6,



and PR-1). Four isolated zones were constructed in Boring MDW-1. For the CEMEX area, a water quality boring was drilled near Boring CX-B1 and designated Boring CX-B1WQ. Another boring was drilled near Boring CX-B2 and designated as Boring CX-B2WQ. A third boring, Boring CX-B4 was drilled approximately 1,500 feet inland from CX-B2WQ and used to collect water quality samples. The locations of the water quality borings (CX-B1WQ, CX-B2WQ, and CX-B4) are shown on Figure 3. Six zones were selected for construction in Boring CX-B1WQ in an effort to assess potential water quality changes between the Dune Sand Aquifer and the underlying aquifer units. The groundwater quality samples were sent to the laboratory with an expedited request. After receipt of groundwater quality results for samples from Boring CX-B1WQ, and after reviewing the geophysical logs and lithologic logs, four zones were selected for Boring CX-B2WQ. The zones were selected to confirm and augment water quality data collected from Boring CX-B1WQ, and to develop an overall profile of groundwater quality at the CEMEX site. Five zones were selected for Boring CX-B4.

Each isolated zone was constructed by placing a bentonite seal below the selected zone interval. A 10-ft PVC screen was placed opposite the selected sampling interval and filter pack consisting of Monterey Sand #3 was placed opposite, above, and below the well screen. A second bentonite seal was placed above the filter pack interval. The bentonite seals effectively isolated the groundwater quality interval from groundwater above and below the selected interval. Each isolated aquifer zone is constructed specifically for the hydrogeologic conditions at the borehole site. The isolated aquifer zone testing forms are provided in Appendix F. Table 3-2 below summarizes the depth of zones by boring selected for the water quality sampling. A total of 31 zones were constructed for water quality sampling.

Table 3-2. Isolated Aquifer Zone Depth Intervals

Zone No.	ML-1	ML-2	ML-3	ML-4	ML-6	PR-1	MDW-1	CX-B1 WQ	CX-B2 WQ	CX-B4
Zone 1 (ft bgs)	113.5- 118.5	167-177	180-190	163.5- 173.5	152-162	190-200	237-247	274-284	215-225	306-316
Zone 2 (ft bgs)	90-100	90-100	103-113	74.5-84.5	100-110	125-135	187-197	237-247	161-171	248-258
Zone 3 (ft bgs)	-	1	1	1	1	,	152-162	182-192	104-114	155-165
Zone 4 (ft bgs)	-	1	,		1		60-70	134-144	55-65	110-120
Zone 5 (ft bgs)	-	-	-	-	1	,		84-94	-	58-68
Zone 6 (ft bgs)	-	-	-		-	-		51-61		
Total Depth (ft bgs)	200	200	200	201	200	200	300	306	250	350

See Appendix F for zone construction details.



Once a zone was constructed, the aquifer unit across from the well screen was developed using a swab and brush to remove fine sediment. A submersible pump was placed in the temporary well and pumped. Field measurements of groundwater quality were collected to evaluate when the groundwater quality had stabilized, and a representative sample of the aquifer unit was collected. Groundwater quality parameters measured and recorded in the field are provided in Table 3-3.

Table 3-3. Field Groundwater Quality Parameters

Parameters and Units					
Time (minutes)	Salinity (ppt)				
Water Level (depth in feet, bgs)	Dissolved Oxygen (DO) (mg/L)				
Temperature (degrees F)	рН				
Conductivity (us/cm)	Oxygen Reduction Potential (ORP) (mV)				
Calculated Total Dissolved Solids (TDS) (mg/L)	Turbidity (NTU)				

The field measurements were collected approximately every three to five minutes, until at least three field parameters stabilized. The stabilization criteria are provided in Table 3-4.

Table 3-4. Parameter Stabilization Criteria

Parameters and Units					
рН	+/- 0.1 unit				
Conductivity	+/- 3%				
ORP	+/- 10 mV				
Turbidity	+/- 10%				
DO	+/- 10%				

Groundwater samples were not collected until the turbidity reading was less than 1 NTU in order to avoid the potential for additional metal concentrations from sediments within the sample. Copies of the field data sheets used to record field parameters during zone testing are provided in Appendix F. The results of the laboratory testing are summarized in Table 3a and Table 3b. Copies of the groundwater quality laboratory reports are provided in Appendix G.



3.1.7 Borehole Destruction

Each exploratory borehole was destroyed immediately following completion of geophysical logging (Borings CX-B1, CX-B2 and CX-B3) or after isolated aquifer zone testing (remainder of borings). Each borehole was destroyed by filling with neat cement and native materials. To prevent material bridging during placement, all materials used for borehole destruction were placed through a tremie pipe. Borehole destruction was accomplished in accordance with the approved borehole destruction plan submitted by Cascade Drilling to Monterey County Health Department and in accordance with DWR Bulletins 74-81 and 74-90. The fine-grained units (i.e., aquitards) encountered beneath the Dune Sand Aquifer were sealed using a neat cement grout to insure that mixing of groundwater does not occur between aquifer units.

3.2 Estimates of Hydraulic Conductivity

Multiple estimates of hydraulic conductivity were made using mechanical grading analysis properties and vertical and horizontal conductivity/permeability values from laboratory analyses of relatively undisturbed soil samples.

3.2.1 Mechanical Grading Analysis

Mechanical grading analyses were used to determine the distribution of sediment grain sizes from samples collected from the continuous core. Three analytical methods were used to estimate hydraulic conductivity from the distribution of grain size in the samples. The Hazen Approximation, Krumbein-Monk, and Kozeny-Carman methods were used to estimate hydraulic conductivity from grain size distribution curves. A brief description of these methods is provided below.

Hazen Approximation

Hazen's Approximation is an empirical equation that estimates hydraulic conductivity to be proportional to the square of the effective grain size, which is expressed as:

$$K = C (d_{10})^2$$

Where:

K = Hydraulic conductivity (cm/s)

C = Hazen's constant, approximately 1 (dimensionless)

 d_{10} = Grain size in mm for which 10% of the particle pass by weight



This method is applicable to sands where the effective grain size (d_{10}) is between approximately 0.1 and 0.3 mm. Hazen's Approximation was originally determined for uniformly graded sands, but it can provide rough but useful estimates for most soils in the fine-grained sand to gravel range (Freeze and Cherry, 1979).

Krumbein-Monk

Krumbein and Monk (1942) described hydraulic conductivity in the form of Darcies for unconsolidated sands with a log-normal grain size distribution. Using this description, they used a semi empirical equation assuming forty percent porosity, which is expressed as:

$$K = \frac{\rho_{\omega}g}{\mu} \cdot \left[\frac{\phi^3}{1-\phi^2}\right] \cdot \frac{d_{\rm m}^2}{180}$$

where:

 ρ_{ω} = Fluid density (kg/m³ or ft/s³), assumed to be the average temperature of groundwater (22 degrees Celsius)

d_m = Particle diameter or characteristic length of a given material (m or ft)

μ = Dynamic viscosity (Pa-s pr lbs-s/ft²), also assumed to be the average temperature of groundwater (22 degrees Celsius)

g = Gravitational constant $(m/s^2 \text{ or ft }/s^2)$

Kozeny-Carman

One of the most widely used equations for determining hydraulic conductivity from characteristic lengths is the Kozeny-Carman Equation. Kozeny proposed in 1927, which was later modified by Carman in 1956, a method for determining hydraulic conductivity from the following:

$$K = \frac{\rho_{\omega} g}{\mu} \left[\frac{n^3}{(1-n)^2} \right] \frac{d_m^2}{180}$$

where:

 ρ_{ω} = Fluid density (kg/m³ of ft/s³), assumed to be the average temperature of groundwater (22 degrees Celsius)



n = Total Porosity
 μ = Dynamic viscosity (Pa-s or lbs-s/ft²), also assumed to be the average temperature of groundwater (22 degrees Celsius)
 g = Gravitational constant (m/s² or ft/s²)
 d_m = Harmonic mean particle diameter calculated from the particle size distribution (m or ft)

and

$$d_{\rm m} = 100\% / \left[\sum \left(\frac{f_{\rm i}}{D_{\rm ave,i}} \right) \right]$$

where:

f_i = fraction of particles between two sieve sizes; larger [I] and smaller [s] (%)

 $D_{\text{ave,i}}$ = average particle size between two sieve sizes (cm) = $D_{li}^{0.5} \times D_{si}^{0.5}$

Table 1 (attached) provides a summary of hydraulic conductivity calculations based on mechanical grading analyses from the three methods. The soil types listed may not represent the complete lithologic interval from which they were obtained since the lithology is generally bedded and gradational.

3.2.2 Summary of Hydraulic Conductivity Values

Table 3-5 summarizes the hydraulic conductivity estimates from mechanical grading analyses for ten soil types collected from both the CEMEX and Moss Landing sites. First, the average hydraulic conductivity was calculated separately for all soil types using each method. Secondly, the range of horizontal hydraulic conductivity shown in the Table 3-5 for each type of soil was determined by the method yielding the minimum average and the method yielding the maximum average hydraulic conductivity.



Table 3-5. Summary of Average Hydraulic Conductivity Estimates by Soil Type

Summary of Hydraulic Conductivity Estimates from Mechanical Grading Analys					
Soil Type (Unified Soils Classification System Designation)	Horizontal Hydraulic Conductivity Range (ft/day)				
Organic Clay (CH)	NA				
Silty Clay (CL)	NA				
Silt (ML)	NA				
Silty Sand (SM)	77 - 223				
Poorly Graded Sand (SP)	112 - 349				
Well Graded Sand (SW)	468 - 1,440				
Sand with Silt (SP-SM)	33 - 135				
Sand with Gravel (SP+Gravel)	342 - 817				
Silty Sand Sand + Gravel (SM+ Gravel)	311 - 1,150				
Well Graded Sand + Gravel (SW + Gravel)	469 - 859				
Well Graded Sand + Gravel (SW + Gravel)	445 - 1,322				
Sand with Clay + Gravel (SW-SC + Gravel)	446 - 1,511				
Gravel (GW)	334 - 849				

Table 3-6 summarizes the hydraulic conductivity estimates using the same approach as Table 3-5 but separately for samples collected from CEMEX and samples collected from Moss Landing. Not all soil types were represented at both sites. In the case where a sample was represented at only one site (i.e., GW: Gravel at CEMEX) the range of hydraulic conductivity was taken from Table 3-5. If a soil type was obtained from both CEMEX and Moss Landing sites (i.e., SW: Well- Graded Sand), the average hydraulic conductivity was calculated separately for each site from the range of values estimated from the samples collected at each site. For the SW: Well-Graded Sand example, the range of average hydraulic conductivity values reported in Table 3-5 falls between the range of average values calculated from each site individually, as shown in Table 3-6.



Table 3-6. Range of Hydraulic Conductivity from Mechanical Grading Analysis (MGA)

	MGA, (CEMEX ¹	MGA, Moss Landing ¹		
Lithology	Min Avg Permeability, K [ft/day]	Max Avg Permeability, K [ft/day]	Min Avg Permeability, K [ft/day]	Max Avg Permeability, K [ft/day]	
GW: Gravel	334	849	-	-	
SM: Silty Sand	50	144	146	421	
SM: Silty Sand with Gravel	-	-	311	1,150	
SP: Sand	113	331	112	356	
SP: Sand with Gravel	176	549	397	907	
SP-SM: Sand with Silt	-	-	33	135	
SP-SM: Sand with Silt and Gravel	-	-	445	1,322	
SW: Well-Graded Sand	286	1,012	619	3,364	
SW: Well-Graded Sand with Gravel	-	-	469	859	
SW-SC: Sand with Clay and Gravel	-	-	446	1,511	

¹ Mechanical grading analysis of formation samples performed by GEOSCIENCE Support Services, Inc. CEMEX MGA includes samples from boreholes CX-B1, CX-B2, CX-B3, and CX-B4. Moss Landing MGA includes samples from boreholes PR-1, ML-1, ML-2, ML-3, ML-4, and ML-6, and MDW-1.

Only one hydraulic conductivity value calculated from pumping test data is available for the aquifer units at CEMEX. Staal, Gardner, and Dunne (SGD, 1992) completed a pumping test in the Dune Sand Aquifer in 1992. Their reported hydraulic conductivity value is 1,750 gpd/ft², or approximately 230 ft/day. Table 3-7 provides a summary of the minimum and maximum hydraulic conductivity values for the CEMEX area. The value reported by SGD is comparable to the value estimated for the CEMEX borehole samples for the Older Dune Sand.

Table 3-7. Hydraulic Conductivity for Geologic Units at CEMEX

Geologic Unit	Minimum K-Value (ft/day)	Maximum K- Value(ft/day)
Dune Sand (Qd)*	273	779
Older Dune Sand (Qod)	136	372
Terrace Deposits (Qt)	113	342

^{*}Data from Moss Landing for Qd used here.

Table 3-8 provides a summary of minimum and maximum hydraulic conductivity values for the Moss Landing area.



Table 3-8. Hydraulic Conductivity for Geologic Units at Moss Landing

Geologic Unit	Minimum K-Value (ft/day)	Maximum K-Value (ft/day)
Dune Sand (Qd)	227	619
Perched "A" Aquifer (Qal)	194	717

3.2.3 Laboratory Permeameter Estimates

Undisturbed drive samples were collected from each exploratory boring. A total of 41 samples were submitted for laboratory vertical and horizontal permeameter testing. Samples were selected to represent the Dune Sand Aquifer, fine-grained units such as clay layers, and the aquifer units underlying the Dune Sand Aquifer. The laboratory test reports are provided in Appendix C. Table 2 (attached) summarizes the laboratory vertical and horizontal permeability results. Table 3-9 below summarizes the range of laboratory permeability values based on soil type. The laboratory results in general are much lower than anticipated. The horizontal values appear significantly lower than an anticipated increase of 10 to 20 times the vertical permeability values.

The values provided from both the laboratory permeameter test and the mechanical grading analyses are approximate and will be revisited during the long-term aquifer test. However, the values estimated using the mechanical grading analysis are much closer to those anticipated from future aquifer testing and will form the starting point for refinements to the model in the CEMEX and Moss Landing area.

Table 3-9. Summary of Laboratory Hydraulic Conductivity Results by Soil Type

Summary of Laboratory Hydraulic Conductivity Results by Soil Type							
Soil Type (Unified Soils Classification System Designation)	Vertical Hydraulic Conductivity Range (ft/day)	Horizontal Hydraulic Conductivity Range (ft/day)					
Organic Clay (CH)	0.003 - 0.014	NA					
Silty Clay (CL)	0.005 - 0.283	NA					
Silt (ML)	0.03	0.02					
Silty Sand (SM)	0.20 - 1.38	0.37 - 4.34					
Poorly Sorted Sand (SP)	0.28 - 17.29	1.80 - 36.56					
Sand + Gravel (SP+ Gravel)	0.26 - 14.91	0.17 - 14.51					
Sand/ Silty Sand (SP/SM)	0.13	0.31					
Sand/Silty Sand/Gravel (SP/SM + Gravel)	24.15	17.74					
Well Graded Sand + Gravel (SW + Gravel)	13.18	11.34					



4.0 GEOHYDROLOGIC SETTING

4.1 Historical Background

This study includes an investigation of the geohydrologic conditions along the coast at the mouth of the Salinas River from Moss Landing south to the CEMEX facility (see Figure 1). Groundwater is present in multiple aquifer systems in several subbasins in the project area. Data from this study indicates that water quality is variable both in vertical and areal distribution. Historically, a large proportion of groundwater was extracted for agricultural purposes in the Salinas Valley. The Salinas Valley Groundwater Basin underlies the long linear Salinas Valley, which extends approximately 100 miles from headwaters in the southeast to Monterey Bay in the northwest at Moss Landing.

The relatively flat fertile floodplains along the Salinas River were developed for farming; therefore, wells were drilled to supply water for the agricultural development. The hydrogeologic nomenclature and hydrogeologic conceptual model was initially developed as a result of the subsurface information obtained from the drilling of the wells for agriculture.

The California Department of Water Resources (1946) cites the Eleventh Census for 1890 regarding irrigation in Monterey County:

...near the mouth of the Salinas River there were reported to be 60 flowing wells upon farms in 1890 most of them being not far from Castroville. They range in depth from 60 to 189 feet, the average being 136 feet.....They are reported to fluctuate with the season, many of them ceasing to flow in the summer..... At Salinas at about 10 miles from the coast, most deep wells are pumped by windmills.

This historical description of groundwater use clearly conveys groundwater use in the Salinas Valley started early, and, as is the case for many parts of California, wells were drilled into the shallow upper aquifers first, followed by wells into deeper aquifers as greater quantities of water were required for supply. The flowing wells described in 1890 confirm that these early wells were drilled beneath an upper confining layer. DWR (1946) reports that the number of farms in the Valley increased from 21 farms in 1889 to 803 farms by 1929. In 1933, it was reported "that the quality of water in Salinas Valley as a whole was excellent." However, with the advancement in well pump technology, many new large capacity pumping plants (wells) were brought into use. This resulted in an increasing number of wells being placed out of use from seawater intrusion by 1944. The description of the depths of the wells shows that the upper aquifer within the Salinas Valley was the first to be intruded by seawater, and experienced the furthest migration of seawater with time. Seawater intrusion maps published by the Monterey County Water Resources Agency (MCWRA) support this condition.



The historical conditions are significant to the current project because seawater was introduced into the freshwater aquifers beginning at the coast, with a continuous landward migration. This condition appears to correlate with the lowering of inland groundwater levels induced from agricultural pumping. It is our understanding, that a well at CEMEX has historically been included for monitoring seawater intrusion.

4.2 Groundwater Subbasins

4.2.1 "Pressure" Subarea and 180/400-Foot Aquifer

Both the Moss Landing and CEMEX areas lie within the 180/400-Foot Aquifer Subbasin as delineated by the DWR. DWR Bulletin 118 describes the 180/400-Foot Aquifer Subbasin as follows:

180/400-Foot Aquifer — Boundary with Corral de Tierra represents the contact between the Quaternary Paso Robles Formation or Aromas Red Sands and the Quaternary Alluvium or Terrace Deposits. Boundary with Seaside Area Subbasin represents seaward projection of the King City Fault (may act as barrier to flow). Northern boundary is the Pajaro Valley Groundwater Basin and coincides with inland projection of a 400-ft deep, buried clay-filled paleodrainage of the Salinas River. Northeastern boundary generally coincides with the northeastern limit of confining conditions in the 180/400-Foot Aquifer Subbasin and Highway 101. Southeastern boundary is the approximate limit of confining conditions in an up-valley direction. Boundaries generally coincide with those of the Pressure Subarea of MCWRA.

The 180/400-Foot Aquifer Subbasin is characterized by confined groundwater conditions both historically and as described in DWR Bulletin 118.

The 180/400-Foot Aquifer Subbasin is bounded by groundwater divides on the south by the Seaside and the Corral de Tierra Subbasins.

4.2.2 Seaside and Corral de Tierra Subbasins

The Seaside Subbasin borders the 180/400-Foot Aquifer Subbasin to the south. The Seaside Subbasin is described by DWR as:

The Seaside Subbasin "northeast boundary is the Salinas Valley proper (180/400-Foot Aquifer), southeast boundary roughly represents the extent of Quaternary sand."

The Corral de Tierra Subbasin borders the 180/400-Foot Aquifer Subbasin on the south, further inland than the Seaside Subbasin. The Corral de Tierra Subbasin is described by DWR as:



The Salinas Valley-Corral de Tierra Area Subbasin comprises the eastern portion of the former Fort Ord and other unincorporated areas. The subbasin includes outcrops of Plio-Pleistocene nonmarine units, including the Aromas Sands, the Paso Robles Formation. The subbasin is bounded on the northwest by the Seaside Area subbasin and on the northeast by the 180/400 foot aquifer subbasin. On the south and southwest the subbasin is bounded by Middle Miocene marine rock units, and a portion of the eastern boundary is a small area of Mesozoic granitic rocks (DWR, 2004).

4.4 Regional Geologic Setting

Older geologic maps from the 1970s are available which show the onshore and offshore area of Monterey Bay and the description and distribution of stratigraphic units in the area. Seminal work in evaluating the Quaternary geology in the study area was completed by John Tinsley III and William R. Dupré in 1975 as doctoral dissertations submitted to Stanford University. Both dissertations address the distribution and genesis of Quaternary geologic units in the study area and will be referred to later in this section. More recently, the California Geological Survey published a report in 2002 titled "Geologic Map of the Monterey 30'x 60' Quadrangle and Adjacent Areas". Geologic maps are available at scales ranging from 1:100,000 to 1:24,000. These maps form the basis for the current conceptual model of geologic conditions in the vicinity of the project site. A geologic map of the project area is provided as Figure 6a.

In general, the geologic units mapped at the surface in the study area include, from oldest to youngest:

- Aromas Sand
- Quaternary Marine Terrace Deposits
- Quaternary Terrace Deposits
- Older Dune Sand
- Older Alluvium
- Younger Dune Deposits
- Quaternary Basin Fill Alluvium and Floodplain Deposits

A discussion of geologic units is provided in the following sections.



4.4.1 Aromas Sand (Qar, Qae, and Qaf)

The Aromas Sand designated as Qar (undiffentiated Aromas Sand), Qae (eolian lithofacies of the Aromas Sand) and Qaf (fluvial lithofacies of the Aromas Sand) is present near the study area. The Aromas Sand is early Pleistocene in age and crops out north of the Salinas Valley proper on southwest facing slopes above Castroville. The Aromas Sand in this area is overlain by Older Dune Sand deposits, terrace deposits, the Antioch Alluvial Fan, and the Chualar Alluvial Fan (see Figure 6a). Due to the current uncertainty associated with the location and/or extent of the Aromas Sand in the CEMEX area and the regional dune highlands, the USGS (Tinsley, 2014) recommends using a question mark (?) following the name Aromas to denote that a type section for the units formally designated as the Aromas Sand in the Moss Landing and Watsonville areas has not been established in the area south of the Salinas River and the Aromas (?) unit south of the Salinas River is likely an equivalent unit. The Aromas Sand (?) crops out in the eastern part of the Ford Ord area. The unit in this area is underlain by the Paso Robles Formation and overlain by Older Dune Sand deposits. Overall, the outcrops of the Aromas Sand form an arcuate shape from south of the Salinas River to the north. The unit has been eroded in the Salinas Valley during lowering of sea levels to elevations between -200 and -300 ft amsl (Kennedy/Jenks, 2004) which roughly corresponds with the Wisconsinan sea level lowstand offshore at -300 ft amsl at 17,000 years before present (bp; USGS, 1991). With sea level rise in the Holocene (11,000 years bp), the Salinas River Valley was backfilled with Valley Fill deposits. According to Tinsley, the "Base of Holocene marine transgression at this locality (Leonardini Well) occurs at approximately 150 ft below mean sea level (-150 ft above mean sea level, amsl)."

4.4.2 Quaternary Marine Terrace Deposits (Qmt)

According to Dupré, marine terraces flank both the northern and southern margins of Monterey Bay. They formed in response to glacioeustatic fluctuations in sea level. The youngest terraces in the Santa Cruz area were formed during the Sangamon sea level highstands (at 102,000 and 118,000 years bp; Dupré, 1990). Quaternary Marine Terraces are mapped near Moss Landing (see Figure 6a and Figure 8) and north of Elkhorn Slough.

4.4.3 Quaternary Terrace Deposits (Qt)

Terrace deposits are present along and elevated above the Salinas River floodplain. The terrace deposits represent former alluvial fan and river floodplain surfaces, and range in age from early to mid-Pleistocene. Terrace surfaces and their relative stratigraphic positions were mapped by Tinsley (1975) using soil stratigraphic methods. The stratigraphic positions of the terraces associated with the alluvial fans in the northern Salinas Valley were used to interpret the stratigraphic relationships shown on Figure 8. According to Tinsley a distinguishing feature of the Salinas River deposits originating from below the Arroyo Seco drainage which enters the Salinas Valley approximately 40 miles upstream from



the south, is an abundance of porcellaneous chert from the Monterey Formation. The clast type can occur both in older terrace deposits (Tinsley, 2014) as well as younger fluvial deposits which lie beneath the Salinas Valley.

4.4.4 Older Dune Sand (Qod)

The Older Dune Sand (late Pleistocene) is also present in project area. These deposits are much more extensive in the project area south of the Salinas River Valley, extending inland as far as the East Garrison of former Fort Ord (approximately 5 miles inland). However, north of the Salinas River, the Older Dune Sand is limited in extent and crops out in small non-contiguous areas. Further north, nearing the Watsonville area, Older Dune Sand deposits are again extensive, occupying much of the coastal areas. Work completed by Dupré (1975) included study of the Manressa and Sunset Dunes, which are the coastal dunes located north of the Salinas River in the Watsonville area. These dunes are similar to what is called the Fort Ord ERG Dune Complex present in the CEMEX and Fort Ord areas. The term "ERG" is used to describe the landform which is made up of a large dune field. The Older Dune Sand deposits in the Fort Ord area are reported to be as much as 250 ft thick (HLA, 2001). The Dupré work has shown that the Older Dune Sand deposits rest on top of terrace deposits (Santa Cruz Terrace).

Dupré (1975) reports:

The Manressa Coastal Dunes conformably overlie the Santa Cruz coastal terrace deposits, hence were deposited during lowering sea level...The Manressa dunes are probably late Sangamonian/early Wisconsinan. The Sunset Dunes are similar in form and probably in origin to the Manressa Dunes, thus they record an interval of dropping sea level following a mid-wisconsinan interstadial highstand.

Dupré notes that the Older Dune Sand deposits (in the Watsonville area) were deposited during a lowering of sea level between the interglacial Sangamon sea level highstand (125,000 - 85,000 years bp) and glacial Wisconsinan sea level lowstand (85,000 - 11,000 years bp). The current Holocene (11,000 years bp to present) represents the most recent interglacial period.

4.4.5 Older Alluvium (Qo)

Older alluvial deposits are not mapped at the surface in the study area, but underlie the Holocene deposits in the Salinas River Valley. These deposits are late Pleistocene and are likely in erosional contact with terrace deposits. The Older Alluvium contains organic "blue clay" horizons located beneath the Holocene floodplain of the Salinas River, and is typically referred to as the Salinas Valley Aquitard (SVA). According to Tinsley (1975), the presence of this "blue clay" indicates that shallow marine to



brackish water estuarine environments prevailed during the deposition of the horizons, forming the principle aquicludes and aquitards in the 180/400 Foot Aquifer Subbasin.

4.4.6 Younger Dune Deposits (Qd)

Younger dune and beach sand deposits extend along the shoreline of Monterey Bay from the southern end of the Bay, northward to Moss Landing. The deposits are absent in the immediate vicinity of the mouth of the Salinas River (USGS Open File Report 02-373). The dune sand deposits extend landward approximately 0.1 to 0.5 miles inland. The Younger Dune Sand is Holocene in age and overlies older Dune Sand south of the Salinas River and older alluvial deposits along the mouth of the Salinas River Valley. It is likely that the recent dune sand rests over fluvial deposits (which form a shallow aquifer) in the area where the Salinas River Valley meets the ocean. However, to the south of the Salinas River Valley near the community of Marina and Fort Ord, the recent dune sand directly overlies older dune sand deposits.

4.4.7 Quaternary Basin Fill (Qb) Alluvium (Q) and Floodplain Deposits (Qfl)

The Quaternary basin fill, alluvium, and floodplain deposits are Holocene in age, consisting of sedimentary material deposited by the Salinas River and/or its tributaries. These units are mapped within the central portion of the Salinas Valley.

4.5 Local Geology

4.5.1 CEMEX Area

In the CEMEX area, younger and older dune deposits overlie Quaternary terrace deposits. The area is within the western edge of the Older Dune Complex, which is bounded by the Salinas River Valley to the north and extends from the coast to a maximum distance of five miles inland (see Figure 6a). The CEMEX area has been dominated by eolian (wind blown) depositional processes, while the Salinas River Valley is dominated by riverine fluvial depositional processes. The CEMEX area represents a distinct geomorphic area from the Salinas River Valley.

The concept of the formation of coastal dunes during the lowering of sea level as reported by Dupré (1975) suggests that the Older Dune deposits are either equivalent in age or older than the sand, silt, and gravel which form the 180-Foot Aquifer in the Salinas Valley to the north. These fluvial deposits which make up the 180-Foot Aquifer deposits were laid down as the Salinas River Valley degraded its channel during Wisconsinan time. The 180-Foot Aquifer was subsequently capped as sea levels rose at the beginning of the Holocene, forming an estuary and the SVA. The geologic units which form the 180-Foot Aquifer are stratigraphically equivalent but chronologically younger than the terrace deposits which underlie the Older Dune deposits at the CEMEX site.



DWR (2004) notes the "180-Foot Aquifer may in part be correlative to older portions of Quaternary terrace deposits or the upper Aromas Sand". Cross-Section 1-1' (Figure 7a) depicts the relationship between the geologic units that make up the 180-Foot Aquifer present beneath the Salinas Valley and the stratigraphic units encountered in the CEMEX boreholes. The degree of hydraulic connection will be initially evaluated using the CM and the NMGWM but, more significantly, will be field investigated with the test slant well program.

4.5.1.1 Findings from CEMEX Boreholes

Four boreholes were drilled to depths between 306 and 350 ft bgs. The locations are shown on Figure 3. Boring CX-B1 was located closest to the ocean. Boring CX-B2 was located 600 ft inland from CX-B1 along the CEMEX haul road. Boring CX-B3 was located near the CEMEX maintenance shop approximately 1,800 feet from Boring CX-B1, and CX-B4 is located 500 feet east of CX-B3 and approximately 2,700 feet from the shoreline. Lithologic units were found to be similar in all four borings (see boring logs in Appendix A1). The table below summarizes the geologic units encountered in the CEMEX borings CX-B1, CX-B2, CX-B3, and CX-B4.

Table 4-1. Depths of Geologic Units in CEMEX Borings (ft bgs)

Depths of Geologic Units in CEMEX Borings (ft bgs)							
Caalagialluit	Borehole						
Geologic Unit	CX-B1	CX-B1 CX-B2 CX-B3 CX-B4					
Qd	0-25	0-28	0-20	0-27			
Qod	25-85	28-90	20-90	27-95			
Qt	85-245	90-240	90-253	95-255			
Qar	below 265	below 270	below 287	below 292			

Geologic Cross-Section 1-1' (Figure 7a) illustrates the extent of the geologic units in the subsurface and indicates the hydrostratigraphic units associated with each geologic unit. Figure 7b is a close up in the CEMEX area.

4.5.2 Moss Landing Area

The investigation at Moss Landing is inclusive of the area from the Salinas River State Beach Molera parking Lot at Monterey Dunes Way (Boring MDW-1) to the Monterey Bay Aquarium Research Institute (MBARI) located at the northern terminal end of Sandholt Road (Boring ML-6). The geologic units include Younger Dune Deposits (Qd), recent alluvium (Qal), and basin fill deposits (Qb) near the coast. The area around the Pacific Coast Highway is underlain by Older Dune Deposits (Qod) and Quaternary Marine Terrace Deposits (Qmt). Further to the northeast, as land surface elevation increase, the alluvial



fan deposits (Qfa) predominate and are underlain by the Aromas Sand (Qar) which crops out near Elkhorn and Prunedale. The distribution of surface geologic units is shown on Figure 6a.

4.5.2.1 Findings from Moss Landing Boreholes

A total of seven exploratory borings were drilled at the Moss Landing study area. The locations of all of the borings are shown on Figure 2. The five borings drilled in Moss Landing Harbor are shown on Figure 4. Lithologic logs of the borings are presented in Appendix A1. Geologic Cross-Sections 2-2' and 3-3' provided as Figure 8 and Figure 9, respectively, depict the geologic relationships in the Moss Landing area. Cross-Section 2-2' shows Pleistocene Alluvial Fan deposits overlain by Quaternary Marine Terrace Deposits, and in erosional contact with Older Alluvium which contains the 180-Foot Aquifer and the Perched "A" Aquifer. The Older Alluvial deposits are interpreted to extend seaward and be exposed in the walls of Monterey Canyon to the west.

Cross-Section 3-3' parallels the coast extending from the City of Marina to Moss Landing Harbor, and depicts mixed units of sand, silt, clay, and gravel which do not appear to be laterally or vertically extensive. The sand and gravel units encountered in Boring PR-1 showed the greatest thickness (99 ft) of permeable alluvium. The unit appears to decrease in thickness to the south and pinch out south of Boring MDW-1. Deposits interpreted as the SVA were penetrated in Boreholes MDW-1, PR-1, and ML-1 (see Figure 9). Figure 4-1 (Tinsley, 1975) provides a schematic depicting the relationship between the Pleistocene alluvial deposits and the alluvium which contains the SVA and 180-Foot Aquifer beneath the Salinas Valley near Salinas.



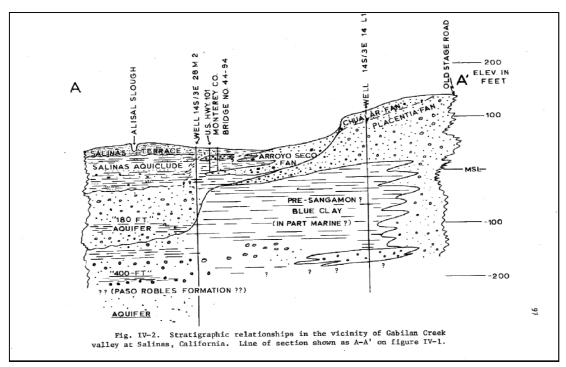


Figure 4-1. Reproduced from Figure IV-2 of Tinsley, 1975

4.6 Hydrostratigraphy

Traditionally, aquifers in the Salinas Valley Groundwater Basin have been named for the average depth at which they occur (e.g., 180-Foot Aquifer). Water-bearing materials in the area, from oldest to youngest, consist of the Pliocene marine Purisima Formation, Plio-Pleistocene Paso Robles Formation, Pleistocene Aromas Sands, and Holocene Valley Fill materials (Greene, 1970).

Table 4-2 below provides a correlation of surface mapped geologic units shown on Figure 6a and the hydrostratigraphic unit associated with the geologic unit. These units correlate with the CM and NMGWM, and are discussed in Section 6.



Table 4-2. Correlation of Geologic and Hydrostratigraphic Units

180/40	0-Foot Aquifer S	ubbasin	CEMEX Area			
Geologic Unit	Geologic Unit Map Symbol	Hydrostratigraphic Units	Geologic Units	Geologic Unit Map Symbol	Hydrostratigraphic Units	
Benthic Zone		Benthic Zone	Benthic Zone		Benthic Zone	
	1	- 1 1//2 1/ 2 15	Dune Sand	Qd		
Alluvium	Qal ¹	Perched "A" Aquifer	Older Dune Sand	Qod	Dune Sand Aquifer	
Older Alluvium	Qo	Salinas Valley Aquitard				
Older Alluvium/ Marine Terrace	Qo/Qmt	180-Foot Aquifer	Older Terrace/ Marine Terrace	Qt (Qmt?)	180-FTE ²	
Older Alluvium/ Older	Qo/Qfa					
Older Alluvial Fan – Placentia	Qfp	180/400-Foot Aquitard			180/400-Foot Aquitard	
Aromas Sand (undifferentiated)	Qar		Aromas Sand (undifferentiated)	Qar (?)		
Aromas Sand – Eolian/ Fluvial Lithofacies	Qae/Qaf	400-Foot Aquifer	(?)		400-Foot Aquifer	
Paso Robles Formation	QT	400/900-Foot Aquitard 900-Foot Aquifer	Paso Robles Formation	QT	400/900-Foot Aquitard 900-Foot Aquifer	

¹Subsurface Holocene geologic unit not mapped at surface

In the 180/400-Foot Aquifer Subbasin, the aquifer units from oldest to youngest include the 900-Foot Aquifer, 400-Foot Aquifer (generally thought to be contained in the upper part of the Aromas Sand), and the 180-Foot Aquifer present with the Older Alluvium and separated from the overlying Perched "A" Aquifer by the Salinas Valley Aquitard. Thicknesses of individual aquifer units vary in previous work by others. For example, Table 4-3 below provides the estimated thickness of the 180-Foot Aquifer suggested by the work of previous investigators. The information summarized in the Table 4-3 below indicates that identifying the elevation range and thickness of the 180-Foot Aquifer varies and depends on the specific investigator and location.



² See Section 4.6.4

Table 4-3. Previous Estimates of Thickness and Elevation Ranges for the 180-Foot Aquifer

Previous Investigator	180-Foot Aquifer Near CEMEX				
rievious ilivestigatoi	Thickness (ft)	Elevation Range (ft amsl)			
Greene, 1970	50-250	20 to -220			
DWR, 1973	50-150	0 to -300			
Tinsley, 1975	100-150	Base of aquifer at -150			
Staal, Gardner, Dunne*, 1991	Not reported	Top of aquifer at -110			
Fugro West, 1996*	Not reported	Top of aquifer at -135			
Harding ESE, 2001	Combines Dune Sand with 180-Foot Aquifer	Base of aquifer at -250			
Kennedy Jenks, 2004	100	-100 to -180			

^{*} The depth to the 180-Foot Aguifer was determined for a site south of CEMEX.

4.6.1 900-Foot Aquifer

The 900-Foot Aquifer is contained within the Plio-Pleistocene Paso Robles Formation. HLA (2001) notes that the 900-Foot Aquifer is part of a "Deep" aquifer system, which also includes what has been called the 800-Foot, 1,000-Foot, and 1,500-Foot Aquifers. For purposes of groundwater modeling, these aquifers will be collectively termed and simulated as the 900-Foot Aquifer.

4.6.2 400-Foot Aquifer

Within the project area, the 400-Foot Aquifer is the aquifer unit which is contained in the upper and lower portions of the Aromas Sand (USGS, 2003). The thickness of the unit has been reported to be approximately 200 ft (HLA, 2001) but may be as thick as 500 feet (USGS, 2003). The unit is separated from the overlying 180-Foot Aquifer by zones of discontinuous aquifers and aquitards which are approximately 10 to 70 ft thick. The aquitards in this area have been designated as the 180/400-Foot Aquitard.

4.6.3 180-Foot Aquifer

As noted previously, the 180-Foot Aquifer has various reported thicknesses. The aquifer is separated from the overlying Perched "A" Aquifer by the SVA. DWR (2003) states that the 180-Foot Aquifer may, in part, be correlative to older portions of Quaternary Terrace Deposits or the upper Aromas Sand. Work completed for this study suggests that the 180-Foot Aquifer is correlative with terrace deposits of Quaternary age that are older but in erosional contact with younger Salinas River fluvial deposits containing the 180-Foot Aquifer in the Salinas Valley.



According to Tinsley (1975), "extrapolation of the stratigraphic position of the 180-Foot Aquifer offshore shows that it lies within the seismic unit which represents the deltaic deposits" reported by Greene in 1970. The work prepared by Greene suggested approximately 200 ft (60m) to 280 ft (85m) (maximum) thickness of the Holocene deltaic deposits. Tinsley (1975) reported that foraminera⁵ from data collected from the water well cuttings suggested that there is 200 ft (60m) to 250 ft (75m) of Holocene sediments near the coast in the southern Salinas River Valley, which correlates well with the work by Greene. However, more recent work by Chin (USGS, 1988) using seismic methods suggests that the offshore Holocene Deltaic deposits are about 70 ft in thickness.

4.6.3.1 Historical Approaches for Identifying the 180-Foot Aquifer

The 180-Foot Aquifer has been historically defined using four separate approaches. The four approaches are: tradition, facies, groundwater flow system, and institutional. A brief description of the approaches applied to water bearing deposits encountered below the Dune Sand at CEMEX is provided below.

Tradition: Traditionally, the 180-Foot Aquifer has been described in narrative, map, and cross-sectional formats. While the descriptions differ among various authors, generally the 180-Foot Aquifer is described as resting beneath the SVA at an average depth of 180 ft bgs, extending offshore, and cropping out on the floor of Monterey Bay. The mapping of seawater intrusion by the MCWRA represents an implied extent of the traditional 180-Foot and 400-Foot Aquifers. At CEMEX, the terrace deposits which underlie dune sand are not capped by the SVA and therefore do not match the traditional description of the 180-Foot Aquifer.

Facies: Some authors have defined the 180-Foot Aquifer in terms of facies. According to Reading (1996) "a facies is a distinctive rock unit that forms under certain conditions of sedimentation, reflecting a particular process or environment." Authors who have described the 180-Foot Aquifer as a sedimentary facies have associated the 180-Foot Aquifer with Salinas River fluvial deposits which were deposited in the pre-Holocene Salinas Valley. Some authors have extended the 180-Foot Aquifer across facies changes.

A "facies change" is a lateral or vertical variation in lithologic or paleontologic characteristics of contemporaneous sedimentary deposits. It is caused by, or reflects, a change in depositional environment" (Neuendorf et al., 2005). For example, in a fluvial system, the center of a river channel may contain sand and gravel while the edges of the river may contain silt and clay deposited in quiet water conditions. A facies change, or change in the sedimentary environment, occurs within the same

⁵ Foraminifera (foraminifers or, informally, just forams) are single-celled organisms (amoeboid protists) with shells (plankton).



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time-stratigraphic unit. Therefore, including various facies changes in the 180-Foot Aquifer is appropriate. The terrace deposits which underlie the CEMEX property are not a facies change within the fluvial sediments which contain the 180-Foot Aquifer since they represent a different time-stratigraphic unit. The terrace deposits are older and are in erosional contact within the various fluvial facies which contain the 180-Foot Aquifer.

Groundwater-flow system: Under pre-development conditions, groundwater flowed horizontally toward Monterey Bay both within the Salinas Valley and within the Dune Highland area in the vicinity of CEMEX. Under post-development conditions, a reversal in groundwater gradient has resulted in groundwater flowing from Monterey Bay inland, causing seawater intrusion. The groundwater flow systems will cross different facies as well as different time-stratigraphic units. The terrace deposits are likely in hydraulic continuity with the 180-Foot Aquifer. Therefore, groundwater flow will occur across the erosional contact from the 180-Foot Aquifer into the terrace deposits (referred to here as the 180-Foot Equivalent Aquifer, or 180-FTE Aquifer) and vice-versa. The degree of flow between the aquifers will be assessed during the test slant well program.

Institutional: The boundaries of the 180-Foot Aquifer may be defined or implied by legislation or ordinances. It is duly recognized that institutional boundaries have been prepared based on the historical conceptual models of the regional hydrogeology and based on the historical data available. For purposes of this document, the alluvial materials encountered near the coast (in the CEMEX area) are based solely on analyses of borehole samples (and geophysical borehole logs). As of yet, no direct correlation can be made between these coastal alluvial deposits and the standard naming convention found further inland (e.g., 180-Foot Aquifer, 400-Foot Aquifer, SVA, etc.). Therefore, in this document, the upper materials have been classified as the Dune Sand Aquifer and the alluvial materials below have been referred to as stratigraphically equivalent to the inland 180-Foot Aquifer (or 180-FTE Aquifer) and should not be construed to alter institutional interpretations.

4.6.4 180-Foot Equivalent Aquifer (Terrace Deposits)

The terrace deposits are water bearing materials beneath the Dune Sand Aquifer in the CEMEX area. The terrace deposits are approximately 160 ft thick at the CEMEX site, thinning seaward. Hydraulic conductivity values are lower than those attributed to the 180-Foot Aquifer. Based on the data collected in this study, the terrace deposits are interpreted to be stratigraphically equivalent to the 180-Foot Aquifer of the Salinas Valley, and may likely be in hydraulic continuity with the 180-Foot Aquifer. Therefore, for the purposes of this investigation, the aquifer interval within the terrace deposits is referred to as 180-Foot Equivalent (180-FTE) Aquifer. The 180-FTE Aquifer is believed to be in hydraulic continuity with the overlying Dune Sand Aquifer; both units extend seaward beneath Monterey Bay and have similar water quality.



4.6.5 Salinas Valley Aquitard

The SVA consists of discontinuous layers of clays ranging in thickness from 0 to 100 ft. It defines the Pressure Area from Chualar to the coast. In the inland areas, the SVA is generally present overlying the 180-Foot Aquifer, separating the 180-Foot Aquifer from the Perched "A" Aquifer (discussed below). The SVA is present beneath the Moss Landing area but not beneath the CEMEX site.

4.6.6 Dune Sand Aquifer

The Dune Sand Aquifer is present beneath the CEMEX site and represents the water bearing units of both the Younger and Older Dune Sand. Based on groundwater quality data collected at the CEMEX site, and the absence of the SVA, the groundwater in the Dune Sand Aquifer is believed to be hydraulically connected to the underlying 180-FTE Aquifer (terrace deposits). The high salinity suggests that the Dune Sand Aquifer is also connected to the ocean. According to HLA (2001), the Dune Sand Aquifer is hydrostratigraphically equivalent to the Perched "A" Aquifer. Work completed by Emcon (1991) for the Marina Peninsula Class III Landfill suggests that there are multiple perched aquifers within the Older Dune Sand. The aquifer designated as the -2 Foot Aquifer at the landfill appears to correlate with the Perched "A" Aquifer of the Salinas Valley. Recent groundwater levels for the -2 Foot Aquifer are shown on Cross-Section 1-1' (Figure 7a).

4.6.7 Perched "A" Aquifer

The Perched "A" Aquifer is found within the Salinas Valley overlying the SVA. According to HLA (2001), an equivalent unit designated as the "A-aquifer" is found exclusively in the Older Dune Sand beneath the former Fort Ord. This relationship further suggests that groundwater within the Perched "A" Aquifer in the Salinas Valley may be hydraulically connected to the groundwater found in the Older Dune Sand.

4.7 Hydrostratigraphic Interpretation of CEMEX Borehole Data

The CEMEX borings encountered groundwater from slightly below ground surface to the bottom of each borehole. The Dune Sand Aquifer is present to a depth of approximately 90 ft bgs. Groundwater quality data indicates that TDS concentrations for the Dune Sand Aquifer range from approximately 4,800 mg/L inland to 27,000 mg/L near the ocean.

Terrace deposits in the 180-FTE Aquifer underlie the Dune Sand Aquifer and consist of a range of fluvial lithologic units, including thin gravel channels and laminated silt and very fine sand deposits. The base of the terrace deposits appears to be marked by a transition to thicker clay units (10-15 ft thick) with interbedded sand and gravel units (about 10-ft thick) above a distinct "blue" clay layer. TDS concentrations in this unit vary from 16,000 mg/L to near sea water (32,000 mg/L). TDS concentrations



in the terrace deposits appear to be similar to those in the Dune Sand Aquifer. The high and low values of TDS appear to represent groundwater within more isolated channels and lenses within the unit.

The units below the "blue" clay⁶ are interpreted to be the 400-Foot Aquifer within the Aromas Sand. TDS concentrations obtained from two isolated zones in this aquifer were approximately 25,000 mg/L to 30,000 mg/L. Table 4-4 below provides a summary of water quality by geologic unit. The TDS concentrations with depth and by geologic unit are shown on Figures 7a and 7b. A detailed discussion of groundwater quality is provided in Section 5.

Table 4-4. Summary of Laboratory Water Quality Results from Boreholes at CEMEX

TDS Concentrations by		Borehole CX-B1 WQ					
Zone	Zone 1	Zone 2	Zone 3	Zone 4	Zone 5	Zone 6	
Depth (ft bgs)	274-284	237-247	182-192	134-144	84-94	51-61	
TDS (mg/L)	25,200	14,600	35,600	26,500	27,400	24,800	
TDS Concentrations by		ı	Borehole C	K-B2 WQ			
Zone	Zone 1	Zone 2	Zone 3	Zone 4			
Depth (ft bgs)	215-225	160.5-170.5	104-114	55-65			
TDS (mg/L)	26,500	16,200	26,800	26,700			
TDS Concentrations by	Borehole CX-B4						
Zone	Zone 1	Zone 2	Zone 3	Zone 4	Zone 5		
Depth (ft bgs)	306-316	248-258	155-165	110-120	58-68		
TDS (mg/L)	29,800	27,200	20,500	24,000	4,815		

4.8 Hydrostratigraphic Interpretation of Moss Landing Boreholes Data

A total of seven borings were drilled in the Moss Landing study area. Figure 8 and Figure 9 are geologic cross-sections constructed from borehole data, and were used to interpret the subsurface stratigraphic and hydrostratigraphic relationships in the Moss Landing area. Cross-Section 2-2' is drawn perpendicular to the shoreline and makes use of the lithologic log from Boring PR-1 and mapped surface geology. The geologic relationships depicted include recent alluvium and older alluvium containing the

⁶ The "blue clay" refers to a distinct lithologic unit encountered in CEMEX borings that was dark greenish gray, a Munsell color of 5GY 3/1. Munsell soil color charts are commonly used in the industry to describe soil colors.



Perched "A" Aquifer, SVA, and the 180-Foot Aquifer present beneath the Salinas River in erosional contact with older alluvial fan deposits located on the northern portion of the Salinas Valley. This relationship was reported by Tinsley (1975) for the area around Salinas and indicates that the aquifers in the Salinas Valley may be in hydraulic connection with groundwater in terrace and alluvial fan deposits. The older alluvial deposits and alluvial fan deposits overlie the Aromas Sand which contains the 400-Foot Aquifer.

Cross-Section 3-3' is drawn parallel to the shoreline and extends from Moss Landing south to the City of Marina. Cross Section 3-3' makes use of the lithologic logs from Boreholes MDW-1, PR-1, ML-1, ML-2, and ML-6. Further south, borehole information from previous studies and driller's logs and data recently collected from CEMEX were used to construct the cross-section. The cross-section depicts a thicker sequence of recent alluvium consisting of permeable sand and gravel material present at depths between 58 ft and 139 ft bgs in PR-1. In the Moss Landing area, the recent alluvium is interbedded with silt, silty sand, and clay. To the south of Boring PR-1, the permeable deposits encountered in Boring PR-1 decrease in thickness and pinch out and the Older Alluvium which contains the SVA and the 180-Foot Aquifer is in erosional contact with the terrace deposits. The alluvial deposits are channel and floodplain deposits near the mouth of the Salinas River. The alluvium is underlain by older alluvium which contains the SVA, and the underlying 180-Foot Aquifer. The 180-Foot Aquifer is cut off to the north by clay gorge fill reported by DWR (1973) associated with Elkhorn Slough.

Table 4-5 below summarizes basic groundwater quality data for the Moss Landing borings. The zones above approximately 100 ft bgs had TDS concentrations ranging from freshwater (423 mg/L) to near seawater (29,000 mg/L). Borings ML-2, ML-3 ML-4 contained brackish water (approximately 5,000 mg/L to 9,000 mg/L). With the exception of Zone 1 from ML-3, the lower zones consistently contained high TDS concentrations ranging from approximately 19,000 mg/L to 34,000 mg/L (ML-6). A detailed discussion of groundwater quality is provided in Section 5.



Table 4-5. Summary of Laboratory Water Quality Results from the Moss Landing Borings

Water		MDW-1		PR-1		1	ML-1	
Quality Parameters	Zone 1	Zone 2	Zone 3	Zone 4	Zone 1	Zone 2	Zone 1	Zone 2
Depth (ft bgs)	237-247	187-197	152-162	60-70	190-200	125-135	113.5-118.5	90-100
TDS (mg/L)	31,000	30,200	26,600	21,900	630	34,000	22,000	3,200
Water	MI	L-2	MI	L-3	ML-4		ML-6	
Quality								
Parameters	Zone 1	Zone 2	Zone 1	Zone 2	Zone 1	Zone 2	Zone 1	Zone 2
Parameters Depth (ft bgs)	Zone 1 167-177	Zone 2 90-100	Zone 1 180-190	Zone 2 103-113	Zone 1 163.5-173.5	Zone 2 74.5-84.5	Zone 1 152-162	Zone 2 100-110

4.9 Updated Conceptual Model

The geologic and hydrogeologic data collected during this investigation was used to prepare the interpretations of hydrostratigraphic relationships in the Moss Landing and CEMEX areas. A conceptual model of the hydrostratigraphic units in the Moss Landing to CEMEX area as interpreted from data collected from this investigation is shown on Figure 4-2.



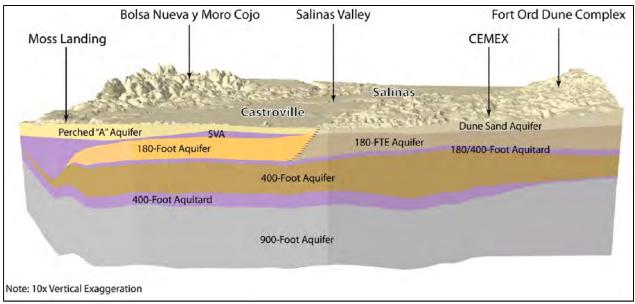


Figure 4-2. Hydrostratigraphic Model Moss Landing to CEMEX Area



5.0 GROUNDWATER QUALITY

5.1 General

5.1.1 Groundwater Levels

Groundwater was encountered in all of the borings drilled during this investigation. Groundwater levels were not established with certainty during this investigation. The groundwater level was measured in the well casing after aquifer zone testing if the zone was left over night to allow full recovery after pumping. In some cases, the zones were removed at the end of pumping to allow for construction of a subsequent zone or for borehole destruction to move the drilling rig to the next location. The installation of permanent monitoring wells during the next phase of investigation will allow an accurate evaluation of groundwater elevations. Table 5-1 below provides groundwater level measurements (depth in ft, bgs) from most of the zones. These are provided as an estimate of depth to water encountered in the temporary well (zone) but may vary with tidal influences or seasonally. In general, the depth to water measured in the boreholes reflects a groundwater surface elevation at or near sea level.

Table 5-1. Depth to Water from Isolated Aquifer Test Zones

		Depth	to Water	(ft bgs)			
Borehole	Zone 1	Zone 2	Zone 3	Zone 4	Zone 5	Zone 6	
Moss Landing							
PR-1	-	-					
ML-1		3.6					
ML-2	3.3	1.6					
ML-3	12.57	10.86					
ML-4	28.68						
ML-6	8.09	9.58					
MDW-1	20.8	19.2	20.9	14.65			
CEMEX							
CX-B1WQ	26		19.53	21.5	19.3	19.9	
CX-B2WQ	28.4	26.31	24.3	24.7			

5.1.2 Groundwater Sampling and Analysis

Groundwater samples collected from the isolated aquifer zone tests were submitted for laboratory analysis. Table 5-2 lists the suite of analyses conducted on each sample. The results of the water quality and age dating analyses will partially form the basis for the interpretations of the hydrogeology in the study area discussed in the sections below. The laboratory analytical data are summarized in Table 3a



and Table 3b. Copies of the field data sheets used to record field parameters during zone testing are provided in Appendix G.

Table 5-2. Water Quality Analyses for Exploratory Boreholes

Constituent	Units	Method Reporting Limit	Method
Physical Properties			
Color	Color Units	3	SM 2120B/EPA 110.2
Odor	T.O.N.		EPA 140.1
Oxidation-Reduction Potential (Field)	mV	-	Field Meter - Myron L 6PII
pH (Lab)	Units	0.1	SM 4500 H+B
pH (Field)	Units	-	Field Meter - YSI Pro Plus
Turbidity (Laboratory)	NTU	0.2	EPA 180.1/SM 2130B
Turbidity (Field)	NTU	-	Field Meter - Hach 2100P
Temperature (Field)	°C	-	Field Meter - YSI Pro Plus
Dissolved Oxygen (Field)	mg/L	-	Field Meter - YSI Pro Plus
Silt Density Index (Field)	-	-	ASTM D4189-07
Threshold Odor Number	T.O.N.	1	EPA 140.1/SM 2150
Total Dissolved Solids (Lab)	mg/L	10	SM 2540 C
Total Dissolved Solids (Field)	mg/L	-	Field Meter - YSI Pro Plus
Specific Conductance (Lab)	μmhos/cm	1	SM 2510 B
Specific Conductance (Field)	μS/cm	-	Field Meter - YSI Pro Plus
General Minerals			
Total Cations	meq/L	-	Calculation
Total Anions	meq/L	-	Calculation
Alkalinity as CaCO ₃	mg/L	3	SM 2320 B
Bicarbonate Alkalinity as HCO ₃	mg/L	3	SM 2320 B
Carbonate Alkalinity as CaCO ₃	mg/L	3	SM 2320 B
Hydroxide Alkalinity as CaCO ₃	mg/L	3	SM 2320 B
Total Hardness as CaCO ₃	mg/L	3	Calculation
Aluminum	μg/L	1	EPA 200.7
Arsenic	μg/L	1	EPA 200.7 / EPA 200.8
Barium, Dissolved	μg/L	0.01	EPA 200.7
Boron, Dissolved	μg/L	0.5	EPA 200.8



Calcium, Dissolved mg/L 1 EPA 200.7 Chloride, Dissolved mg/L 1 EPA 300.0 Copper, Total μg/L 50 EPA 200.7 Fluoride, Dissolved mg/L 0.1 EPA 300.0 / SM 4500 FC Iodide, Dissolved μg/L 100 EPA 200.7 / EPA 200.8 Iron, Dissolved μg/L 100 EPA 200.7 / EPA 200.8 Iron, Total μg/L 10 EPA 200.7 / EPA 200.8 Ithium μg/L 10 EPA 200.7 / EPA 60108 Magnesium, Dissolved mg/L 1 EPA 200.7 / EPA 200.8 Manganese, Dissolved μg/L 20 EPA 200.7 / EPA 60108 Manganese, Dissolved μg/L 20 EPA 200.7 / EPA 200.8 Manganese, Dissolved μg/L 20 EPA 200.7 / EPA 200.8 Manganese, Dissolved mg/L 1 EPA 200.7 / EPA 200.8 Manganese, Dissolved mg/L 1 EPA 303.2 / EPA 200.8 Mitrogen, Nitrate as NO ₃ mg/L 1 EPA 353.2 / EPA 300.0 Nitrogen, Nitrate as No ₃		/-	0.4	504 00C 0
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$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	Phosphorus, ortho, Dissolved	mg/L as P	0.01	EPA 365.3
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$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	Silica, Dissolved	mg/L	1	SM 4500 SiE
Sulfate as SO_4 , dissolved mg/L 0.5 EPA 300.0 Zinc, Total μ g/L 50 EPA 200.7 **Radiology / Age Dating Methods** Delta-Deuterium δ^2 H - TC/EA/IRMS Delta Oxygen-18 δ^{18} O - TC/EA/IRMS Tritium TU Tritium, prec. est. TU **Volatile Organic Compounds** VOCs plus Oxygenates (MTBE) μ g/L varies EPA 524.2 **EPA Organic Methods** EDB and DBCP μ g/L varies EPA 504.1 Chlorinated Pesticides & PCB's as DCP μ g/L varies EPA 508 Chlorinated Acid Herbicides μ g/L varies EPA 515 Nitrogen & Phosphorus Pesticides DEHP, μ g/L varies EPA 525	Sodium, Dissolved	mg/L	1	EPA 200.7
Zinc, Total $\mu g/L$ 50 EPA 200.7 **Radiology / Age Dating Methods** Delta-Deuterium $\delta^2 H$ - TC/EA/IRMS Delta Oxygen-18 $\delta^{18}O$ - TC/EA/IRMS Tritium TU Tritium, prec. est. TU **Volatile Organic Compounds** VOCs plus Oxygenates (MTBE) $\mu g/L$ varies EPA 524.2 **EPA Organic Methods** EDB and DBCP $\mu g/L$ varies EPA 504.1 Chlorinated Pesticides & PCB's as DCP $\mu g/L$ varies EPA 508 Chlorinated Acid Herbicides $\mu g/L$ varies EPA 515 Nitrogen & Phosphorus Pesticides DEHP, $\mu g/L$ varies EPA 525	Strontium, Dissolved	mg/L	0.1	EPA 200.7 / EPA 200.8
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Sulfate as SO ₄ , dissolved	mg/L	0.5	EPA 300.0
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Zinc, Total	μg/L	50	EPA 200.7
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Tritium, prec. est. TU Volatile Organic Compounds VOCs plus Oxygenates (MTBE) μg/L varies EPA 524.2 EPA Organic Methods EDB and DBCP μg/L varies EPA 504.1 Chlorinated Pesticides & PCB's as DCP μg/L varies EPA 508 Chlorinated Acid Herbicides μg/L varies EPA 515 Nitrogen & Phosphorus Pesticides DEHP, μg/L varies EPA 525	Delta Oxygen-18	δ^{18} O	-	TC/EA/IRMS
$\begin{tabular}{cccccccccccccccccccccccccccccccccccc$	Tritium	TU	-	-
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	Volatile Organic Compounds			
	VOCs plus Oxygenates (MTBE)	μg/L	varies	EPA 524.2
Chlorinated Pesticides & PCB's as DCP μ g/L varies EPA 508 Chlorinated Acid Herbicides μ g/L varies EPA 515 Nitrogen & Phosphorus Pesticides DEHP, μ g/L varies EPA 525	EPA Organic Methods			
Chlorinated Pesticides & PCB's as DCP μ g/L varies EPA 508 Chlorinated Acid Herbicides μ g/L varies EPA 515 Nitrogen & Phosphorus Pesticides DEHP, μ g/L varies EPA 525		μg/L	varies	EPA 504.1
$ \begin{array}{cccc} \text{Chlorinated Acid Herbicides} & \mu g/L & \text{varies} & \text{EPA 515} \\ \text{Nitrogen \& Phosphorus Pesticides DEHP,} & \mu g/L & \text{varies} & \text{EPA 525} \\ \end{array} $	Chlorinated Pesticides & PCB's as DCP		varies	EPA 508
Nitrogen & Phosphorus Pesticides DEHP, µg/L varies EPA 525	Chlorinated Acid Herbicides		varies	EPA 515
	DEHA, Benzo(a)Pyrene			



Carbamates	μg/L	varies	EPA 531.1
Glyphosate	μg/L	varies	EPA 547
Endothall	μg/L	varies	EPA 548.1
Diquat	μg/L	varies	EPA 549.1
Dioxin (2,3,7,8 TCDD)	μg/L	varies	EPA 1613

NTU = Nephelometric Turbidity Units

mg = Milligram μS = Microsiemens

Due to time constraints, the need to work through weekends, and the need to submit samples to laboratories on the weekend, several laboratories were used for the analytical work. In addition, specialist laboratories were used for age dating using the tritium and oxygen/deuterium isotope analyses. The following are the State Certified Laboratories and specialist laboratories used for analytical testing.

- BSK Associates
- Ceres Analytical Laboratory
- Maxxam Analytics
- Monterey Bay Analytical Services
- Pace Analytical
- SIRFER Stable Isotope Ratio Facility for Environmental Research (University of Utah)
- Weck Laboratories, Inc.
- GEOCHRON Laboratories
- McCampbell Analytical, Inc.

5.2 Groundwater Quality - CEMEX Area

Lithologic, geophysical, and groundwater quality data was collected from borings drilled at the CEMEX facility. The geologic data and geophysical data were used with other published data and driller's logs to construct Cross-Section 1-1' (see Figures 7a and 7b). The cross-section extends from offshore, eastward, through the CEMEX facility and the Monterey Peninsula Landfill into the Salinas Valley. The stratigraphic relationships indicate that groundwater aquifers beneath the CEMEX facility are present in the Younger and Older Dune Sand, in terrace deposits below the Dune Sand, and in what is interpreted as Aromas Sand (?) below the terrace deposits. The terrace deposits are separated from the underlying Aromas Sand (?) by a distinct "blue" clay unit which suggests a change in depositional environment at an elevation of approximately -220 ft amsl. The groundwater present in the terrace deposits appears to be hydrostratigraphically equivalent to the 180-Foot Aquifer is therefore termed 180-FTE Aquifer to be consistent with the nomenclature used in this region. As interpreted, the 180-FTE Aquifer transitions



eastward and is in erosional contact with the older alluvium (which contains the 180-Foot Aquifer) in the Salinas Valley. The sedimentary transition eastward towards the Salinas Valley is shown in Figure 7a. The 180-FTE and 180-Foot Aquifers, although depositionally and chronologically different, are hydrostratigraphically equivalent. The degree of hydrostratigraphic equivalence will be evaluated by the long-term test slant well aquifer testing program.

Table 5-3 summarizes TDS concentrations by depth and interpreted hydrostratigraphic unit at CEMEX. TDS concentrations in the Dune Sand Aquifer range from approximately 28,000 mg/L near the shore to approximately 4,800 mg/L inland in the vicinity of the CEMEX Office (see Figure 3).

Table 5-3 Summary of Water Quality by Hydrostratigraphic Unit-CEMEX

Hydrostratigraphic	CX-B1WQ				CX-B2WQ			CX-B4		
Unit						TDS				
51t	Zone	Depth(ft, bgs)	TDS (mg/L)	Zone	Depth(ft, bgs)	(mg/L)	Zone	Depth(ft, bgs)	TDS (mg/L)	
Dune Sand Aguifer	6	51-61	24,452	4	55-65	26,700	5	58-68	4,815	
Dune Sand Aquiter	5	84-94	28,111							
180-FTE	4	134-144	26,921	3	104-114	26,800	4	110-120	24,000	
100-FTL	3	182-192	32,034	2	160.5-170.5	16,200	3	155-165	20,500	
180-400-Aquitard (?)	2	237-247	16,122							
400 ET Aquifor	1	274-284	24,888	1	215-225	26,500	2	248-258	27,200	
400-FT Aquifer							1	306-316	29,800	

This condition indicates that the Dune Sand Aquifer is directly influenced by the ocean. This influence decreases inland where the infiltration of precipitation and applied agricultural water provide the greater influence.

Groundwater in the 180-FTE Aquifer ranges in TDS concentration, from approximately 16,000 mg/L to approximately 32,000 mg/L. The TDS concentration is generally consistent from the near shore area to the inland area near the CEMEX office. This condition indicates that surface water does not influence the TDS concentration and that the groundwater is influenced by seawater intrusion. The old CEMEX well was reportedly screened in the 180-FTE Aquifer and was abandoned due to high TDS content. However, the driller's log shows that the well was perforated from 246 to 506 ft bgs, which would have placed the perforations in the 400-Foot Aquifer based on the current interpretation. Similar TDS concentrations in the Dune Sand Aquifer within at least 1,500 ft of the shore and the underlying 180-FTE Aquifer, suggest that the two aquifers are in hydraulic connection. In addition, the range of TDS concentrations in the lower portion of the 180-FTE Aquifer suggests that groundwater is present in sediment lenses that may be more isolated from each other and potentially locally isolated from the overlying aquifers.



The Dune Sand Aquifer and upper portion of the 180-FTE Aquifer contain groundwater that is enriched in calcium and strontium, suggesting that geochemical transformation from seawater intrusion has impacted the groundwater in approximately the upper 200 ft. The tritium analysis for samples from CX-B1WQ and CX-B2WQ is discussed in Section 5.8 and indicates that groundwater in the Dune Sand Aquifer is youngest, which is consistent with influence from rainfall and irrigation. The groundwater in the upper portion of the 180-FTE Aquifer may be slightly older and apparently has not had time for geochemical processes from seawater intrusion to impact the quality. The complete age dating analysis will be provided as an addendum to this technical memorandum.

The Dune Sand Aquifer extends seaward and merges with Holocene deltaic deposits beneath the seafloor of Monterey Bay. The base of the terrace deposits in the 180-FTE Aquifer also extend seaward and are unconformably overlain by the Holocene Deltaic deposits at an elevation of approximately -220 ft amsl.

5.3 Groundwater Quality - Moss Landing Area

The Moss Landing area is located at the mouth of the Salinas River, which overlies the 180/400-Foot Aquifer Subbasin. The six exploratory borings primarily penetrated fluvial sediments associated with Holocene Salinas River deposition.

The Perched "A" Aquifer is ascribed to the Holocene river alluvium and considered to be the hydrostratigraphic equivalent of the Dune Sand Aquifer located to the south. The Perched "A" Aquifer in the Moss Landing area is composed of interbedded river and floodplain deposits. With the exception of the sediments penetrated in Boring PR-1, individual sand and sand and gravel lenses do not appear to be either vertically or areally extensive. Significant variations in TDS concentrations suggest that fresh groundwater is mixed with seawater, and is likely present in semi-isolated lenticular deposits.

Table 5-4 provides a summary of TDS concentrations by hydrostratigraphic unit in the Moss Landing area. TDS concentrations in the Perched "A" Aquifer appear to be influenced by fresh or brackish water in the Moss Landing Harbor area, as indicated by TDS concentrations ranging from 3,200 mg/L to 8,600 mg/L in Borings ML-1, Ml-2, ML-3 and ML-4 located near waterways. Groundwater samples from Borings MDW-1, PR-1 and ML-6 were at near seawater quality, reflecting proximity to the ocean.

Boring PR-1 penetrated a very permeable unit in the Perched "A" Aquifer between 58 ft to 139 ft bgs. Groundwater in this zone interval approximated seawater quality (i.e., 34,000 mg/L TDS). It is interpreted that the lowest portion of Boring PR-1 penetrated the SVA. Very low TDS concentrations (630 mg/L) encountered in the lowest zone in Boring PR-1 suggests that isolated zones of freshwater



may exist within the 180-Foot Aquifer or that the sand unit is laterally discontinuous and may be interbedded with the SVA. In this last interpretation, Boring PR-1 did not completely penetrate the SVA.

Table 5-4. Summary of Water Quality by Hydrostratigraphic Unit- Moss Landing

Hydrostratigraphic		MDW-1			PR-1			ML-1	
Unit			TDS			TDS			TDS
Offic	Zone	Depth(ft, bgs)	(mg/L)	Zone	Depth(ft, bgs)	(mg/L)	Zone	Depth(ft, bgs)	(mg/L)
	4	60-70	21,900						
Perched A Aquifer				2	125-135	34,000	2	90-100	3,200
							1	113.5-118.5	22,000
	3	152-162	26,600						
180-FT Aquifer	2	187-197	30,200						
	1	237-247	31,000	1	190-200	630*			

Hydrostratigraphic	ML-2				ML-3			ML-4			ML-6	
Unit			TDS			TDS			TDS			TDS
Offic	Zone	Depth(ft, bgs)	(mg/L)									
Danahad A Assifan	2	90-100	8,100	2	103-113	4,200	2	74.5-84.5	8,600	2	100-110	28,000
Perched A Aquifer	1	167-177	19,000	1	189-190	7,400	1	163.5-173.5	21,000	1	152-162	34,000

^{*}Groundwater from Zone of PR-1 may be contained in an isolated zone within the SVA

Boring MDW-1 penetrated the 180-Foot Aquifer. Groundwater collected from three depth intervals within the 180-Foot Aquifer had TDS concentrations close to seawater.

5.4 Determining Average Central California Coast Seawater Quality

Average salinity estimates for the central California coastal region were established based on historical salinity measurements taken at the Granite Canyon monitoring station operated by the Moss Landing Marine Laboratory (Shore Stations Monitoring Program, 2014). Daily salinity measurements were made based on samples collected near the intake for the Marine Pollution Studies Laboratory. An average 33.69 Practical Salinity Units (PSU) salinity was calculated from the Granite Canyon monitoring data based on the average of daily salinity measurements from January 1986 through January 2011.

The composition of major chemical constituents in central California coastal seawater was then calculated from the major chemical constituent concentrations in standard seawater (JGOFS, 1997) multiplied by the ratio of the average local salinity (approximately 33.69) to standard seawater salinity (approximately 35.17). Standard seawater composition and average central California coastal seawater composition is listed in Table 5-5.



Table 5-5. Standard Seawater and Central California Coast Seawater

Parameter	Units	Mean Seawater Values	Central California Coast Average Seawater Values **
Total Dissolved Solids	mg/L	35,176	33,694
Salinity	PSU*	35.17	33.69
Potassium	mg/L	399	382
Sodium	mg/L	10,784	10,329
Magnesium	mg/L	1,284	1,230
Calcium	mg/L	412	395
Strontium	mg/L	7.9	7.57
Bicarbonate	mg/L	108	103
Chloride	mg/L	19,352	18,537
Fluoride	mg/L	1.3	1.25
Sulfate	mg/L	2,712	2,598
Total Boron	mg/L	4.55	4.35
Bromide	mg/L	67.3	64.5

^{*} PSU = Practical Salinity Unit

5.5 Borehole Water Quality Results

Table 5-6 lists the boreholes where water quality samples were collected and the corresponding depth intervals, measured TDS, and calculated TDS. Complete water quality analysis from borehole testing is included in Appendix G. Measured TDS values listed in Table 5-6 were determined using Standard Method 2540, and the calculated TDS values were determined from the water quality analysis for each borehole. Calculated water quality included bicarbonate and all other major and minor ions. Trilinear groundwater plots for the water quality data from CEMEX borings (Boring CX-B1WQ, CX-B2WQ, and CX-B4) are presented on Figure 10. Trilinear groundwater plots for the water quality data from the Moss Landing borings (ML-1, ML-2, ML-3, ML-4, ML-6, PR-1, and MDW-1) are presented on Figure 11. The water quality from the CEMEX borings and the Moss Landing borings plot similarly, suggesting a common source water.



^{**} Ocean water composition calculated from mean salinities measured at the Granite Canyon Monitoring Station by Moss Landing Marine Laboratories. Average Salinity based on 1988 – 2011 monitoring data.

Table 5-6. Comparison of Measured TDS and Calculated TDS for Borehole Water Quality Samples

Zone	Depth Interval (ft)	Measured Total Dissolved Solids mg/L	Calculated Total Dissolved Solids mg/L	Agreement Between Calculated and Measured TDS % Difference
CEMEX Boreholes				
CX-B1WQ-1	274-284	25,200	24,606	-2.4%
CX-B1WQ-2	237-247	14,600	15,177	3.8%
CX-B1WQ-3	182-192	35,600	32,719	-8.8%
CX-B1WQ-4	134-144	26,500	25,547	-3.7%
CX-B1WQ-5	84-94	27,400	26,458	-3.6%
CX-B1WQ-6	51-61	24,800	23,663	-4.8%
CX-B2WQ-1	215 - 225	26,500	23,041	-15.0%
CX-B2WQ-2	161 - 171	16,200	12,599	-28.6%
CX-B2WQ-3	104 - 114	26,800	24,790	-8.1%
CX-B2WQ-4	55 - 65	26,700	25,153	-6.2%
CX-B4-1	306 - 316	29,800	25,130	-18.6%
CX-B4-2	248 - 258	27,200	25,072	-8.5%
CX-B4-3	155 - 165	20,500	18,293	-12.1%
CX-B4-4	110 - 120	24,000	19,744	-21.6%
CX-B4-5	58 - 68	4,815	3,884	-24.0%
Moss Landing Bore	eholes			
ML-1-1	113.5-123.5	22,000	21,399	-2.8%
ML-1-2	90-100	3,200	3,094	-3.4%
ML-2-1	167-177	19,000	21,870	13.1%
ML-2-2	90-100	8,100	6,872	-17.9%
ML-3-1	180-190	7,400	6,732	-9.9%
ML-3-2	103-113	4,200	4,229	0.7%
ML-4-1	163.5-173.5	21,000	18,542	-13.3%
ML-4-2	74.5-84.5	8,600	8,002	-7.5%
ML-6-1	152-162	34,000	33,230	-2.3%
ML-6-2	100-110	28,000	28,580	2.0%
PR-1-1	190-200	630	760	17.1%
PR-1-2	125-135	34,000	33,767	-0.7%
MDW-1-1	237 - 247	31,000	28,789	-7.7%
MDW-1-2	187 - 197	30,200	29,778	-1.4%
MDW-1-3	152 - 162	26,600	24,772	-7.4%
MDW-1-4	60 - 70	21,900	20,814	-5.2%

5.6 Distinguishing Water Quality from Upper and Lower Aquifers

One of the objectives of the sampling effort was to determine if water quality measured in the upper aquifers could be distinguished from that in the lower aquifers. Several water quality analytical and age dating methods were used to aid in differentiating the upper aquifers from the lower aquifers. Vengosh (2002) used ratios of calcium, magnesium, and lithium to evaluate the source of increased salinity in the Salinas Valley. The methods employed by Vengosh were applied to the water quality samples collected for this investigation. The results are discussed below.

Groundwater samples collected were analyzed for tritium content for determining relative age as well as oxygen (δ^{18} O) and hydrogen (δ^{2} H) isotopes to evaluate the relative contribution of different source waters. The results of these analyses are discussed in Section 5.8 and 5.7.3, respectively.



5.7 Evaluation of Source Waters

5.7.1 CEMEX Boreholes

Prior work in Salinas Valley and coastal central California by Vengosh (2002) had evaluated the geochemical interactions, which occur when seawater intrudes into inland aquifers. When compared to the local seawater values, shifts in some chemical constituents including calcium, sodium, strontium, and boron occur in intruded seawater. Vengosh reported that intruded seawater had enriched ratios of calcium, magnesium, and lithium when compared to those seen in standard seawater.

Water quality data from CEMEX boreholes were analyzed by comparing chloride ratios of the major ion groups with those of standard seawater for the central California coastal region. Chloride is used as a reference in these comparisons, as it is generally conservative and has not been reported to undergo water/rock exchange reactions. Figures 12 through 18 show the ratios of chloride to TDS, Sodium, Calcium, Sulfate, Bromide, Boron, and Strontium measured at different depths in CEMEX borehole CX-B1WQ, CX-B2WQ-1, and CX-B4-1. The dashed line shown in each figure represents the ratio of chloride to the given ion based on the average ocean water values measured for the central California coast (see Table 5-3).

TDS levels in CX-B1WQ zones 1, 4, 5, and 6 are similar (approximately 23,000 to 26,000 mg/L) whereas Zone 2 is substantially lower (15,177 mg/L) and Zone 3 is substantially higher at 32,700 mg/L (see Table 5-3). The chloride/TDS ratio in all six of the zones measured in CEMEX Borehole CX-B1 generally corresponds to diluted seawater (Figure 12). With the exception of Zone 2, chloride/TDS ratios from CX1-B2WQ are similar and tightly clustered around 25,000 mg/L TDS. Each of the zones sampled in Borehole CX-B4 is consistent with diluted seawater ratios for chloride/TDS over a range of TDS values ranging from approximately 4,000 mg/L in the upper zone to 25,000 mg/L in the two lower zones (Figure 12).

When comparing the relative ratios of chloride/sodium and chloride/calcium for Boreholes CX-B1WQ, CX-B2WQ, and CX-B4, there is a clear departure from the local seawater ratios for most of the borehole zones sampled. Figure 13 shows that sodium is comparably depleted in borehole water samples as the chloride/sodium ratios are generally below the local seawater ratio. The relative depletion in sodium is greater in the lower zone samples of all three boreholes as compared to the upper zones (Figure 13). Chloride/calcium ratios shown on Figure 14 indicate that calcium enrichment has occurred as chloride/calcium ratios are well above the diluted seawater line. The trend in relative calcium enrichment is greater at lower zone and decreases in the upper zones for all three boreholes in the CEMEX area.



Figure 15 shows the relative depletion and enrichment of sodium and calcium in the three CEMEX area boreholes as calculated using the Δ Ca and Δ Na values, which are determined based on the measured and calculated values based on the standard seawater ratio.

Calcium enrichment and sodium depletion was reported by Vengosh in intruded seawater and was attributed to a base-exchange reaction with clay minerals where calcium is exchanged with sodium between the solid and liquid phase. Figure 14 suggests that the shallower zones in Boreholes CX-B1WQ, CX-B2WQ, and CX-B4 have undergone less calcium enrichment and the lowermost zones have seen the highest amount of calcium enrichment relative to diluted seawater.

Figures 16 and 17 show the ratio of chloride/boron and chloride/strontium, respectively in the Cemex area boreholes. The boron and strontium ratios in the upper zones in Borehole CX-B1WQ (Zones 4, 5, and 6) have similar depletion magnitudes (with respect to Boron, Figure 16) and enrichment with respect to Strontium (Figure 17). Boreholes CX-B4 and CX-B2WQ shows a similar trend to that of CX-B1WQ where the lower zones show a greater departure from the seawater dilution line that the upper zones.

In summary, the results from Boreholes CX-B1WQ, CX-B2WQ, and CX-B4 suggest that the water from the shallower zones (above 144 ft) may be distinguished from water from the deeper zones even if they are at the same TDS level. Water from the deepest zone (274-284 ft) shows a marked distinction in the amount of calcium and strontium enrichment, and sodium depletion when compared to shallower zones. The difference in the amount of calcium and strontium enrichment and sodium depletion between the upper zones and lower zones in the CEMEX area boreholes is likely a function of the relative abundance of clay formation materials in the lower formation as well as groundwater age.

5.7.2 Moss Landing Boreholes

Moss Landing water quality analysis is discussed in two general regions; the Moss Landing Harbor area (Borings ML-1, ML-2, ML-3, ML-4, and ML-5) and the area south of Potrero Road (Borings PR-1 and MDW-1). Water quality samples were collected from a shallow and deep zone in each of the five boreholes drilled in the immediate Moss Landing area (ML boreholes). Results from water quality samples in the Moss Landing Area are listed in Table 5-6.

5.7.2.1 Moss Landing Harbor Area

Chloride ratios of the major ions were compared against the average coastal seawater values to determine if water quality from the upper and lower zones could be distinguished from each other.



TDS results for the Moss Landing boreholes show that the deeper zones in Boreholes ML-1, ML 2, and ML-4 have substantially higher TDS levels than the shallow zones. Borehole ML-3 and ML-6 both showed less variation between TDS measured in the upper and lower zones (Table 5 4).

Figure 19 shows the chloride/TDS ratios from water samples collected from the Moss Landing area boreholes. The dashed line on Figure 19 represents the chloride/TDS ratio of average diluted seawater along the central California coast. The TDS/chloride ratios measured in the Moss Landing boreholes are in relatively close agreement with the seawater dilution line, which indicates the water is consistent with intruded seawater, which has been diluted.

Relative sodium depletion and calcium enrichment is shown on Figure 20 and Figure 21. Results indicate that a relative enrichment of calcium and depletion of sodium has occurred, similar to trends seen in the CEMEX area boreholes. Figure 21 shows a comparison of the net calcium enrichment compared against the net sodium depletion where it can be seen that this phenomena is occurring to some extent in nearly all samples. These data do not show a clear trend with respect to relative enrichment values seen in the upper and lower samples in the ML boreholes.

Figures 22 and 23 show the ratios of chloride to boron and strontium. Enrichment and depletion relative to diluted seawater may also be seen in these constituents in the ML boreholes. The relative depletion of boron and enrichment of strontium in lower zones of the Moss Landing Area boreholes correlate with CEMEX area borehole results and suggest base ion exchange with underlying clay formation materials.

The chloride/sulfate ratios (Figure 24) are generally lower in the Moss Landing boreholes, which may indicate sulfate reduction or some other geochemical transformations are occurring.

Water quality data from the Moss Landing area boreholes do show similar geochemical transformations as seen in the CEMEX area, however, there is not a clear trend between the upper and lower zones in the ML- boreholes. Although a substantial difference in TDS between the upper and lower zones is seen in some of the ML- boreholes, the ratios of chloride to the other major ions do not show a reliable trend with respect to relative enrichment or depletion at the Moss Landing site.

5.7.2.2 Molera and Potrero Road Parking Lots, Salinas River State Beach

Water quality samples were collected from a shallow zone and deep zone at the Potrero Road borehole (PR-1) and from four zones at the Molera Parking Lot located approximately one mile south of the Potrero Road parking lot.



Water quality data for Borehole PR-1 show that the lower zone sample is fresh water (TDS = 630 mg/L) and the upper zone sample is consistent with undiluted seawater (TDS = 34,000 mg/L). When comparing the chloride/major ion ratios in the high TDS sample at Potrero Road, there is not a substantial enrichment or depletion with respect to local seawater ratios (see Figures 19 through 24). This indicates that the geochemical transformations of intruded seawater into freshwater, which results in enrichment or depletion, are not occurring at this site.

TDS values in the MDW-1 borehole ranged from approximately 21,000 mg/L in the lowermost zone to approximately 29,000 mg/L in the upper zone. With respect to relative sodium depletion and calcium enrichment, a clear trend (Figure 21 and 22) is seen in the MDW-1 borehole were relative sodium depletion increases from the lower zones to the upper zones

Ratios of chloride to boron and strontium (Figures 23 and 24) indicate that the uppermost zone in the MDW-1 borehole (MDW-1-4, 60'-70') is consistent with diluted seawater for chloride/boron ratios and chloride/strontium ratios. The lower zones in the MDW-1 borehole show a greater departure from the diluted seawater line as a function of depth.

The chloride/sulfate ratios (Figure 25) for the MDW-1 borehole samples show close agreement with the diluted seawater line suggesting that geochemical and/or biological sulfate transformations are not occurring.

5.7.3 Results of δ^2 H and δ^{18} O Analysis

Stable isotopes of oxygen and hydrogen were analyzed in water samples collected from the CEMEX borehole (CX-B1WQ), Moss Landing boreholes, and Potrero Road borehole. Isotope data were measured for all borehole water quality samples collected except ML-1 Zone 1 and ML-1 Zone 2. Water quality samples from ML-1 were not collected because the samples containers were not made available by the firm responsible for the sampling. Isotopic results from Boreholes CX-B2WQ, CX-B4 and MDW-1 is forthcoming and will be provided as an addendum to this report when they are available. Table 5-7 lists the results of the available oxygen and hydrogen isotopic analyses for groundwater samples collected from CEMEX and Moss Landing.



Table 5-7. Results of Oxygen and Hydrogen Isotope Analyses

Borehole and Zone Designation	Delta-Deuterium (δ ² H) (‰)*	Delta-Oxygen 18 (δ ¹⁸ O) (‰)*
CX-B1WQ-1	-18.4	-2.6
CX-B1WQ-2	-29.1	-4.26
CX-B1WQ-3	-6.21	-0.84
CX-B1WQ-4	-14	-2.03
CX-B1WQ-5	-12	-1.56
CX-B1WQ-6	-15.1	-2.08
ML-2-1	-19.2	-3.07
ML-2-2	-37.6	-5.3
ML-3-1	-40.1	-6.04
ML-3-2	-43.6	-6.43
ML-4-1	-24.5	-3.57
ML-4-2	-35.9	-5.23
ML-6-1	-5.55	-0.59
ML-6-2	-11	-1.33
PR-1-1	-42.5	-6.35
PR-1-2	-3	-0.4

The ratio of $\delta^{18}O$ and $\delta^{2}H$ may be used in geochemical analysis to evaluate the relative contribution of different source waters (e.g., surface water and ground water) when evaluating water mixtures. The relative enrichment or depletion of a given source water with respect to $\delta^{2}H$ and $\delta^{18}O$ may be used as a "fingerprint". If there is a sufficient distinction between different water sources, then the relative contribution from a given source may be estimated.

Results from isotopic analyses of borehole water samples for the CEMEX borehole are shown in Figure 26 and results from the Moss Landing boreholes and Potrero Road borehole is shown in Figure 27. The $\delta^{18}O$ and $\delta^{2}H$ data in both Figures are plotted against the Global Meteoric Water Line (GMWL) for reference. Isotopic data are referenced to Vienna Standard Mean Ocean Water (VSMOW) values, which is shown as $\delta^{18}O=0\%$ and $\delta^{2}H=0\%$ values on both plots.

Isotopic data measured at the CEMEX site and at Moss Landing show a linear trend with respect to $\delta^{18}O$ and δ^2H . At the CEMEX facility, $\delta^{18}O/\delta^2H$ data show a linear relationship with the upper end points corresponding to Borehole CX-B1WQ Zone 3, which had the highest TDS (32,700 mg/L) and Borehole CX-B1WQ Zone 2 which had the lowest TDS (14,600 mg/L) (see Figure 26). Data measured at Moss Landing were bracketed by endpoints corresponding to 4,200 mg/L and 33,200 mg/L TDS in Boreholes ML-3 Zone 2 and ML-6 Zone 1, respectively (see Figure 27).



Isotopic results from the relatively low TDS boreholes (Boreholes ML-3 Zone 2 and PR-1 Zone 1) indicate that groundwater has not undergone significant evaporation, or geochemical isotopic fractionation, as the values are near the GMWL. For both the CEMEX site and Moss Landing sites, the trend of the borehole data intercepts the GMWL at similar values (δ^2 H values ranging from -46 % to approximately -52 %), which suggests that the fresh groundwater, which is mixing with intruded seawater at the CEMEX facility, closely corresponds to the GMWL.

Isotopic values measured in samples CX-B1WQ Zone 3, ML-6 Zone 1, and PR-1 Zone 2 represent a local endpoint for intruded seawater, which varies slightly between the sites. Samples from PR-1 Zone 2 are closest to VSMOW values ($\delta^{18}O = -0.4$ % and $\delta^{2}H = -3.0$ %) while ML-6 Zone 1 and CXB1WQ Zone 3 show slightly more depletion in both $\delta^{18}O$ and $\delta^{2}H$ with respect to VSMOW.

5.8 Results of Tritium Analysis

5.8.1 Background: Tritium Source and Interpretation

Tritium is the radioactive isotope of hydrogen, which is often used as a tracer to target young waters (less than about 50 to 60 years old) and to show if there is a presence of modern recharge. The reported half-life of tritium varies; the current recommended half-life is 12.32 years, but some sources use the older half-life of 12.43 years (Kazemi et al., 2006; Tritium Laboratory, 2010). Tritium is produced through the natural cosmic ray bombardment of nitrogen and deuterium in the upper atmosphere, through the natural neutron radiation of lithium in rocks (especially granitic rocks), and through certain anthropogenic activities.

One of the most important and significant sources of tritium is from thermonuclear tests which were conducted in the northern hemisphere by the United States, United Kingdom, and former Soviet Union beginning in 1952 and peaking around 1963-1964. Additional French and Chinese tests were also conducted in the late 1970s. At the northern hemisphere peak in 1963, the tritium concentrations arising from thermonuclear weapons were three orders of magnitude greater than natural tritium concentrations, which usually range between 3-10 TU in the northern hemisphere and 1-5 TU in the southern hemisphere (Kazemi et al., 2006; Happle, 2010). This bomb pulse tritium signature can be traced into the subsurface and is sometimes used to provide information on the rate of groundwater recharge. However, waters younger than the mid-1960s will not show the bomb tritium peak.

Most methods used for analyzing tritium content yield only qualitative or semi-quantitative results; the precise age cannot be determined. Much of the reason for this is caused by uncertainty due to spatial and temporal variations in initial tritium concentrations at the time of recharge. In addition, it is possible to get similar tritium results from waters recharged before and after the tritium peak. This non-uniqueness is another uncertainty that has to be taken into consideration when analyzing the tritium



results. The presence of tritium itself, however, indicates the presence of "young" water (i.e., less than about 50-60 years old) due to recharge, or possibly borehole leakage. Waters older than about the mid-1950s will generally yield values at or below the tritium detection level of 0.8 TU. The absence of tritium does not in itself necessarily indicate an absence of modern recharge. All groundwater samples from wells represent a mixture of water molecules that may have a very wide range of age distributions arising from differences in flow paths. Therefore, the reported concentrations represent some sort of an average that may be produced from the mixing of water of different ages.

Measured tritium concentrations are expressed in Tritium Units (TU) where one TU is the equivalent of one tritium atom (or one THO molecule) per 1018 atoms of hydrogen (or 1018 H2O molecules). Tritium concentrations are also commonly reported in terms of Tritium Ratios (TR), where 1TR = 1TU. One TU is also equivalent to 0.1181 Becquerel per kilogram (Bq/kg), where 1 Becquerel is equal to one decay per second (Tritium Laboratory, 2010).

5.8.2 Tritium Results CX-B1WQ and CX-B2WQ

Tritium samples were taken from all borings conducted during this investigation. Tritium results for the Moss Landing borings are being re-run using a different method to reduce the detection limits. The results from Moss Landing and Borehole CX-B4 from CEMEX will be provided as an addendum to this report. Groundwater samples were analyzed for tritium at Geochron Laboratories in Chelmsford, Massachusetts using a half-life of 12.43 years. The measured tritium concentrations from CX-B1WQ and CX-B2WQ are presented in Table 5-8.

Table 5-8. Results of Tritium Analyses – CX-B1 WQ and CX-B2WQ

Boring	Water Quality Zone Zone	Depth Interval (ft, bgs)	Tritium Activity [TU] units	Error [TU] units	
CX-B1WQ	1	274-284	0.35	±0.09	
CX-B1WQ	2	237-247	0.04	±0.09	
CX-B1WQ	3	182-192	0.01	±0.09	
CX-B1WQ	4	134-144	0.5	±0.09	
CX-B1WQ	5	84-94	0.48	±0.09	
CX-B1WQ	6	51-61	0.81	±0.09	
CX-B2WQ	1	215-225	0.1	±0.09	
CX-B2WQ	2	161-171	0.18	±0.09	
CX-B2WQ	3	104-114	0.44	±0.09	
CX-B2WQ	4	55-65	0.62	±0.09	



These values are also displayed graphically on Figure 5-1 as the tritium concentration versus the average sample depth.

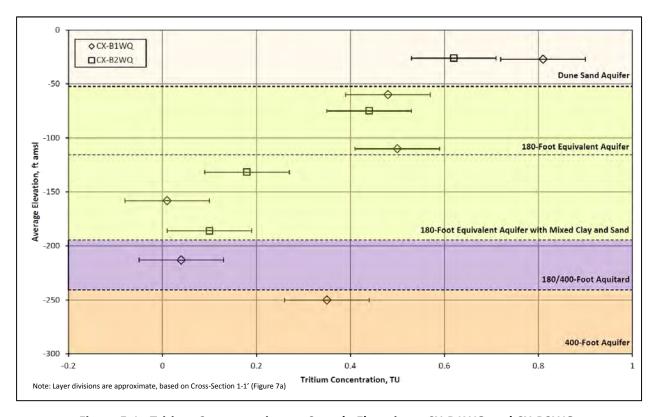


Figure 5-1. Tritium Concentration vs. Sample Elevation – CX-B1WQ and CX-B2WQ

Tritium concentration measured in groundwater samples from Boreholes CX-B1WQ and CX-B2WQ generally decreases with depth, indicating that water possibly takes longer to reach these locations. However, samples taken from elevations between -132 and -213 ft amsl (CX-B1WQ Zones 2 and 3, and CX-B2WQ Zones 1 and 2) have the lowest tritium concentrations. This depth at the base of the 180-FTE Aquifer contains a higher percentage of fine-grained materials and is underlain by the 180/400-Foot Aquitard. This implies that the presence of fine-grained sediments in the lower zone of the 180-FTE Aquifer and the 180/400-Foot Aquitard impedes the movement of water, resulting in water with an older age.

In a study conducted by Michel and others (1997), tritium concentrations along the coast of the Oxnard Plain in California were analyzed. All of the tritium samples came back with very low values and there was no apparent tritium spike in the data, which is similar to the results seen here. Michel et al. interpreted this to mean that the water at the sampled locations entered the subsurface prior to the 1963 tritium peak. Therefore, assuming there is no mixing with different source water, all of the



borehole tritium results from this study indicate that the water is older than the 1960s, with the exception of CX-B1WQ Zone 6 sample collected at 51 to 61 ft bgs.



6.0 NORTH MARINA AND CEMEX GROUNDWATER MODELS

GEOSCIENCE developed the NMGWM which covers the region of the current project, (see Figure 28). The NMGWM has been used to evaluate several proposed projects in the region and will be used, in part, to simulate the effects of slant well pumping. The model was developed in 2008 using computer codes MODFLOW and MT3DMS. In order to accurately model local effects of slant well pumping, a focused model, designated as the CM, is proposed. The CM will be located within the NMGWM centered at the CEMEX site. It will be constructed using the SEAWAT computer code (SEAWAT is a generic MODFLOW/MT3DMS-based computer program designed to simulate three-dimensional variable-density groundwater flow coupled with solute transport) to allow the simulation of sea water intrusion. The CM model will consist of 540 rows and columns with a uniform cell size of 20 feet to a side (see Figure 28), which is a significant refinement over the uniform grid size of 200 ft by 200 ft in the NMGWM. The decreased grid size will allow for a very accurate calibration by matching changes in groundwater levels and quality with historical data.

The exploratory boring information collected during this study has provided valuable data needed to determine the thickness and extent of the Dune Sand Aquifer, Perched "A" Aquifer, and the 180-FTE Aquifer and hydraulic conductivity data for model input. The model layers representing the Dune Sand Aquifer, Perched "A" Aquifer, SVA, and 180-FTE Aquifer will be refined using the new data. Aquifer parameters used in the model will be updated during and after the test slant well program as appropriate to reflect the water level changes occurring in the aquifers during the test slant well pumping.

6.1 Aguifer Characteristics

Hydraulic conductivity values for sediments encountered in the borings were evaluated using both laboratory permeameter test results and using grain-size distribution versus hydraulic conductivity relationship methods published by four different workers. The results are discussed in Section 3.2. Our experience has shown that laboratory permeameter testing typically results in much lower hydraulic conductivity values than those determined by grain-size distribution. Work recently completed by GEOSCIENCE in a coastal aquifer in Southern California, similar to the aquifers encountered in the current study, showed that hydraulic conductivity values calculated from pumping test data closely matched the hydraulic conductivity values using grain-size relationships (GEOSCIENCE, 2013). However, the hydraulic conductivity values determined by grain size distribution can vary significantly from pumping test results depending on the formation tested and selected grain size relationship used for analysis. Nonetheless, the hydraulic conductivity values assigned to the various geologic and aquifer units represent the best available data and will be used for constructing the CM and refining the



NMGWM. The hydraulic conductivity values will be updated with data obtained from the test slant well program.

For groundwater modeling, typical storativity values will be assigned to the aquifer units. Site specific storativity values will be calculated from data to be collected from the long-term pumping test which will be conducted during a subsequent phase of field investigations.

6.2 Model Layer Boundaries

Model layer boundaries and layer extents were defined using the cross-sections prepared from borehole data (see location map Figure 28, Cross-Sections 1-1', 2-2', and 3-3' on Figures 7a through 9, and Cross-Sections A-A' through G-G' on Figures 30 through 36) prepared using lithologic logs and wells from Kennedy/Jenks (2004), DWR and USGS WRIR 02-4003 (2002). The correlation of geologic and hydrostratigraphic units with the regional and local models is summarized in Table 6-1. As seen in the table, the NMGWM will further be refined in the CEMEX Model through the addition of model layers. The NMGWM layers 2 and 4 will each be modeled by 3 layers in the CEMEX Model (layers 2 through 4 and layers 6 through 8, respectively). This division allows for the refinement of aquifer parameters to more accurately reflect the different geologic layers present in these hydrostratigraphic units.



Table 6-1. Correlation of Geologic and Hydrostratigraphic with SVIGSM, NMGWM, CM Model Layers

180/400-Foot Aquifer Subbasin			CEMEX Area					
Surface Geologic Units	Surface Geologic Units Map Symbol	Hydro- stratigraphic Units	Surface Geologic Units	Surface Geologic Units Map Symbol	Hydro- stratigraphic Units	SVIGSM Layer ¹	NMGWM Layer	CEMEX Model Layer
Benthic Zone	-	Benthic Zone	-	-	Benthic Zone	Constant Head	1	1
	Qal ²	Perched "A" Aquifer	Dune Sand	Qd	Dune Sand Aquifer	1a	2	2
Alluvium			Older Dune Sand	Qod				3
Older Alluvium	Qo	Salinas Valley Aquitard	Older Terrace/ Marine Terrace Qt (Qmt?)		1a	3	5	
		180-Foot Aquifer		Qt (Qmt?)	180-FTE Aquifer	1	4	6
Older Alluvium/ Marine Terrace	Qo/Qmt							7
Older Alluvium/ Older Alluvium Fan-Antioch	Qo/Qfa							8
Older Alluvial Fan – Placentia	Qfp	180/400- Foot Aquitard	Aromas Sand (undifferenciated) (?)	Qar (?)	180/400- Foot Aquitard	2a	5	9
Aromas Sand (undifferentiated)	Qar				400-Foot Aquifer	2	6	
Aromas Sand – Eolian/Fluvial Lithofacies	Qae/Qaf	- 400-Foot Aquifer						10
Paso Robles Formation	QT Ac	400/900- Foot Aquitard	Paso Robles	QT	400/900- Foot Aquitard	3a	7	11
		900-Foot Aquifer	Formation		900-Foot Aquifer	3	8	12

¹SVIGSM considers "a" layers to be aquitards (vertical hydraulic conductivity and thickness are input)

Ninety One (91) control points were used to develop the thickness of each model layer and were based on data from all of the cross-sections. The points were then contoured to provide the rest of the model layer surface. The elevation of each model layer is the top elevation minus the determined thickness.



²Subsurface Holocene geologic unit not mapped at surface

For example, the bottom elevation of model layer 1 is the surface elevation minus the thickness of model layer 1; the bottom elevation of model layer 2 is the bottom elevation of model layer 1 minus the thickness of model layer 2, etc. The layer thicknesses for the NMGWM are shown on Figures 37 through 43.

6.3 Hydraulic conductivity

Initial model values for the refinement of horizontal hydraulic conductivity were estimated based on the descriptions of borehole samples, laboratory data, and grain size distribution and hydraulic conductivity relationships. A discussion of the development of the horizontal hydraulic conductivity values is provided in Section 3.2.

6.3.1 Vertical Hydraulic Conductivity

Values for the refinement of model layer vertical hydraulic conductivity were estimated based on the descriptions of borehole samples and a series of curves developed to show the relationship between sediment texture and hydraulic conductivity. These curves, representing maximum and minimum horizontal and vertical hydraulic conductivity values, were developed using the following equation (Durbin, 2013; Faunt, 2009):

$$K_{i} = (K_{c}^{p} F_{c,i} + K_{f}^{p} F_{f,i})^{1/p}$$

where:

Ki = Hydraulic conductivity for cell i [ft/day]

Kc = Horizontal hydraulic conductivity for coarse-grained material [ft/day]

Kf = Horizontal hydraulic conductivity for fine-grained material [ft/day]

Fc,i = Fraction of coarse-grained material in cell i [unitless]

Ff,i = Fraction of fine-grained material in cell i [unitless]

p = Empirical parameter

Lithologic log intervals from the borings were classified as either being "coarse-grained" or "fine-grained" based on the sediment texture described in the logs and texture classification procedures observed in the USGS Professional Paper 1766 (Faunt ed., 2009). Coarse-grained sediment was defined as having a grain size of fine sand or greater (i.e., sand, gravel, pebbles, and cobbles). Fine-grained material was defined as any texture that consisted predominately (greater than 50%) of silt or clay.



To determine the Kc and Kf, the individual lithologic intervals for each borehole were first assigned a maximum or minimum hydraulic conductivity value based on the soil classification for that interval and the estimates of horizontal conductivity made from borehole sample grain size distribution curves. The methods used to estimate the sample hydraulic conductivities are described in greater detail in Section 3.2.1. The weighted Kc and Kf were then calculated for each borehole and each model layer using both the minimum and maximum hydraulic conductivities in order to provide a possible range of Kc and Kf that could be expected for each area (i.e., CEMEX area and Moss Landing area). The results for the CEMEX area are provided in Tables 6 and 7 for the maximum and minimum hydraulic conductivity values respectively and the results for the Moss Landing area are provided in Tables 8 and 9 for the maximum and minimum hydraulic conductivity values, respectively.

The empirical parameter shown in the equation above imparts a particular textural structure to help approximate flow in a heterogeneous anisotropic groundwater system. P values of 0.93 and -0.62 were used for calculating horizontal and vertical hydraulic conductivity, respectively, based on numerical experiments conducted by Durbin (2013).

Figures 44 through 47 show the different curves for the calculation of hydraulic conductivity, and the ranges shown represent the initial values for horizontal and vertical hydraulic conductivity which will be used for the refinement of model aquifer parameters. These values will be modified during model calibration. Figures 44 and 45 show the sediment texture versus hydraulic conductivity at the CEMEX site for the Dune Sand Aquifer and 180-FTE Aquifer, respectively. For the Dune Sand Aquifer, it was estimated that the average percentage of coarse-grained deposits was 98%. Therefore, the horizontal hydraulic conductivity is expected to range from 109 to 304 ft/day with an average of 207 ft/day, while the vertical hydraulic conductivity is expected to range from approximately 8 to 12 ft/day with an average of approximately 10 ft/day. It was estimated that for the 180-FTE Aquifer, the average percentage of coarse-grained deposits was 78%. This correlates with a horizontal hydraulic conductivity value ranging from 71 to 216 ft/day and averaging 143 ft/day. The vertical hydraulic conductivity for this aquifer is expected to range from 0.11 to 0.21 ft/day with an average of 0.16 ft/day.

The sediment texture versus hydraulic conductivity curves for the Dune Sand/Perched "A" Aquifer near the Moss Landing site is shown on Figure 46. These two aquifers are combined because they represent a single model layer. Based on the borehole grain size analysis presented above, the average percentage of coarse-grained deposits is estimated at 49%. As shown, this correlates to a horizontal hydraulic conductivity ranging from 101 to 333 ft/day with an average of 217 ft/day and a vertical hydraulic conductivity ranging from 0.04 to 0.06 ft/day with an average of 0.05 ft/day.

Figure 47 shows the sediment texture versus hydraulic conductivity at the Potrero Road site for the Dune Sand/Perched "A" Aquifer. It was estimated that the average percentage of coarse-grained



deposits here was 93%. Therefore, the horizontal hydraulic conductivity is expected to range from 367 to 1,205 ft/day with an average of 786 ft/day, while the vertical hydraulic conductivity is expected to range from 0.92 to 1.5 ft/day with an average of 1.2 ft/day.



7.0 FINDINGS

7.1 General

- The conceptual hydrogeologic model developed from this investigation suggests that a
 feedwater supply system using slant wells at the CEMEX site is feasible and can utilize the Dune
 Sand Aquifer and the underlying terrace deposits as conduits to extract water through the
 seafloor beneath Monterey Bay.
- This opinion will be tested using the newly constructed CEMEX Model and the refined NMGWM and should be field tested using a test slant well and groundwater monitoring system as described in the Hydrogeologic Investigation Workplan.
- A permeable unit of significant thickness containing groundwater of seawater quality was penetrated in the Moss Landing Boring PR-1 near Boring ML-1. To the north, this unit pinches out and mixes with fine-grained sediments. To the south, the unit decreases in thickness to approximately 25 feet in boring MDW-1 over a distance of approximately one mile.
- The conceptual model also indicates that the Perched "A" Aquifer between the Molera and Sandholt Road Salinas River State Beach parking lots could provide an alternative target for construction of a subsurface feedwater supply system.

7.2 CEMEX Area

The CEMEX facility is located on the westernmost edge of the 180/400-Foot Aquifer Subbasin of the Salinas Valley Groundwater Basin, as currently mapped by DWR (2003) and the MCWRA (2011). The findings of the investigation at CEMEX are summarized below:

- A significant clay layer is not present beneath the Dune Sand Aquifer at the CEMEX site at elevations commonly attributed to the SVA, suggesting a different depositional environment than that of the 180-Foot Aquifer in the Salinas Valley. The water quality data suggests groundwater in the Dune Sand Aquifer may be in hydraulic continuity with the underlying aquifer units. The degree of hydraulic continuity will be determined by construction of aquifer specific monitoring wells and the long-term pumping test of the test slant well.
- Stratigraphic relationships and lithologic observations indicate that the aquifer system underlying the Dune Sand Aquifer consists of terrace deposits that are older than the inland 180-Foot Aquifer deposits, since they underlie the Older Dune Sand.



- The terrace deposits appear to be a distinct lithologic unit in terms of geologic history and depositional environment in the Dune Highland area and may be hydrostratigraphically equivalent to the 180-Foot Aquifer in the Salinas Valley.
- For purposes of this document the alluvial materials encountered near the coast (in the CEMEX area) are based solely on analyses of borehole samples (and geophysical borehole logs). As of yet, no direct correlation can be made between these coastal alluvial deposits and the standard naming convention found further inland (e.g., 180-Foot Aquifer, 400-Foot Aquifer, SVA, etc.).
- As a hydrogeologic unit, the terrace deposits will be designated as the 180-FTE Aquifer. The extent of hydrostratigraphic equivalence will be evaluated through a pumping test utilizing the test slant wells and a monitoring network.
- The current interpretation of the distinctive dark greenish-gray clay found at depths ranging from 241 to 282 ft bgs at CEMEX is that it may represent a change in the depositional history and is underlain by a unit equivalent to the Aromas Sand(?)/400-Foot Aquifer. However, results of groundwater quality sampling from the 400-Foot Aquifer have results similar to that of the overlying Dune Sand Aquifer and 180-FTE Aquifer.
- Both the Dune Sand Aquifer and the underlying 180-FTE Aquifer extend seaward beneath the Monterey Bay.
- Groundwater in the Dune Sand Aquifer and most of the groundwater in the 180-FTE Aquifer exhibit high concentrations of TDS, ranging from 24,000 to 32,000 mg/L.
- Hydraulic conductivity for the Dune Sand at CEMEX ranged from an average low value of 273 ft/day to an average high value of 779 ft/day.
- Hydraulic conductivity for the Older Dune Sand at CEMEX ranged from an average low value of 136 ft/day to an average high value of 372 ft/day.
- Hydraulic conductivity for the 180-FTE terrace deposits ranged from an average low value of 113 ft/day to an average high value of 342 ft/day.
- Hydraulic conductivity values will be further refined based on the long-term test slant well pumping test.
- Analysis of cation/anion ratios indicates that groundwater in the lower portion of 180-FTE Aquifer and in the 400-Foot Aquifer have been geochemically altered due to seawater intrusion.
- Tritium results indicate that groundwater in the lower portion of the 180-FTE Aquifer is older than groundwater in the upper portion of the 180-FTE Aquifer and the Dune Sand Aquifer.



- Analysis of oxygen and hydrogen isotopes suggests that in both the CEMEX and Moss Landing sites, saltwater from the ocean is mixing with a freshwater source that has not undergone significant evaporation (as would be expected of a surface water source).
- Hydrostratigraphic relationships indicate that slant wells drilled into the Dune Sand Aquifer and 180-FTE Aquifer will receive recharge primarily from ocean sources through vertical leakage from the sea floor and horizontal recharge from offshore subsea aquifers. This will be tested by the CM and refined NMGWM as well as field pumping tests.

7.3 Moss Landing Hydrogeologic Conditions

The Moss Landing area is located north of the mouth of the Salinas River, which overlies the westernmost edge of the 180/400-Foot Aquifer Subbasin. Borings were drilled and sampled at Moss Landing Harbor and at the Molera, Potrero Road, and Sandholt Road parking lots of Salinas River State Beach. The exploratory borings primarily penetrated fluvial sediments associated with Holocene and Late Pleistocene Salinas River deposition.

The Perched⁷ "A" Aquifer is ascribed to the Holocene river alluvium and considered to be the hydrostratigraphic equivalent of the Dune Sand Aquifer located to the south.

- The Perched "A" Aquifer in the Moss Landing area is composed of interbedded river and floodplain deposits.
- With the exception of the sediments penetrated in Boring PR-1 and MDW-1, individual sand and sand and gravel lenses do not appear to be either vertically or areally extensive in Moss Landing.
- Significant variations in TDS concentrations suggest that groundwater is mixed with seawater, and is likely present in semi-isolated lenticular deposits.
- In general, the upper isolated aquifer test zones were above a depth of 110 ft bgs. TDS concentrations ranged from 3,200 mg/L to 34,000 mg/L.
- The lower isolated aquifer zones were generally constructed at depths exceeding 150 ft bgs. With the exception of Zone 1 of PR-1 (190-200 ft bgs) at 630 mg/L, the TDS concentrations ranged from 7,400 mg/L to 34,000 mg/L.

⁷ The term Perched "A" Aquifer refers to the shallow aquifer above the Salinas Valley Aquitard. Traditionally, the term "perched" aquifer refers to a hydrogeologic condition where an aquifer is formed by groundwater being present above (perching on) an impermeable unit such as clay but with an unsaturated portion of an aquifer between the bottom of the clay and the underlying saturated portion of a lower aquifer.



- Boring PR-1 penetrated a very permeable unit in the Perched "A" Aquifer from 54 to 139 ft bgs.
 Groundwater in this interval approximated seawater quality (i.e., 34,000 mg/L). This unit is
 interpreted to continue, but decrease in thickness southward towards Boring MDW-1. To the
 north, the unit is interbedded with fine-grained units.
- It is interpreted that the lowest portion of Boring PR-1 penetrated the SVA. Very low TDS concentrations (630 mg/L) encountered in the lowest zone in Boring PR-1 suggest that isolated zones of freshwater may exist within the 180-Foot Aquifer or that the sand unit is laterally discontinuous and may be interbedded with the SVA. In this last interpretation, Boring PR-1 did not completely penetrate the SVA.
- Hydraulic conductivity values for the permeable portion of the Perched "A" Aquifer penetrated in PR-1 ranged from 194 ft/day to 717 ft/day, based upon relationships between grain size distribution and hydraulic conductivity.
- The permeable unit between Boring PR-1 and MDW-1 represents a potential location for slant wells.
- The Moss Landing Borings (ML-1, ML-2, ML-3, ML-4, and ML-6) did not penetrate significant thicknesses of permeable deposits to produce the required feedwater supply volume for the MPWSP.

7.4 Groundwater Models

The geologic and hydrogeologic data collected during this investigation was used to prepare the interpretations of hydrostratigraphic relationships in the Moss Landing and CEMEX areas which will be used to refine the NMGWM and to develop the CEMEX focused groundwater model. Table 6-1 summarizes the correlation of geologic and hydrostratigraphic units with model layers.



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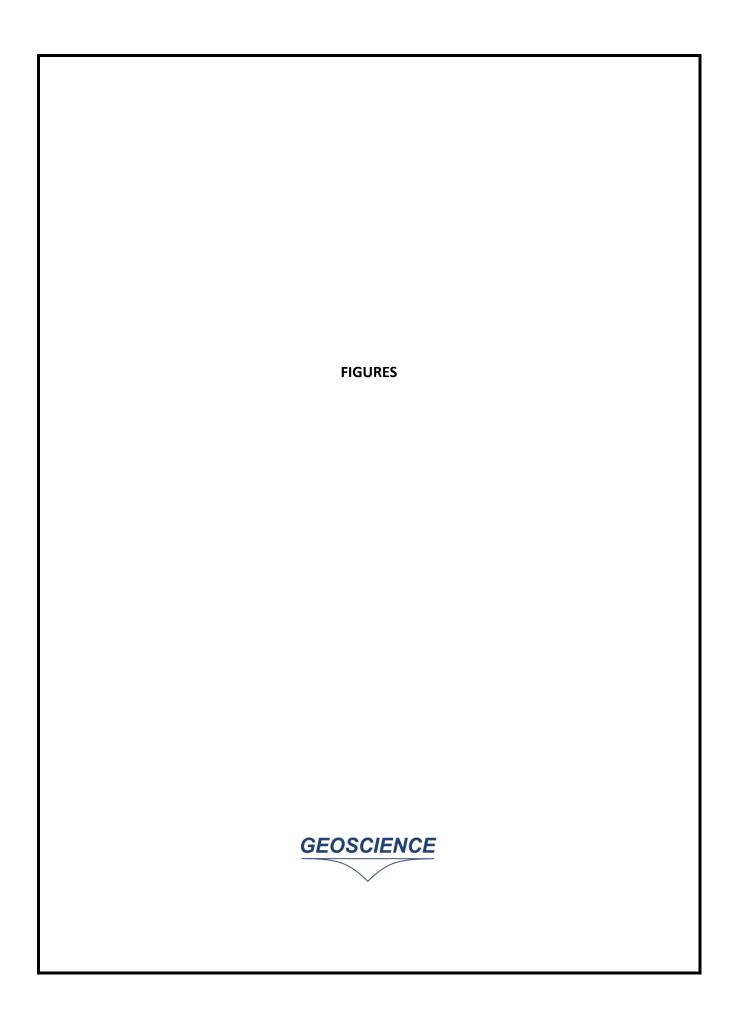


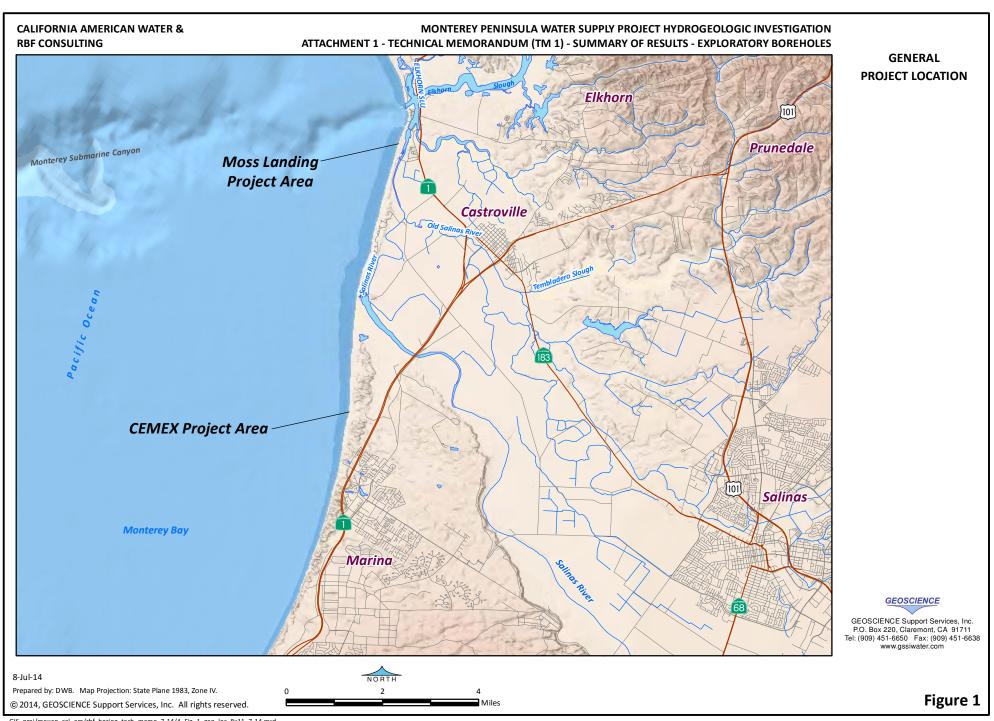
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 MONTEREY PENINSULA WATER SUPPLY PROJECT
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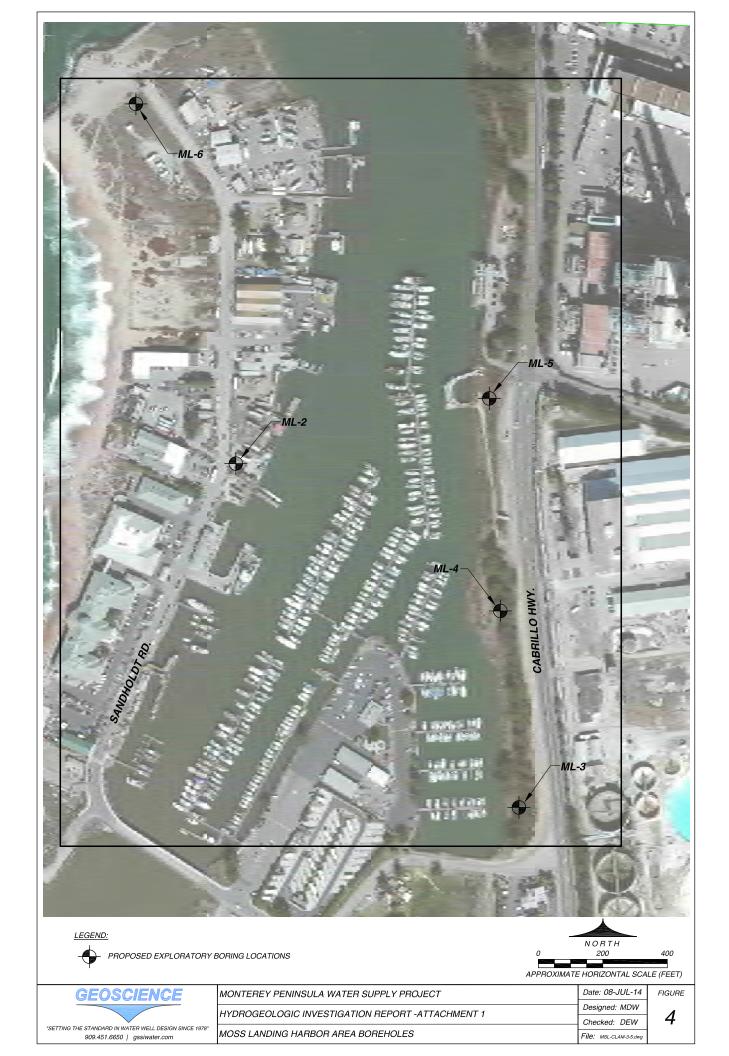
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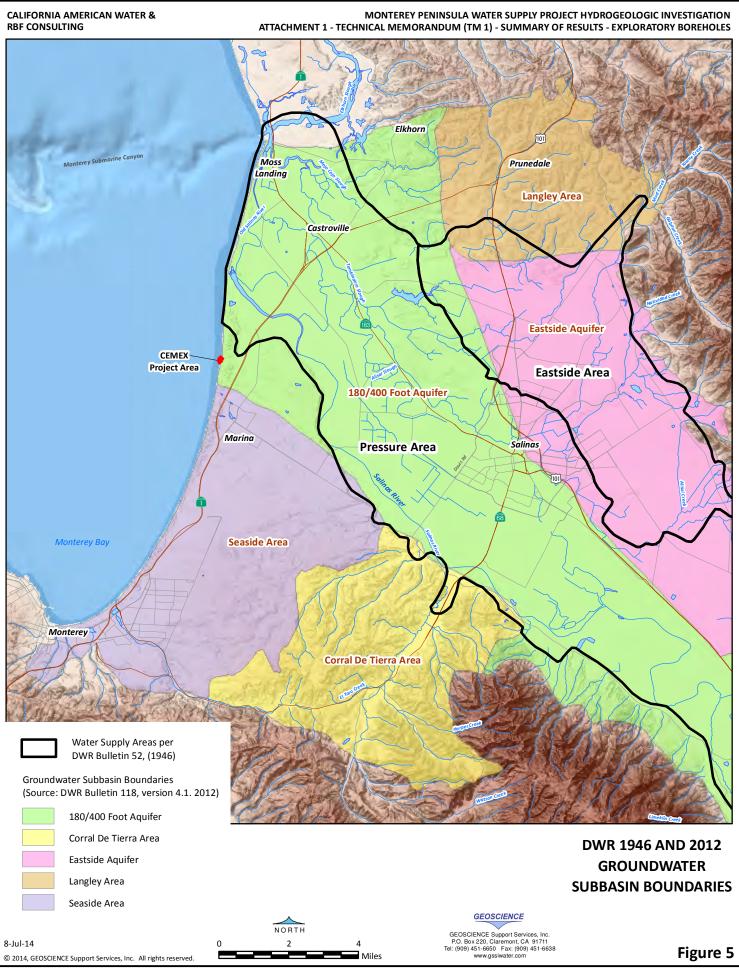
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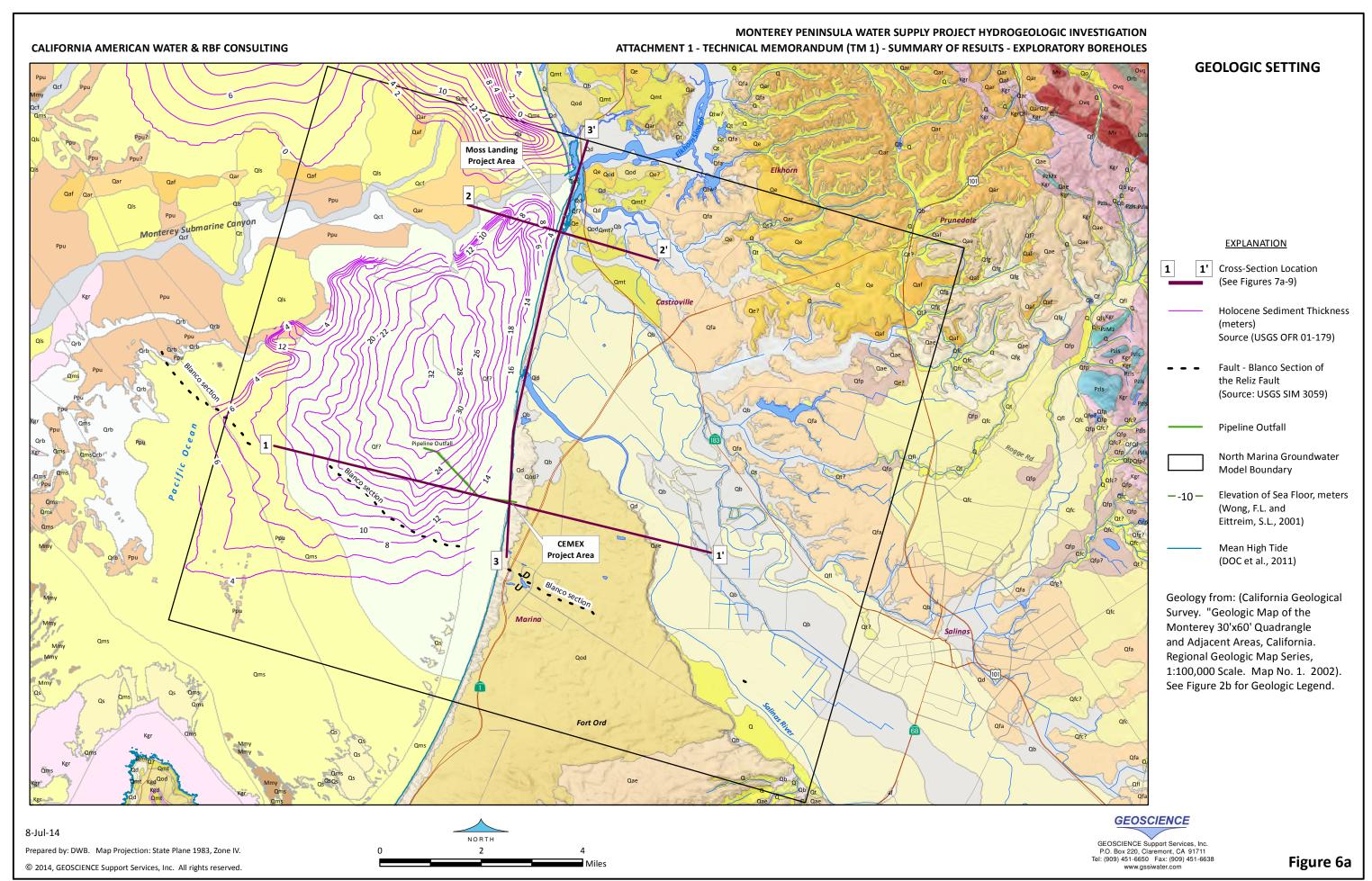
FIGURE

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MONTEREY PENINSULA WATER SUPPLY PROJECT HYDROGEOLOGIC INVESTIGATION ATTACHMENT 1 - TECHNICAL MEMORANDUM (TM 1) SUMMARY OF RESULTS - EXPLORATORY BOREHOLES

California Geological Survey GEOLOGIC MAP OF THE MONTEREY 30'x60' QUADRANGLE AND ADJACENT AREAS, CALIFORNIA

Compiled by David L. Wagner, H. Gary Greene, George J. Saucedo and Cynthia L. Pridmore. 2002

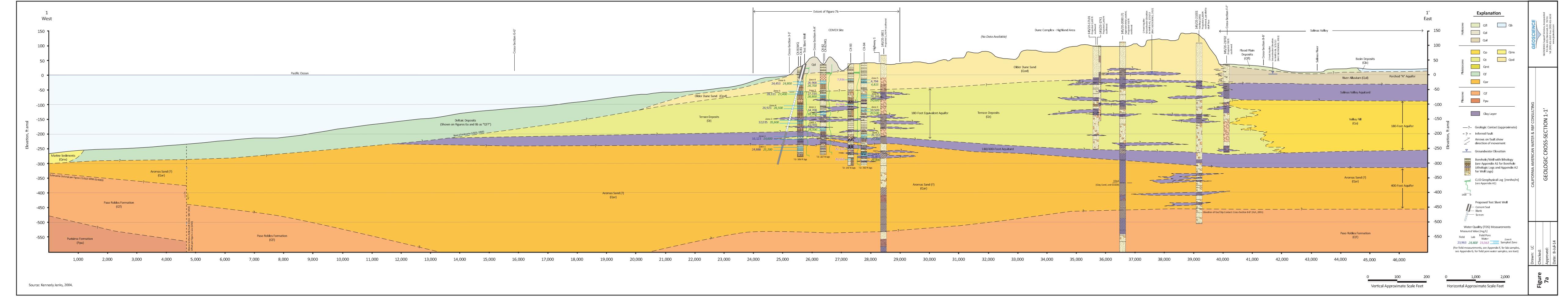
	and Cyntina L. Fridinore.	2002						
	af - Artificial Fill							
Holocene	Q - Alluvium Qfl - Flood Plain Depos	Qb - Basin Deposits						
поюсене	Qs - Sand							
	Qe - Eolian Sand Qd - Dune Sand	Qcf - Canyon Fill (offshore)						
	Qal (*) - River Alluvium							
	Qo - Older Alluvium Qls - Landslide Deposit	Qms - Marine Sediments						
	Qt - Terrace Deposits Qod - Older Dune Sand	1						
	Qmt - Marine Terrace Deposits							
	Qf - Alluvial Fan Deposits Qtw - Terrace Deposits of Qct - Submarine Canyon Terrace							
	(Deltaic deposits offshore) Watsonville T							
Pleistocene	Qfa - Fan Deposits of Antioch							
	Qfc - Fan Deposits of Chular							
	Qfp - Fan Deposits of Placentia	Qfp - Fan Deposits of Placentia						
	Qfg - Fan Deposits of Gloria	* NOTE: Qal is not shown as a map unit.						
	Qar - Aromas Sand (undivided)	Stratigraphic relationships indicate						
	Qae - Eolian Facies Oaf - Fluvial Facies	its position in the subsurface.						
	QT - Plio-Pleistocene Continental Deposits							
Pliocene	Ppu - Purisma Formation							
	MPe - Etchegoin Formation							
	Mv - Unnamed Miocene Volcanic Rocks							
Miocene	Mmy - Monterey Formation							
Miloceffe	Tv - Tertiary Volcanic Rocks							
	Mus - Unnamed Miocene Sandstone							
•	Orb - Red Beds							
Oligocene	Ovq - Vaqueros Sandstone							
	EOsj - San Juan Bautista Formation							
Paleocene- Eocene	Ebu - Unnamed Eocene Sedimentary Rocks							
Eocene	Ec - Carmelo Formation							
	Kgr - Granitic Rocks							
Cretaceous	Kqm - Quartz Monzonite							
	Kgd - Granodiorite							
Jurassic	PzMz - Prebatholithic Metasedimentary Rocks							
	Pzls - Carbonate Rocks							
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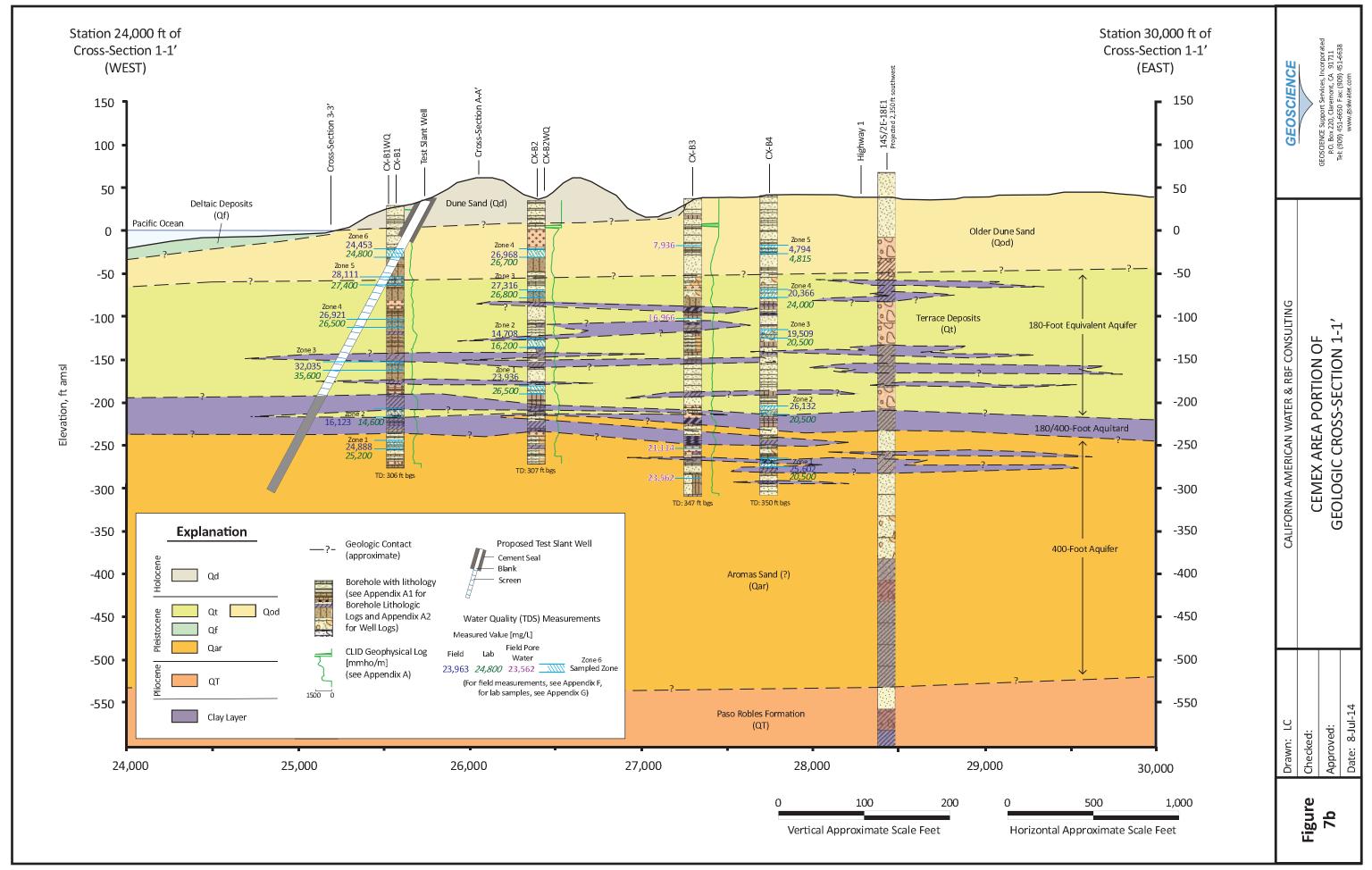
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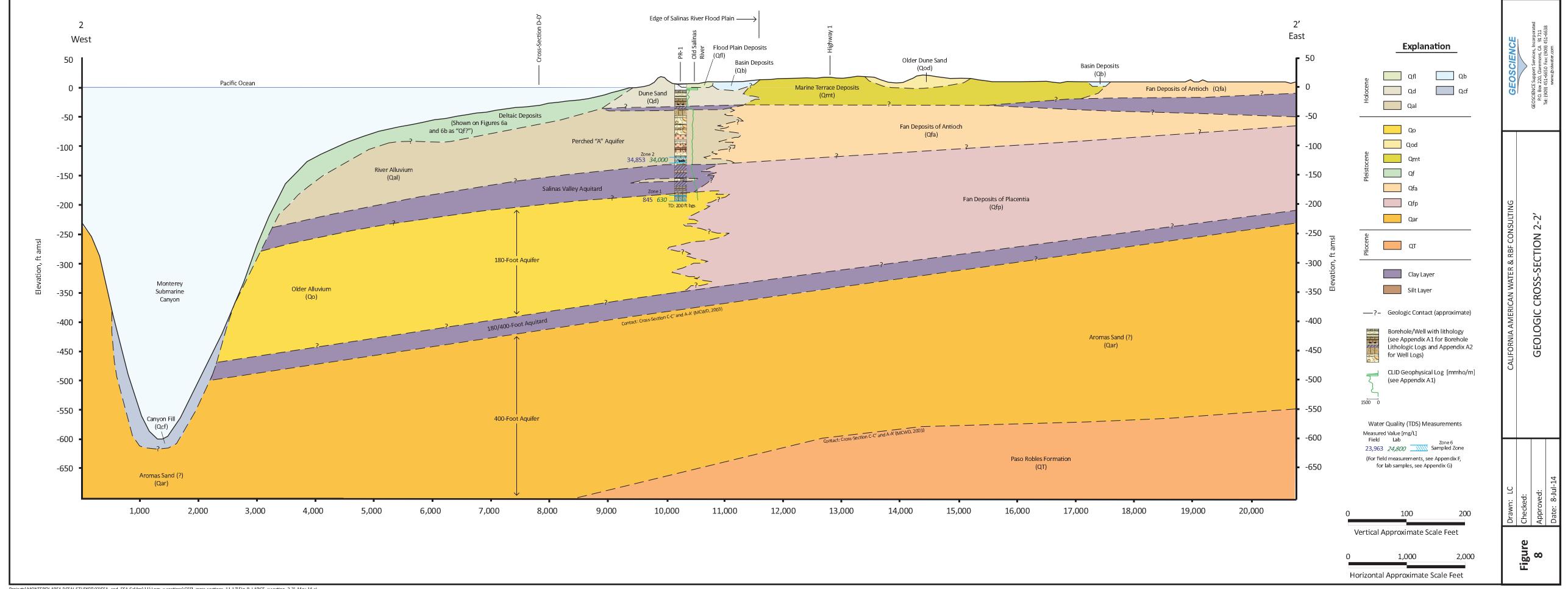
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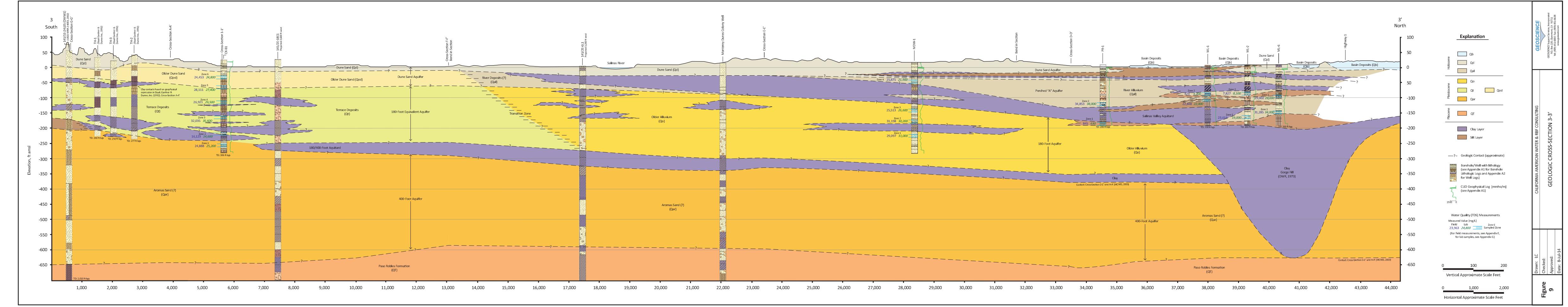
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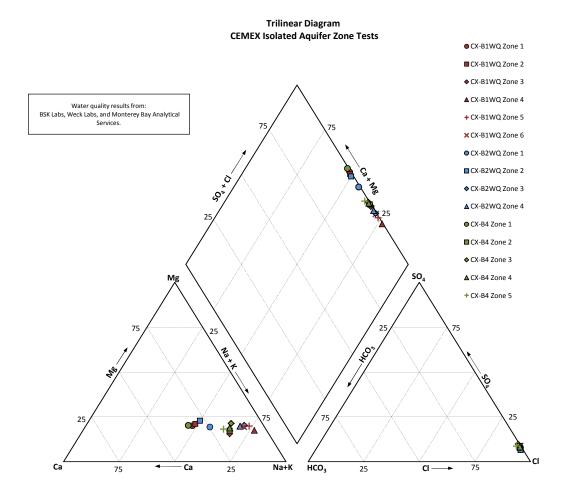
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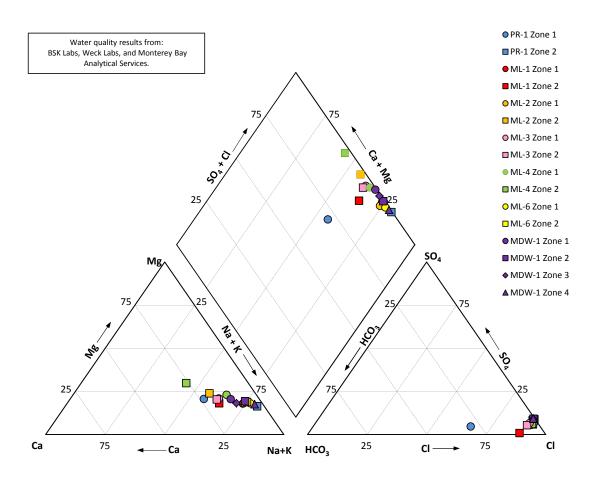






Trilinear Diagram

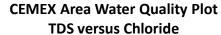
Moss Landing Isolated Aquifer Zone Tests

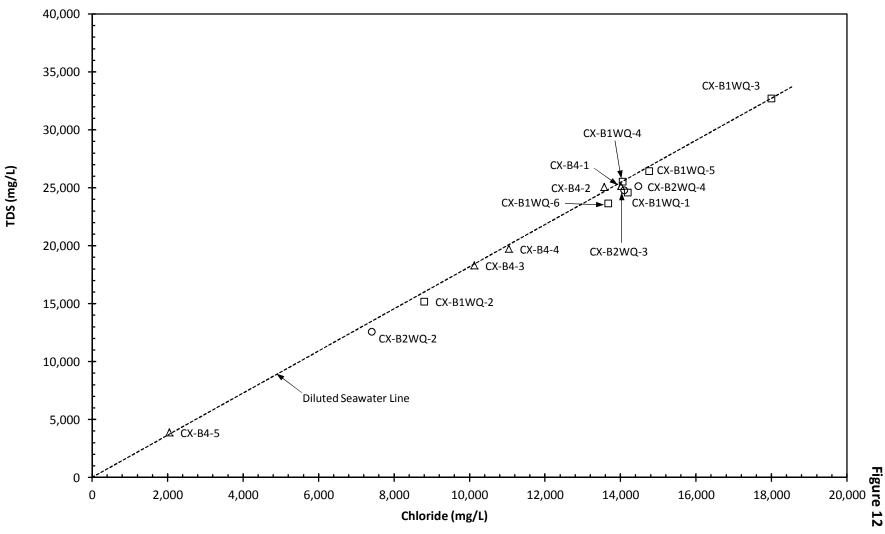


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Monterey Peninsula Water Supply Project Hydrogeologic Investigation

Attachment 1 - Technical Memorandum (TM 1) - Summary of Results - Exploratory Boreholes



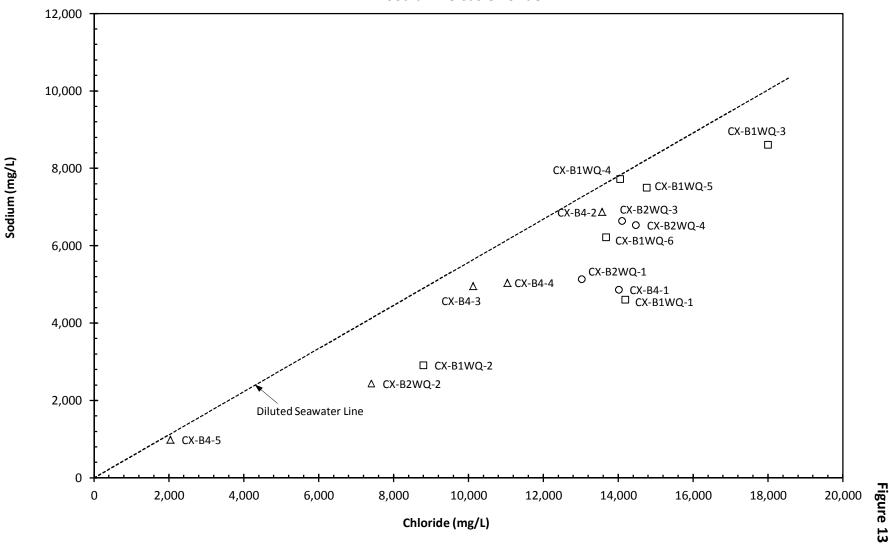


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Monterey Peninsula Water Supply Project Hydrogeologic Investigation

Attachment 1 - Technical Memorandum (TM 1) - Summary of Results - Exploratory Boreholes



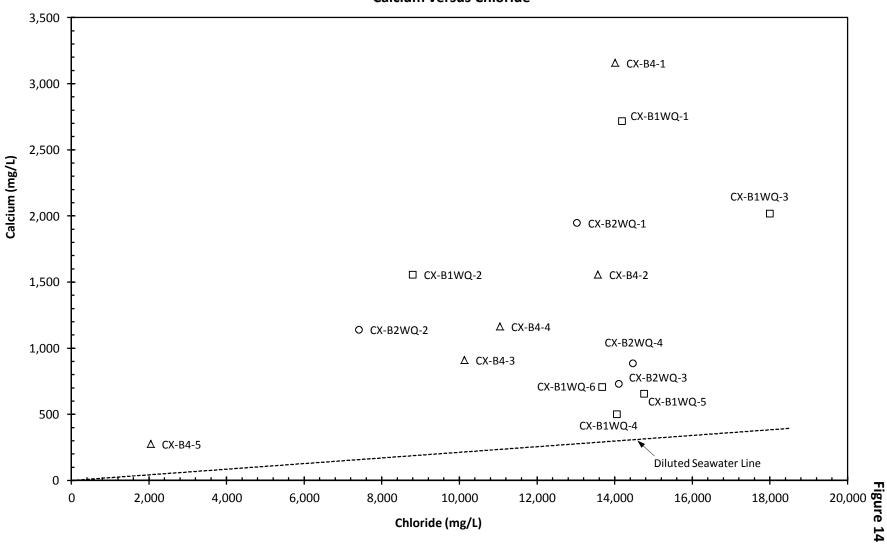


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CEMEX Area Water Quality Plot Calcium versus Chloride

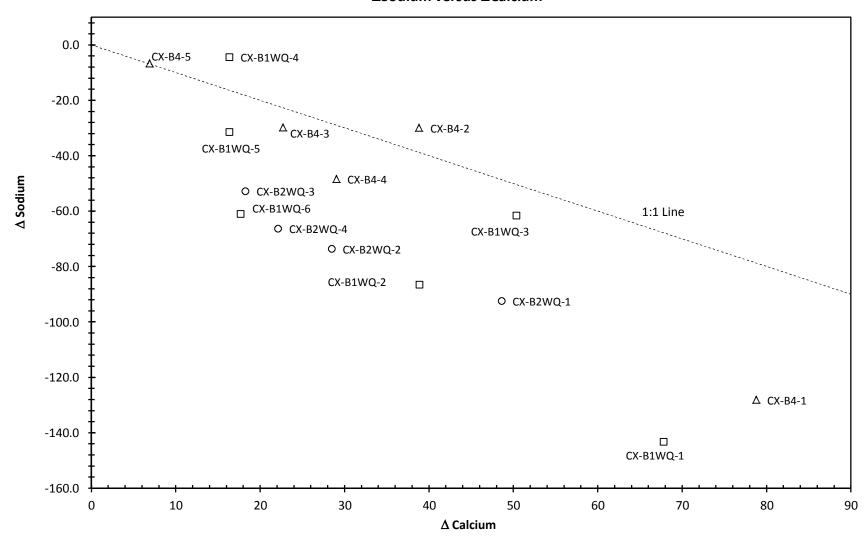


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CEMEX Area Water Quality Plot ΔSodium versus ΔCalcium

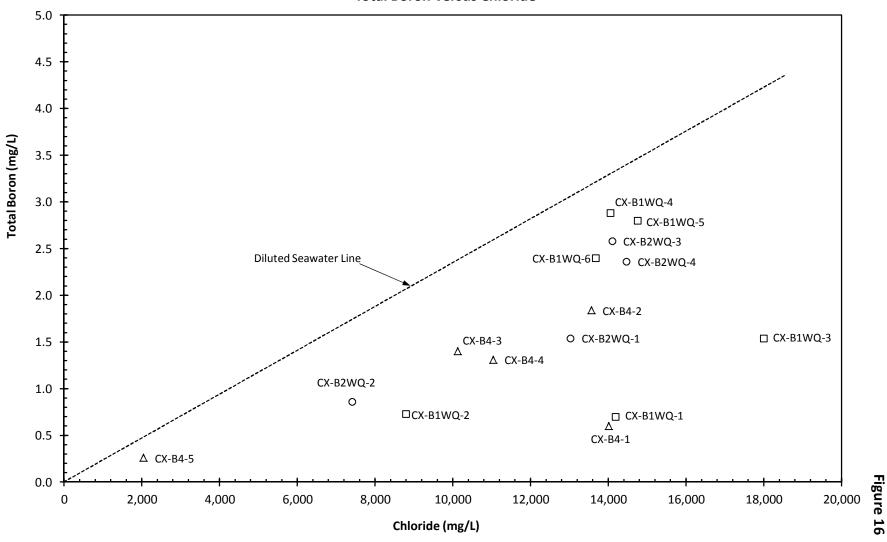


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CEMEX Area Water Quality Plot Total Boron versus Chloride

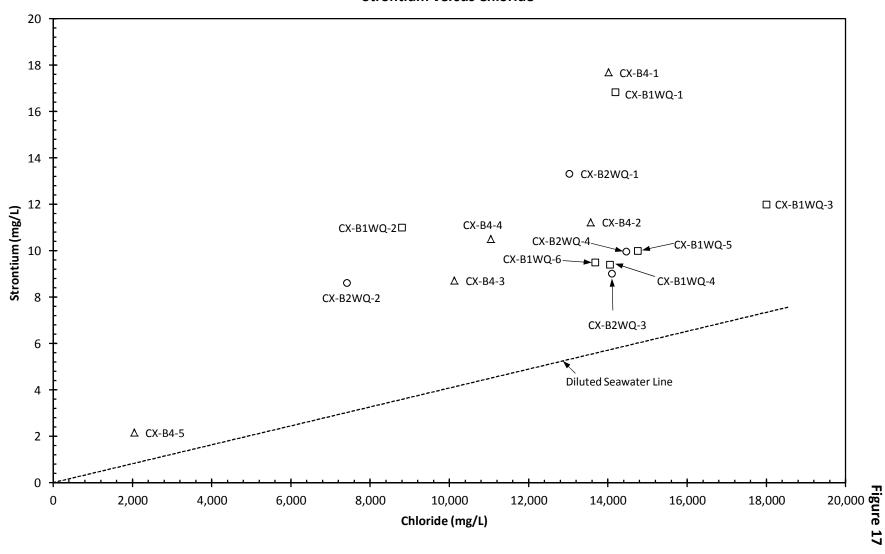


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CEMEX Area Water Quality Plot Strontium versus Chloride

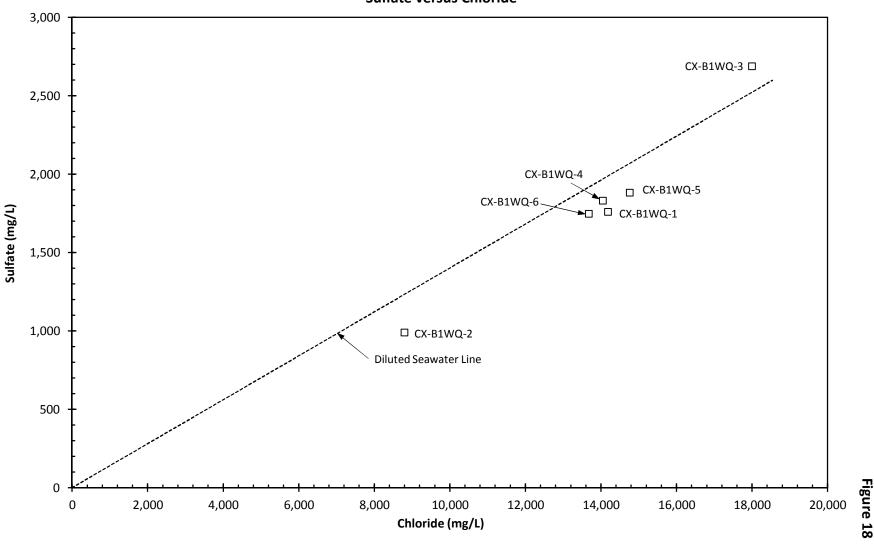


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CEMEX Area Water Quality Plot Sulfate versus Chloride



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Moss Landing Area Water Quality Plot TDS versus Chloride

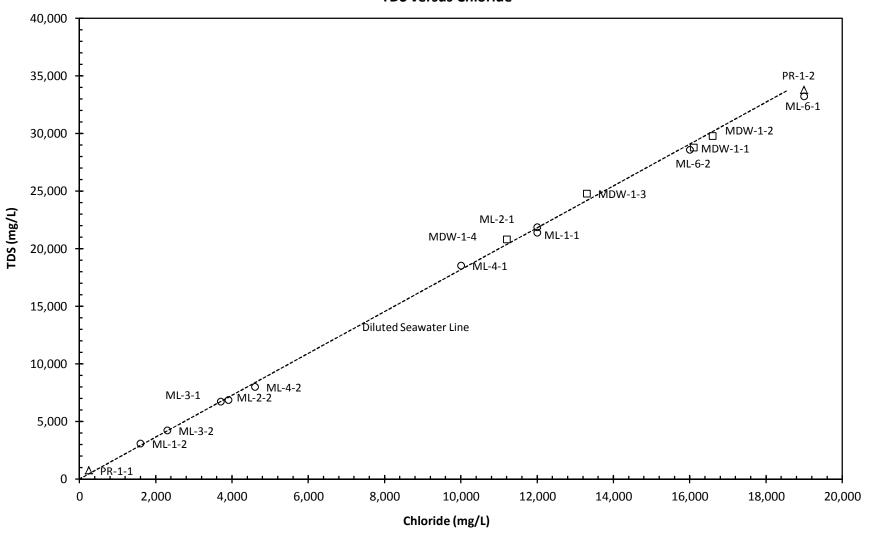


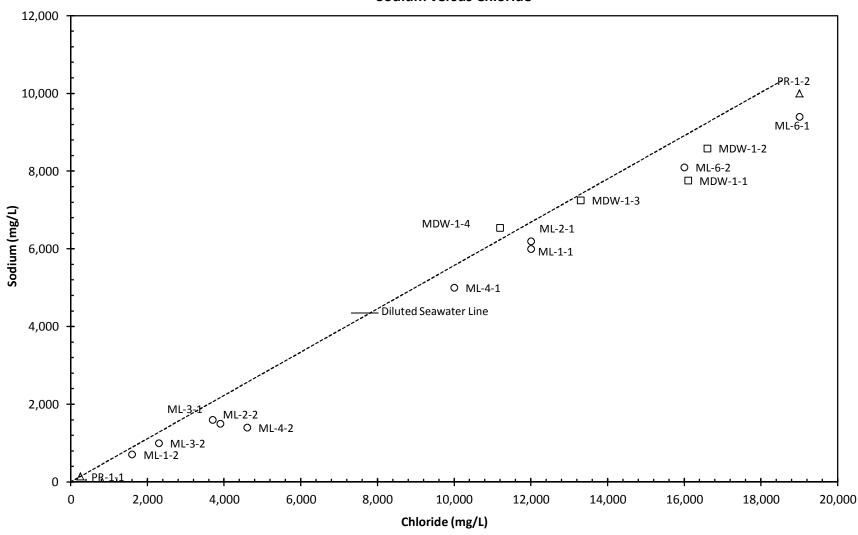
Figure 19

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Moss Landing Area Water Quality Plot Sodium versus Chloride

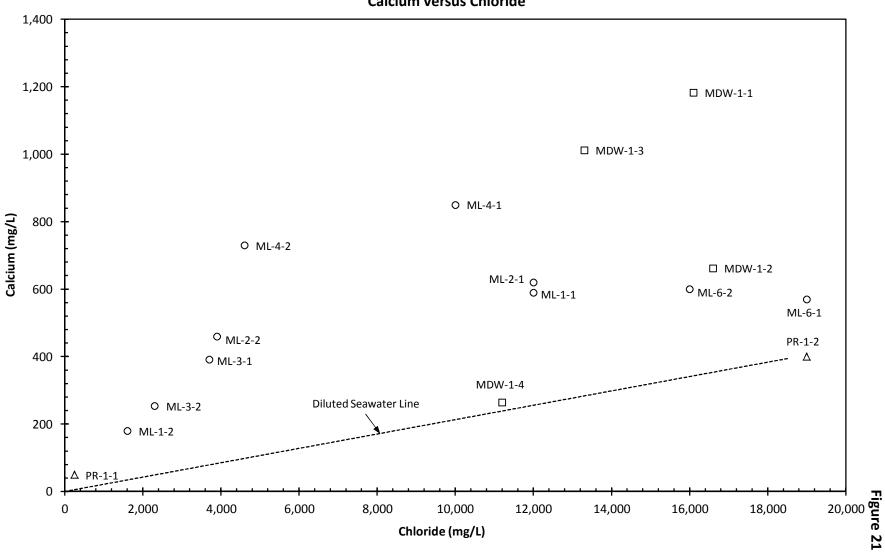


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Moss Landing Area Water Quality Plot Calcium versus Chloride

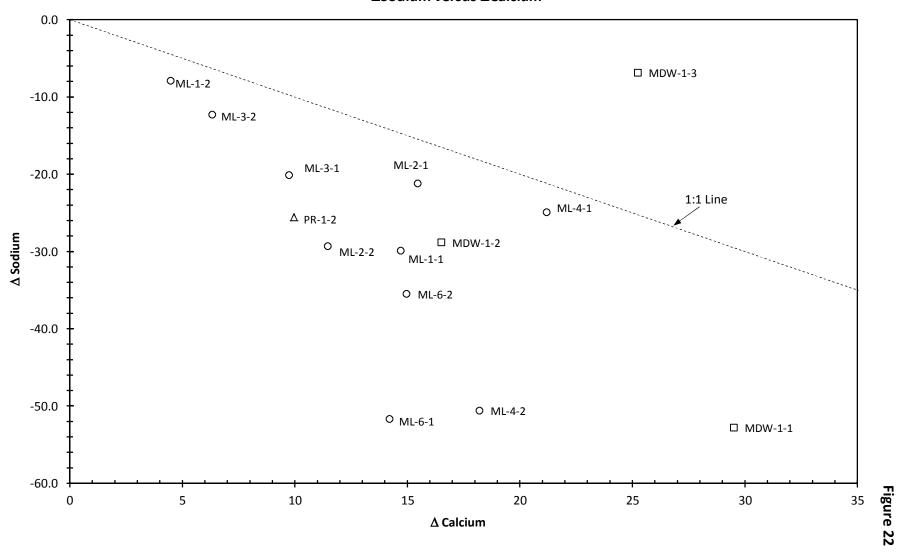


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Moss Landing Area Water Quality Plot ΔSodium versus ΔCalcium

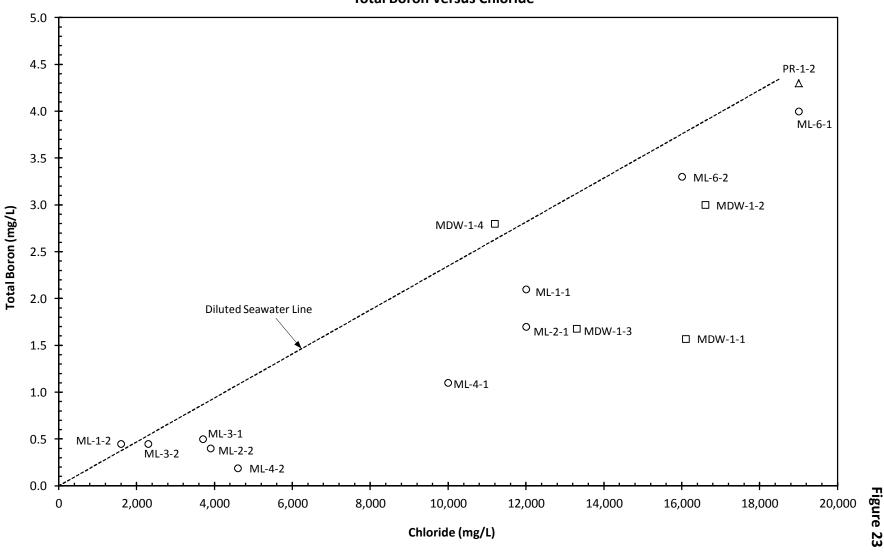


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Moss Landing Area Water Quality Plot Total Boron versus Chloride

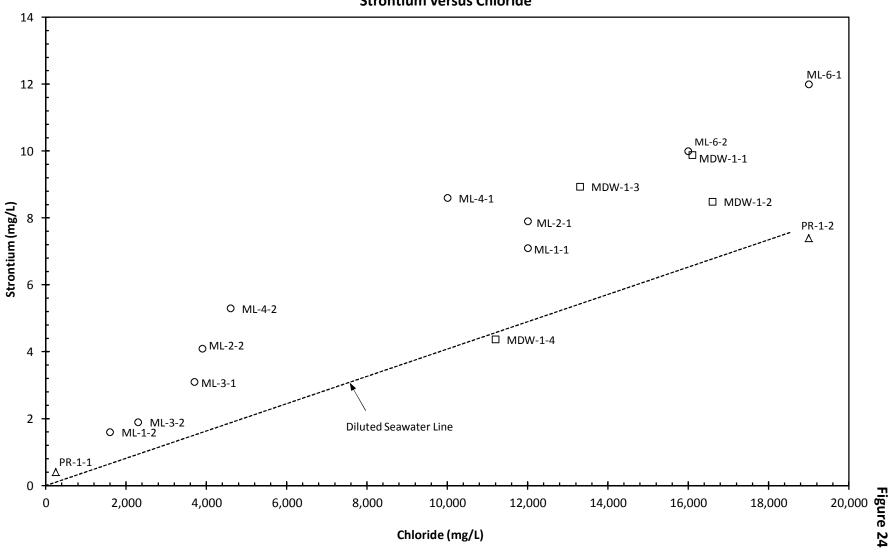


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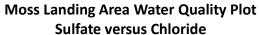
Moss Landing Area Water Quality Plot Strontium versus Chloride

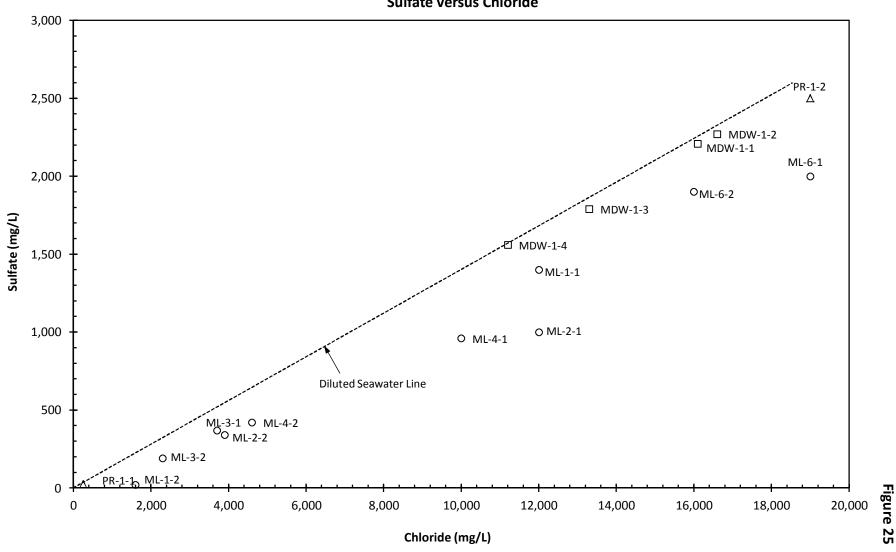


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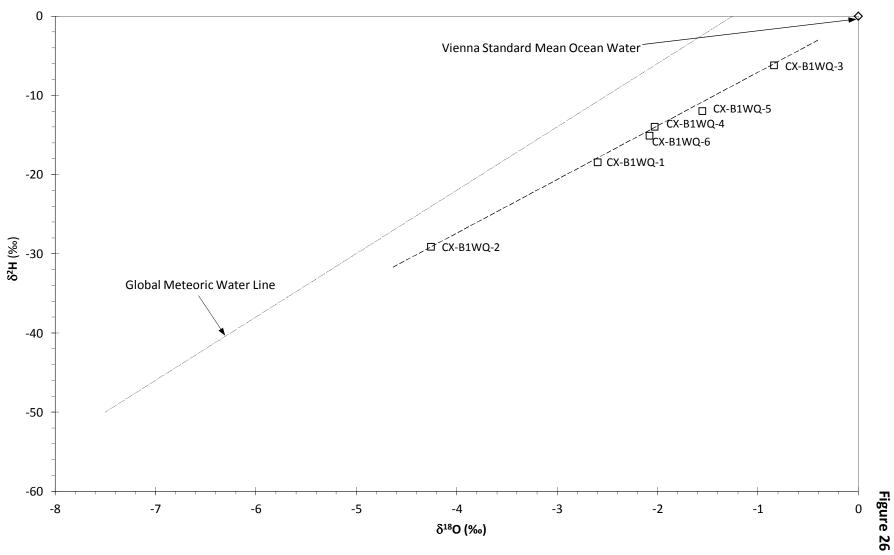


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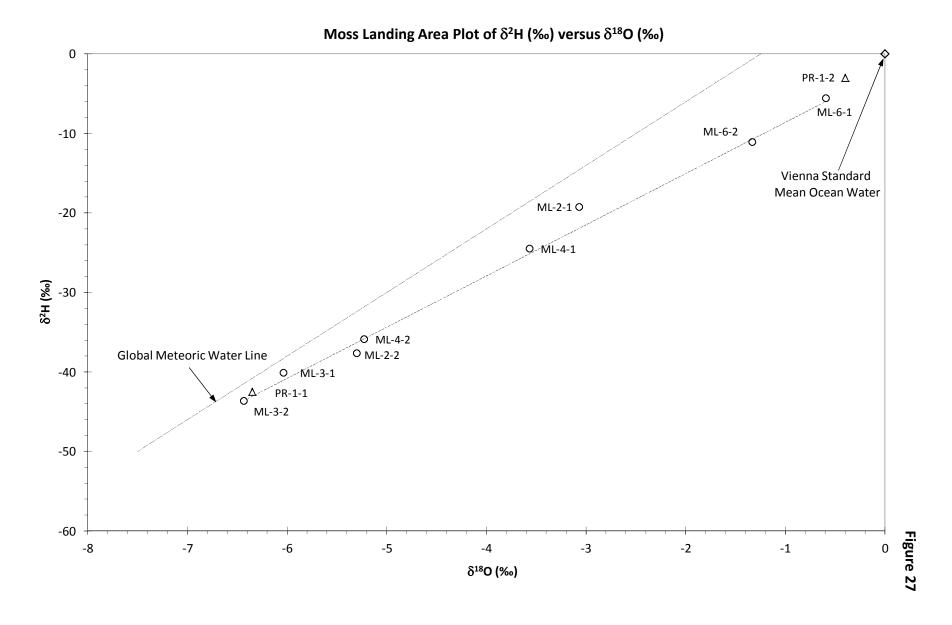




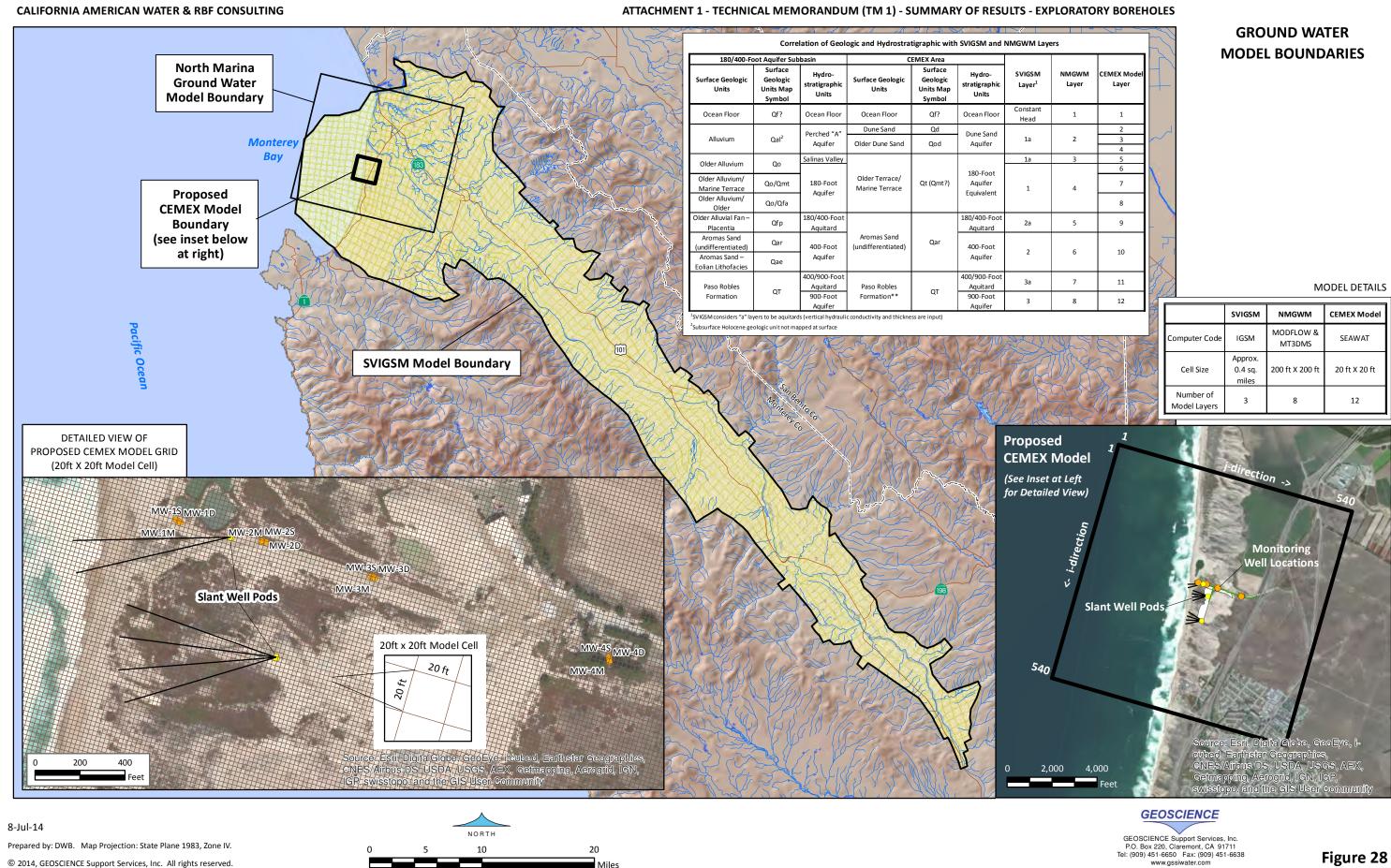
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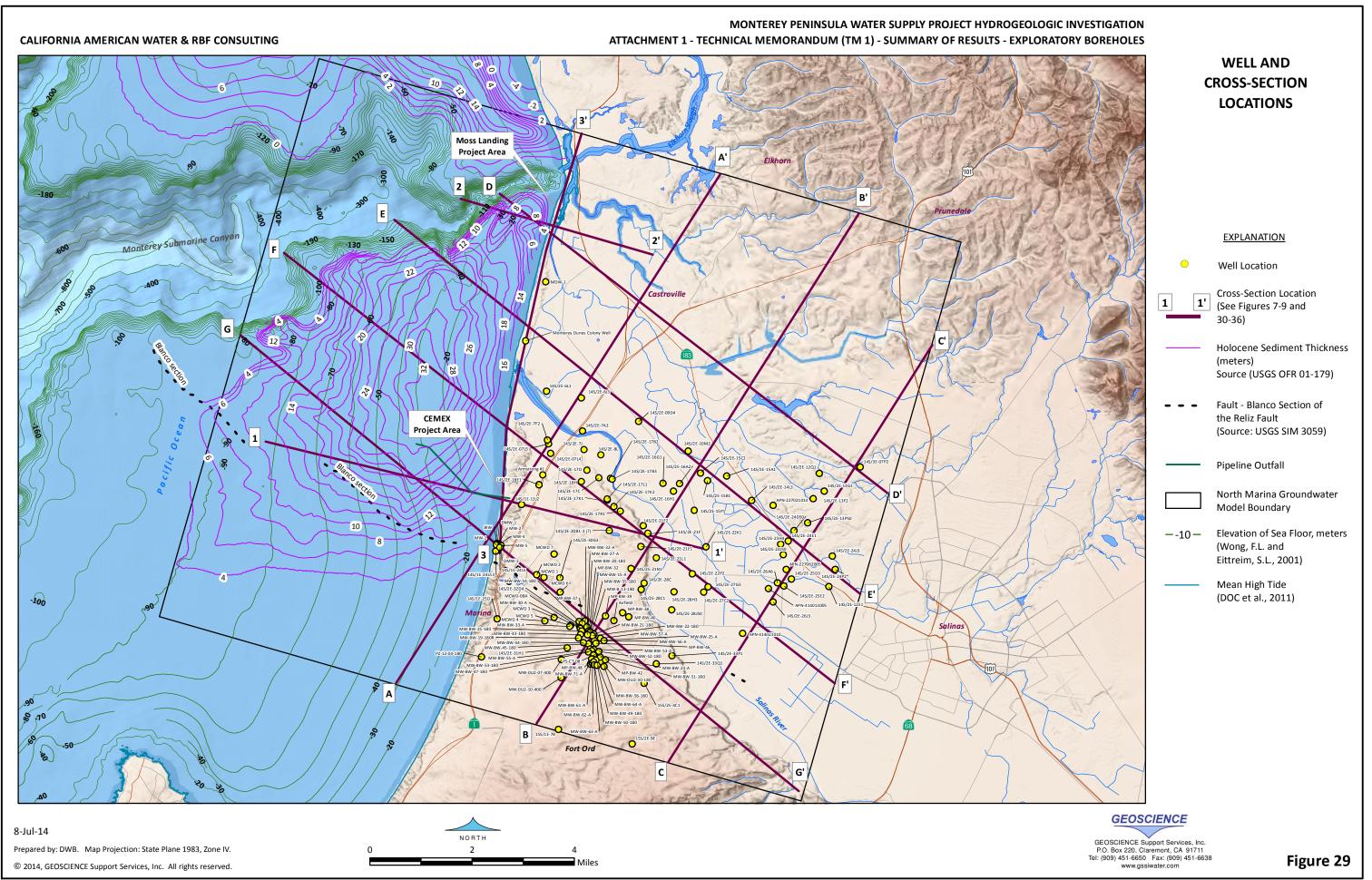
Monterey Peninsula Water Supply Project Hydrogeologic Investigation

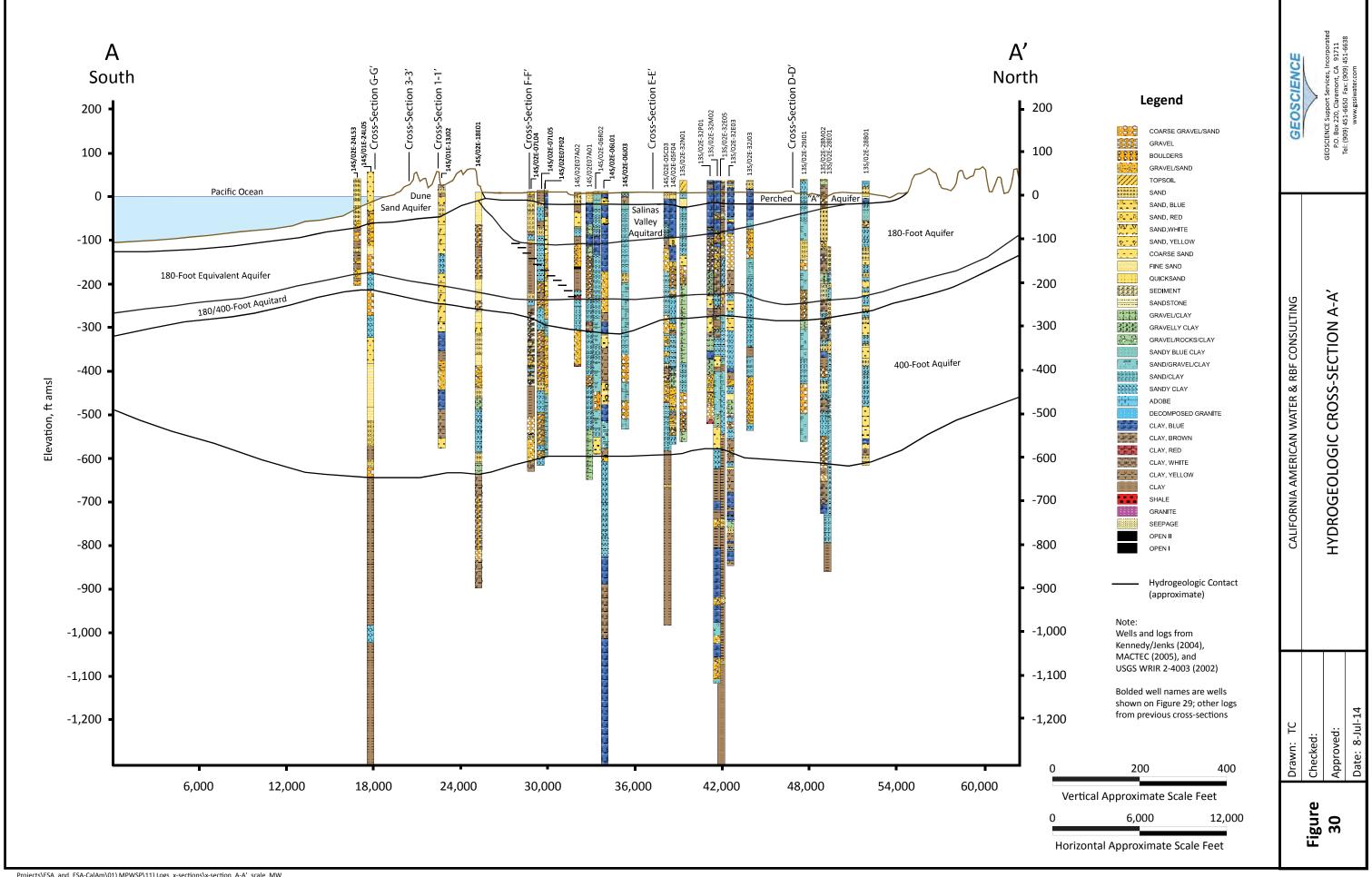
Attachment 1 - Technical Memorandum (TM 1) - Summary of Results - Exploratory Boreholes

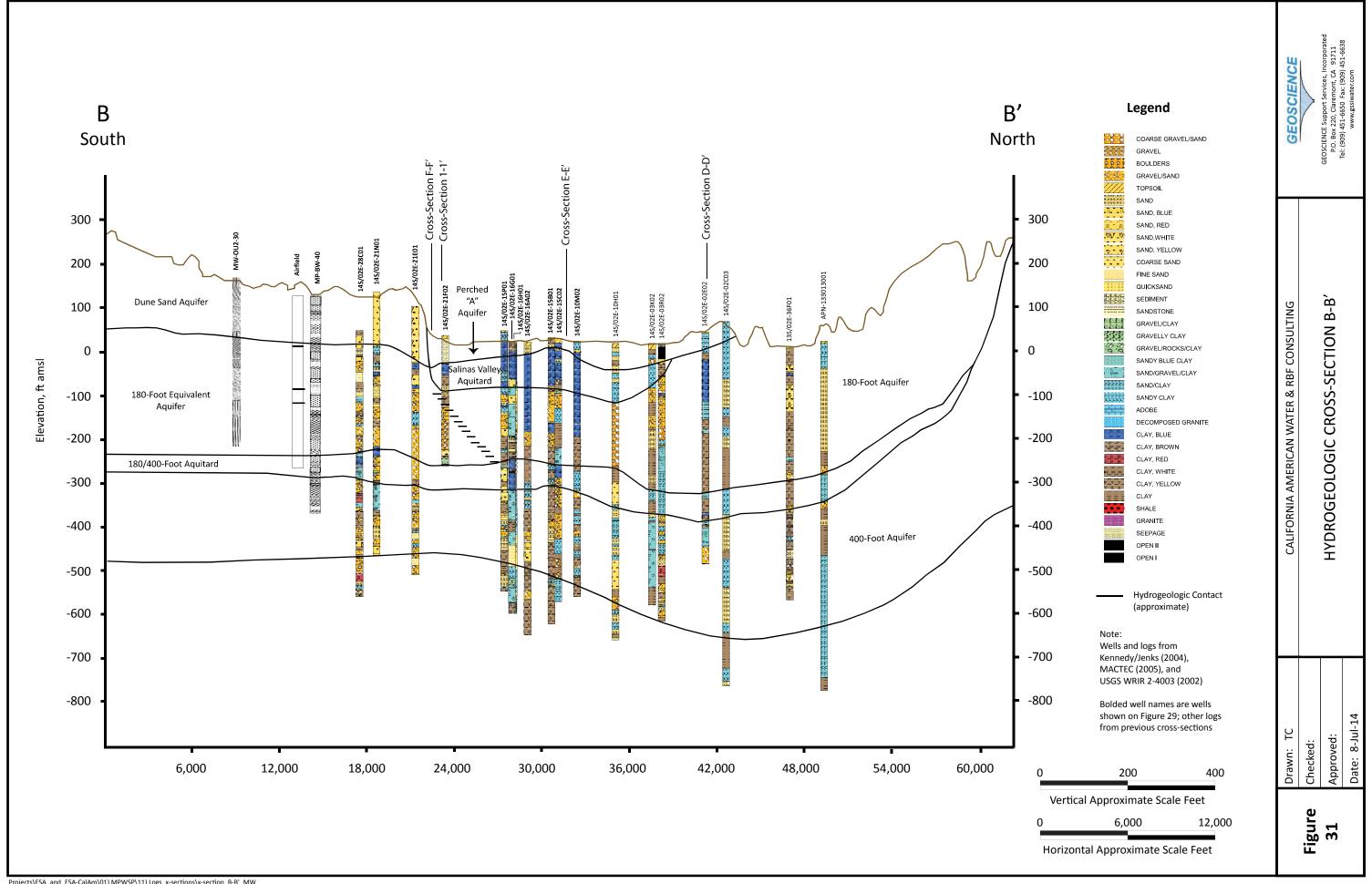


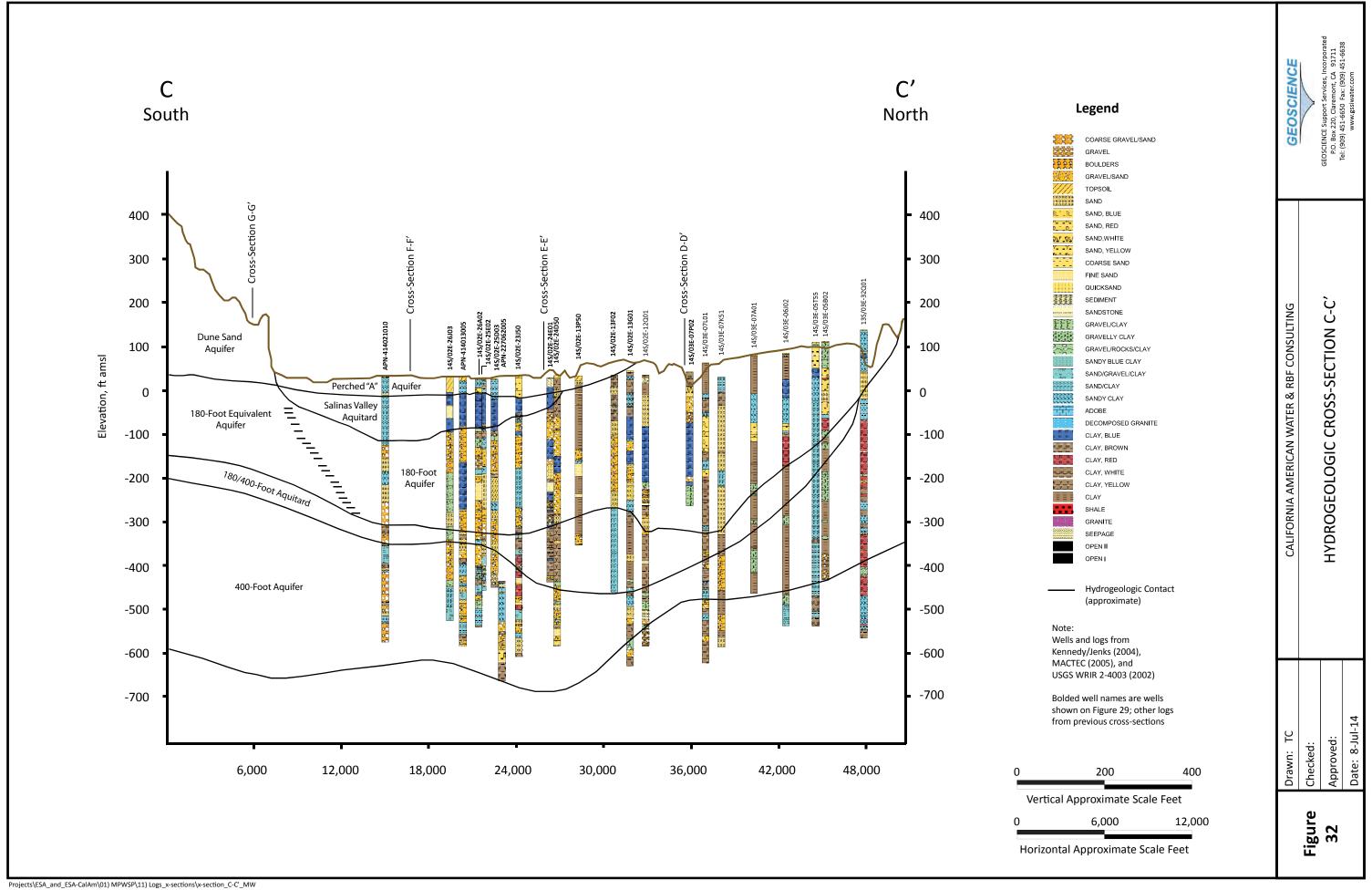
MONTEREY PENINSULA WATER SUPPLY PROJECT HYDROGEOLOGIC INVESTIGATION

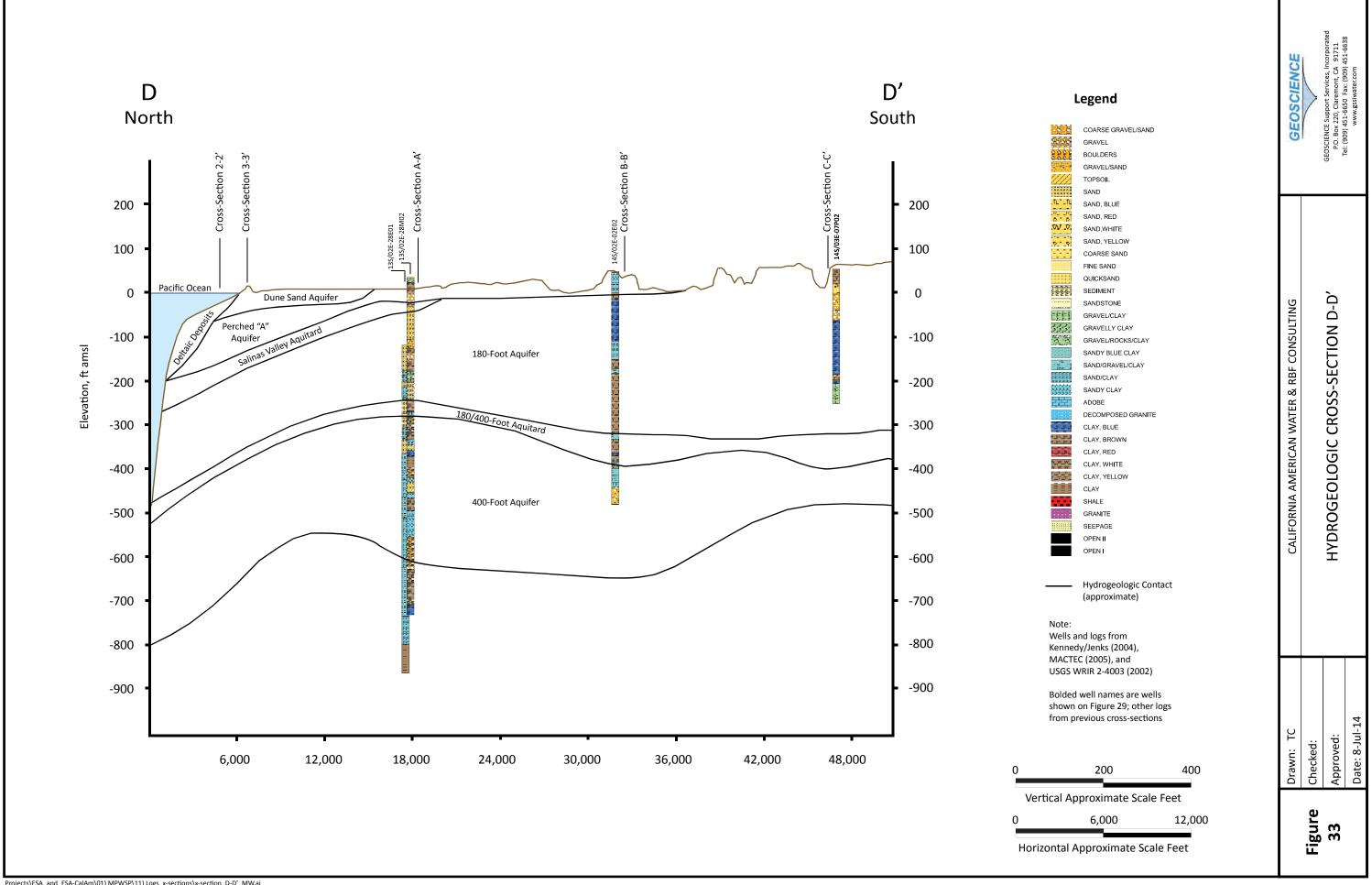


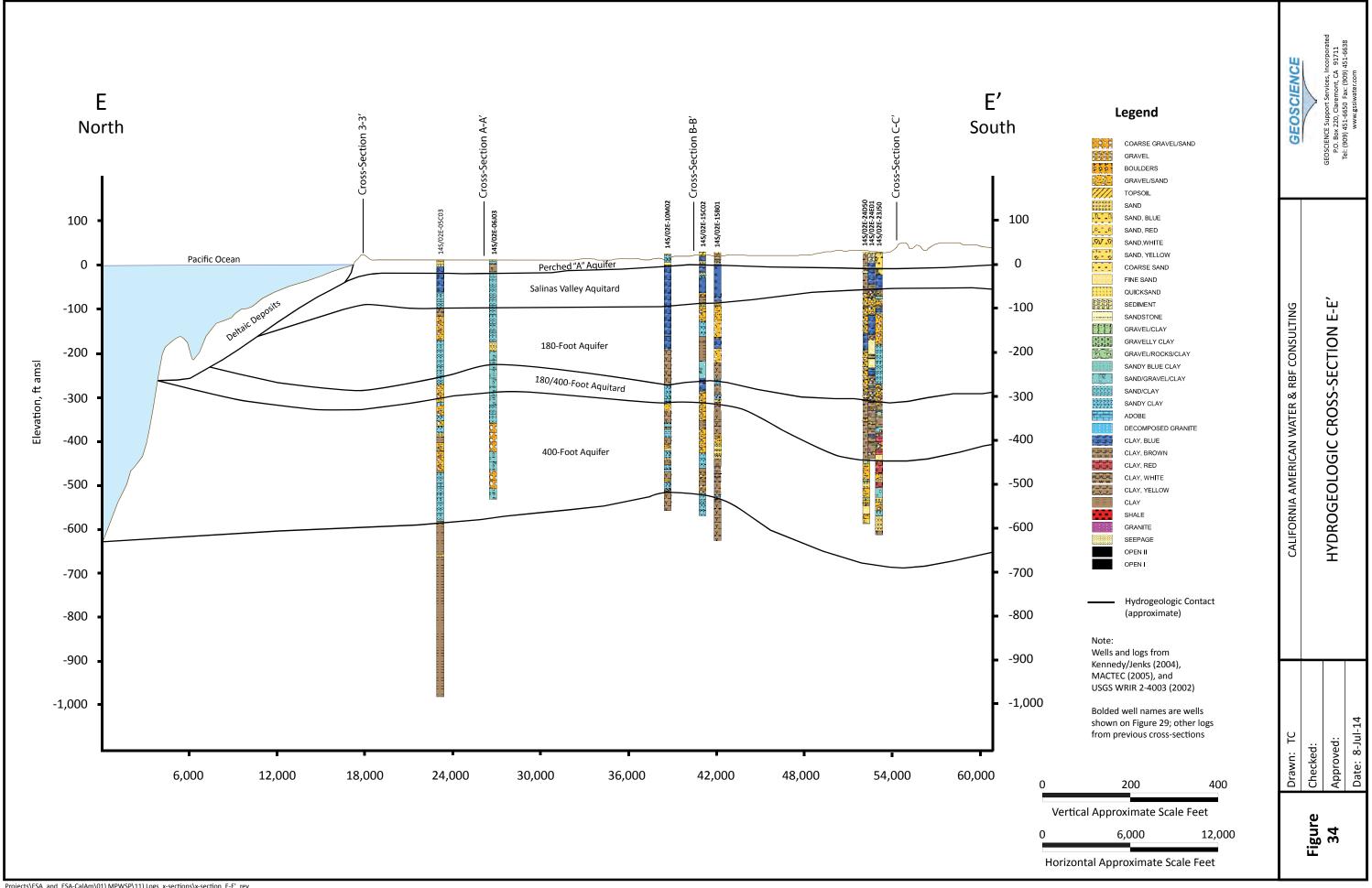


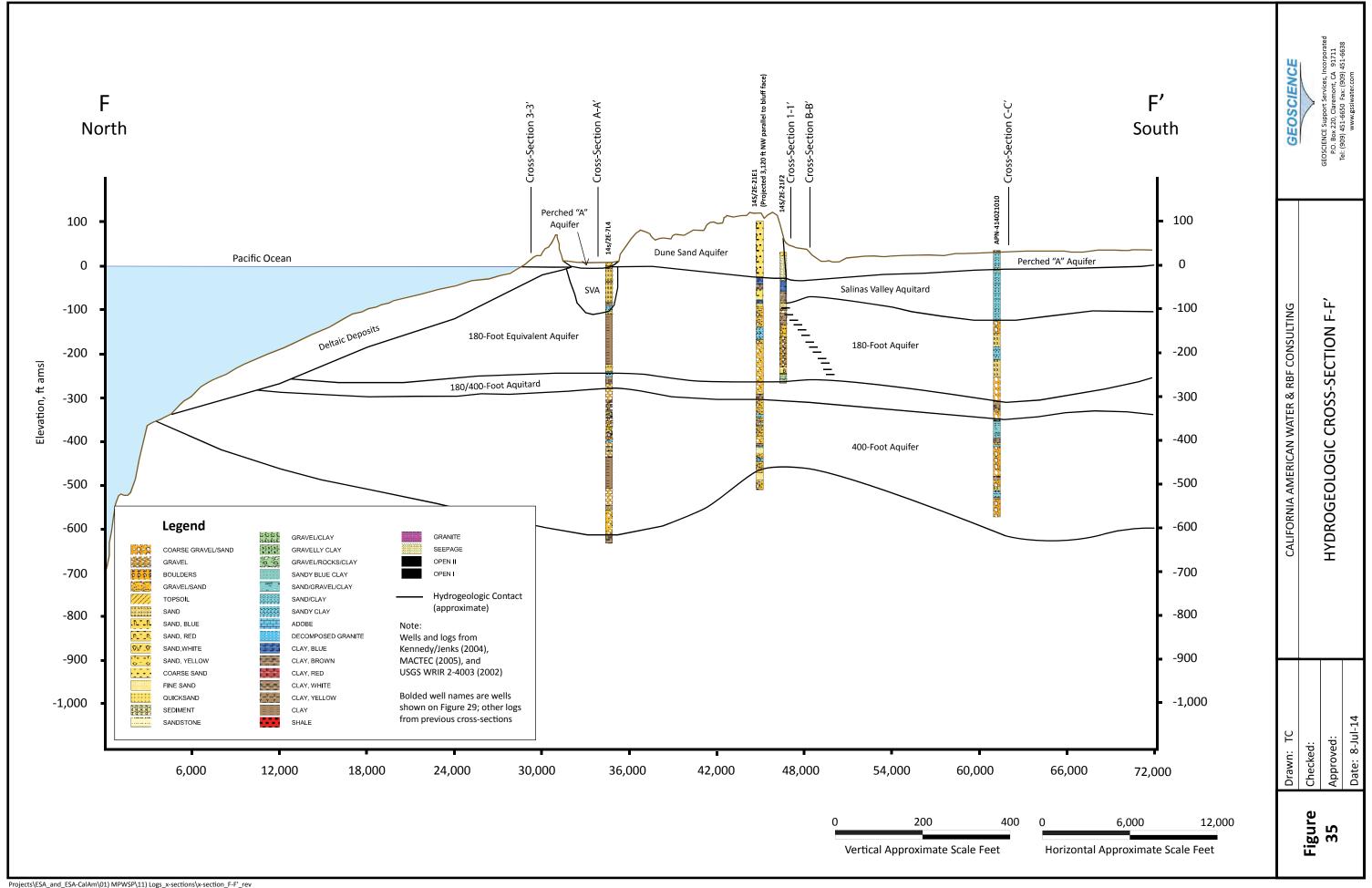


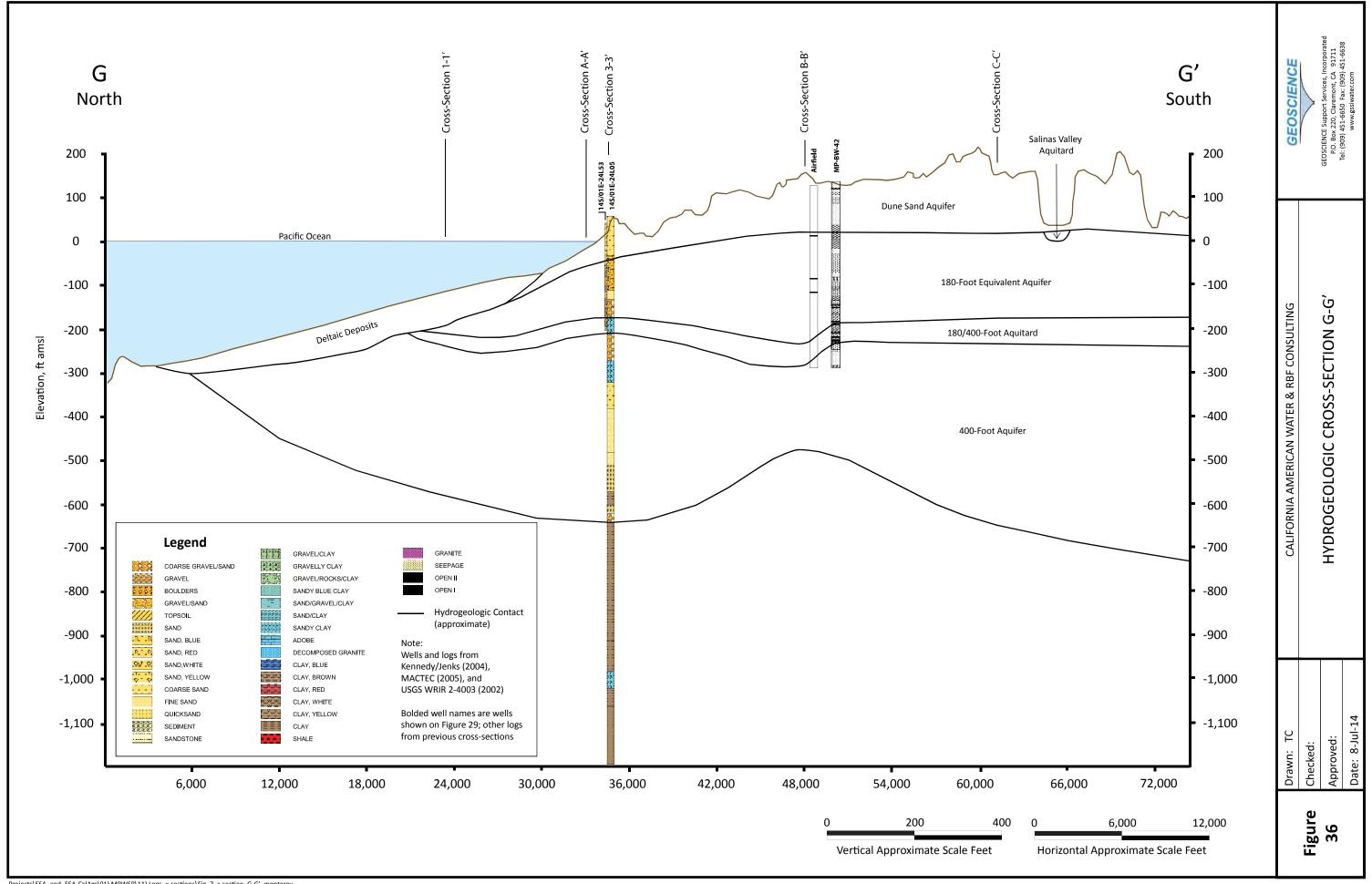


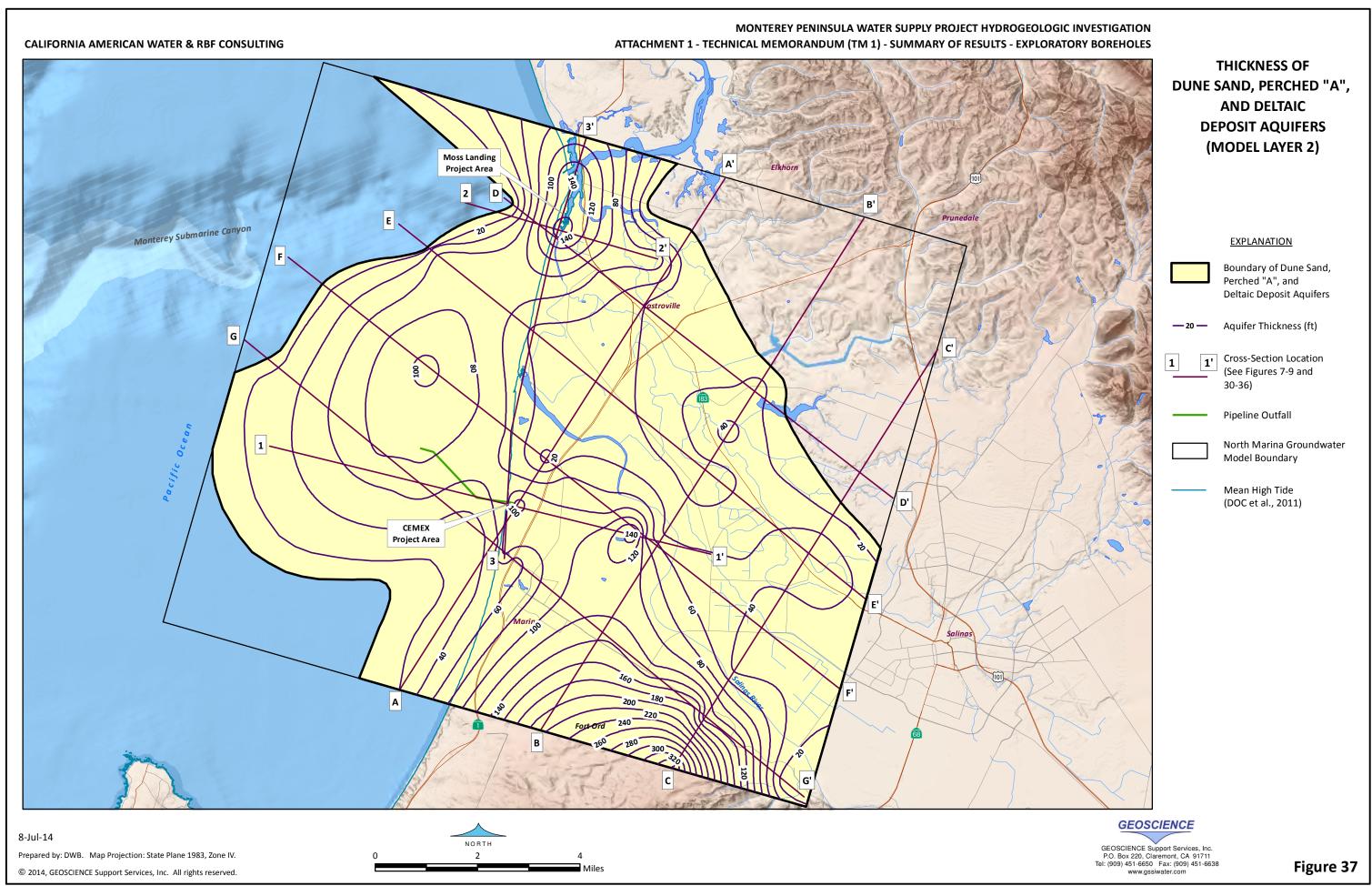


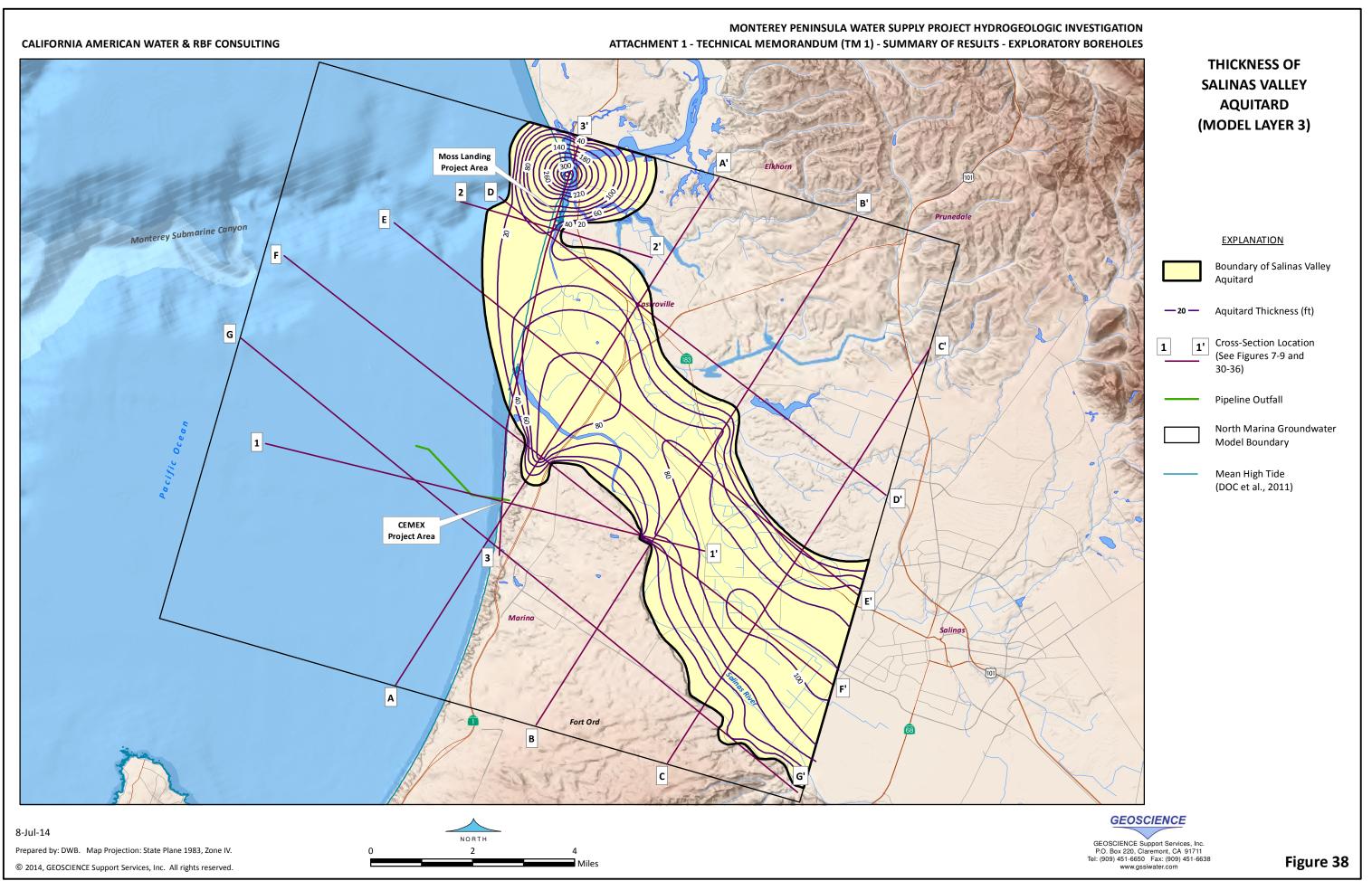


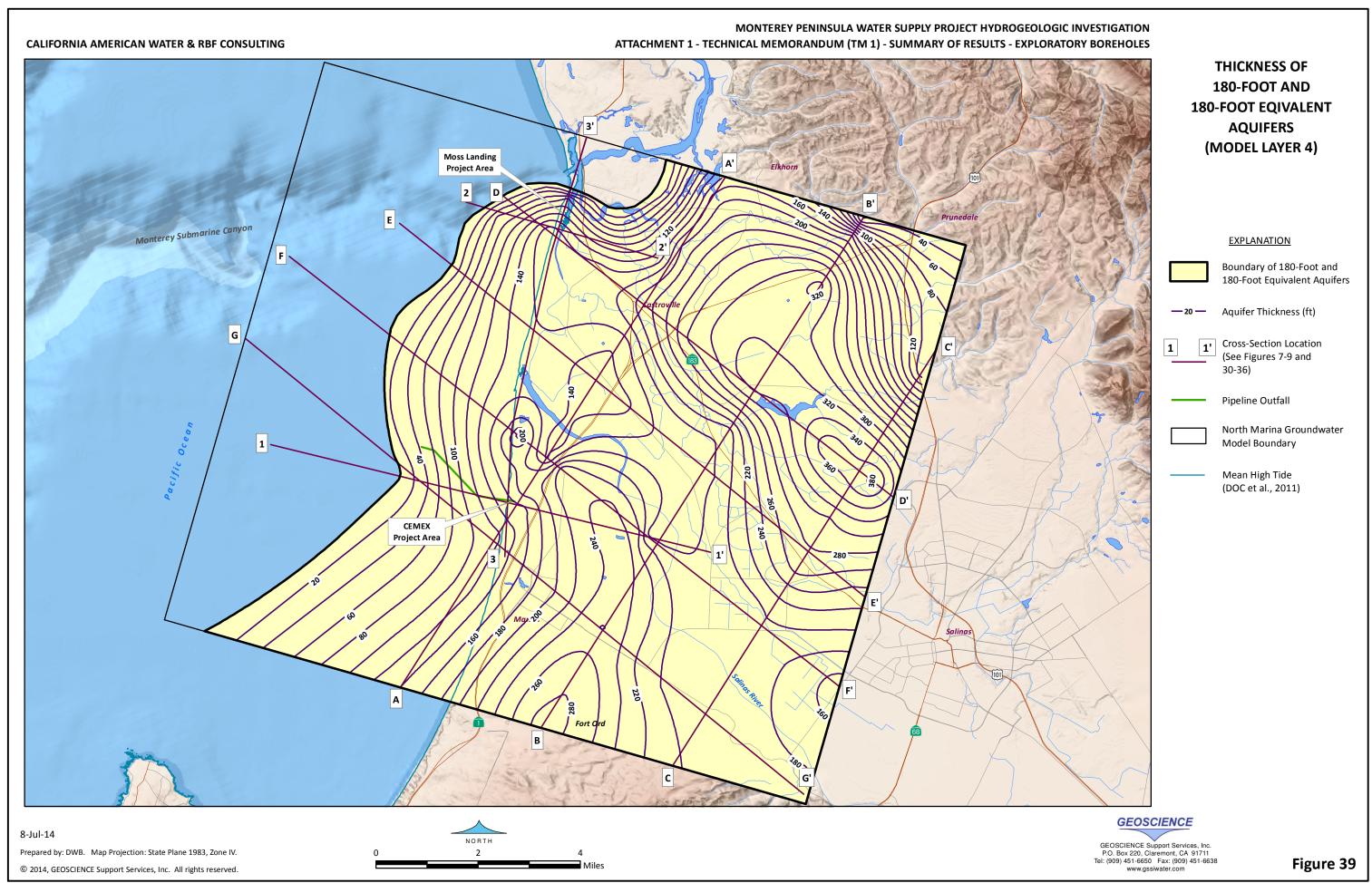


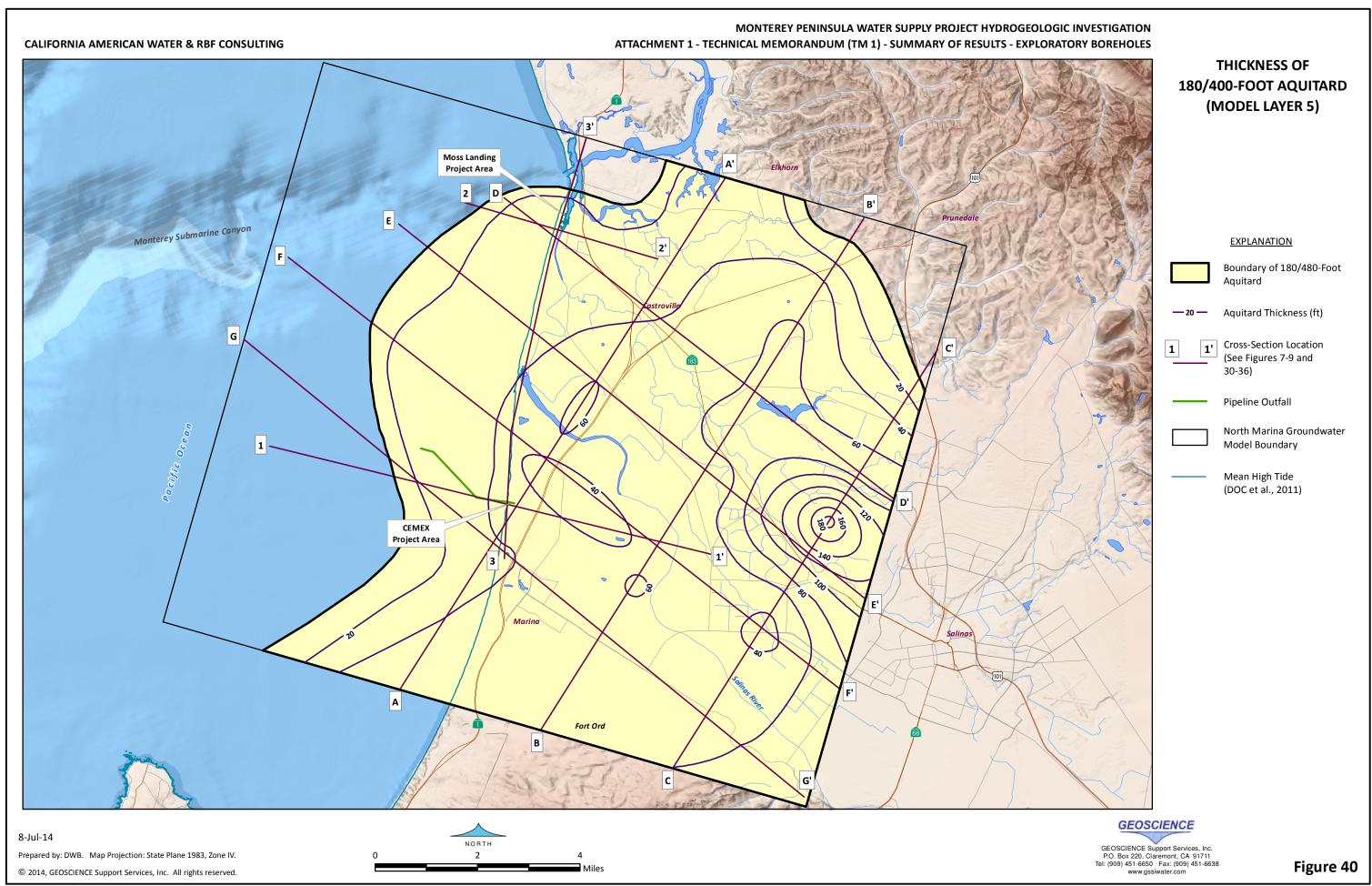


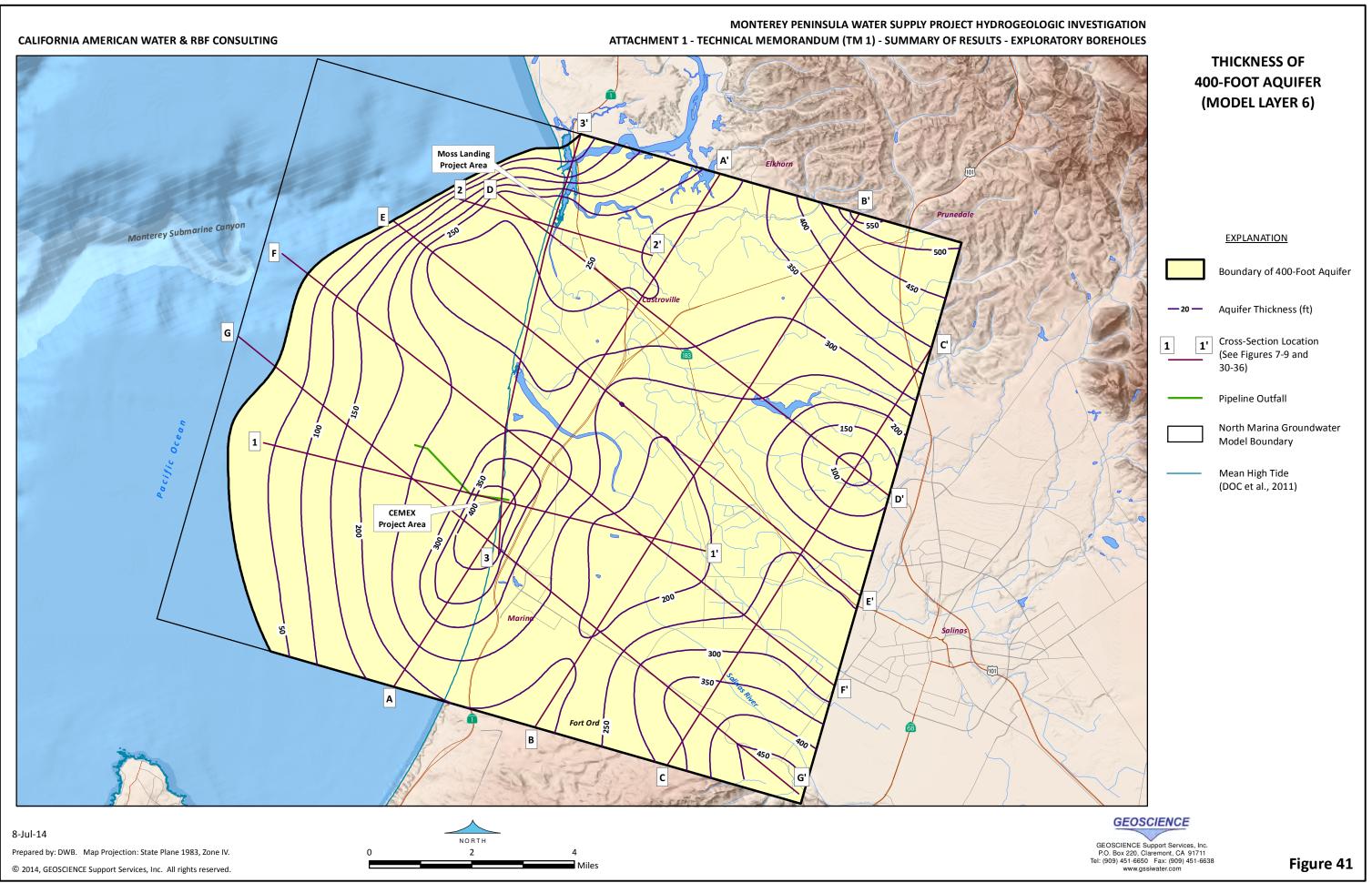


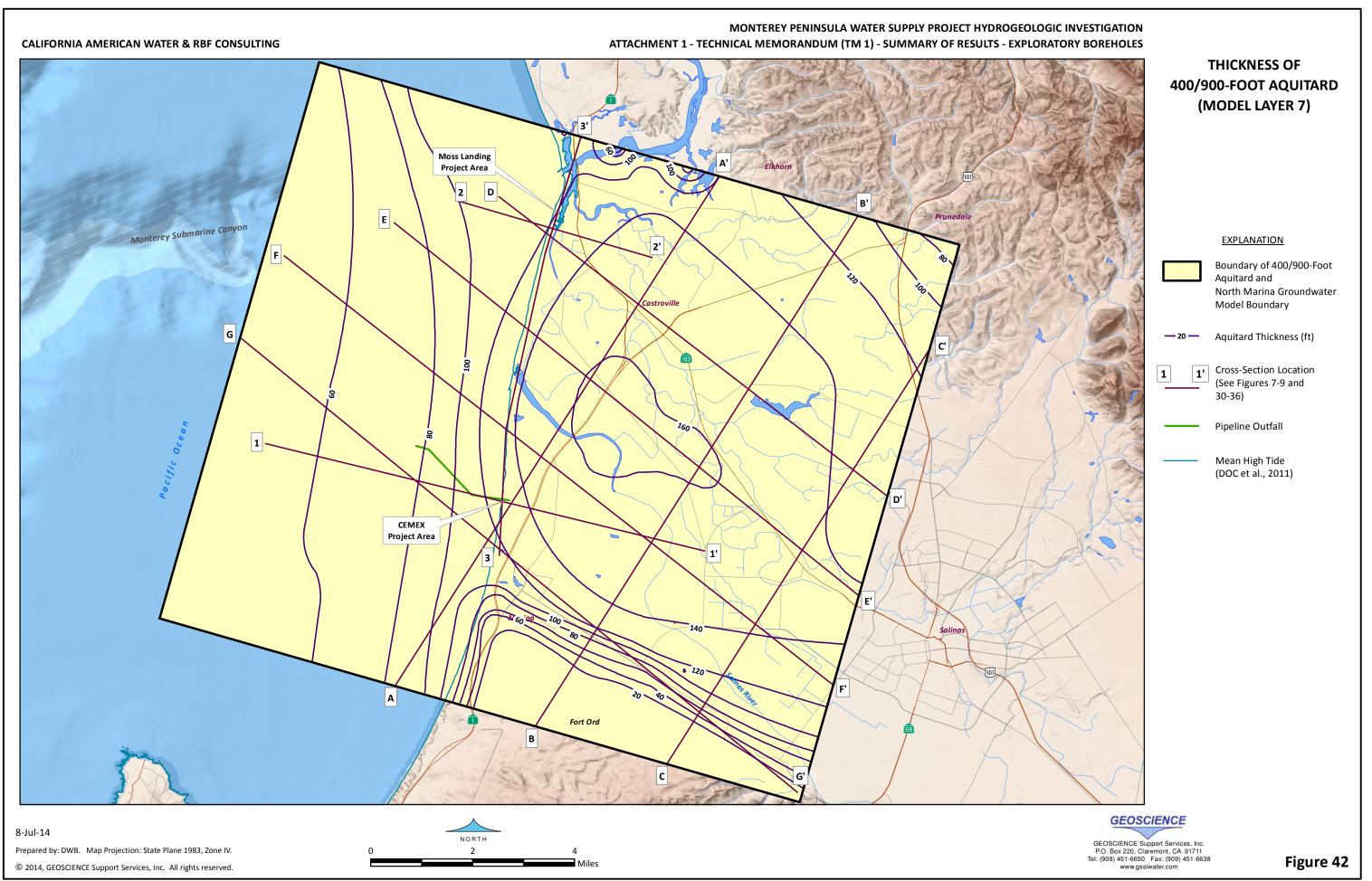


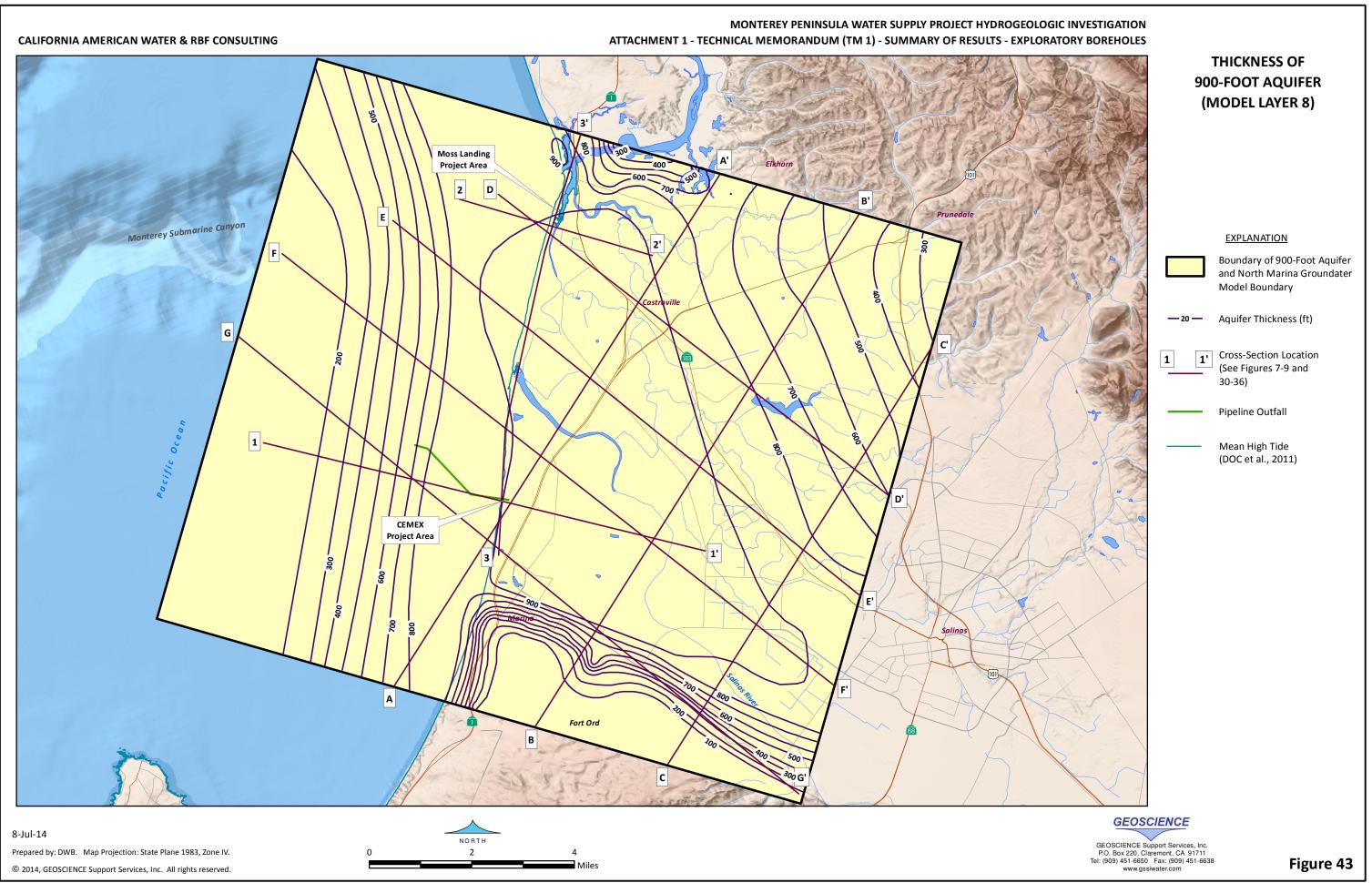










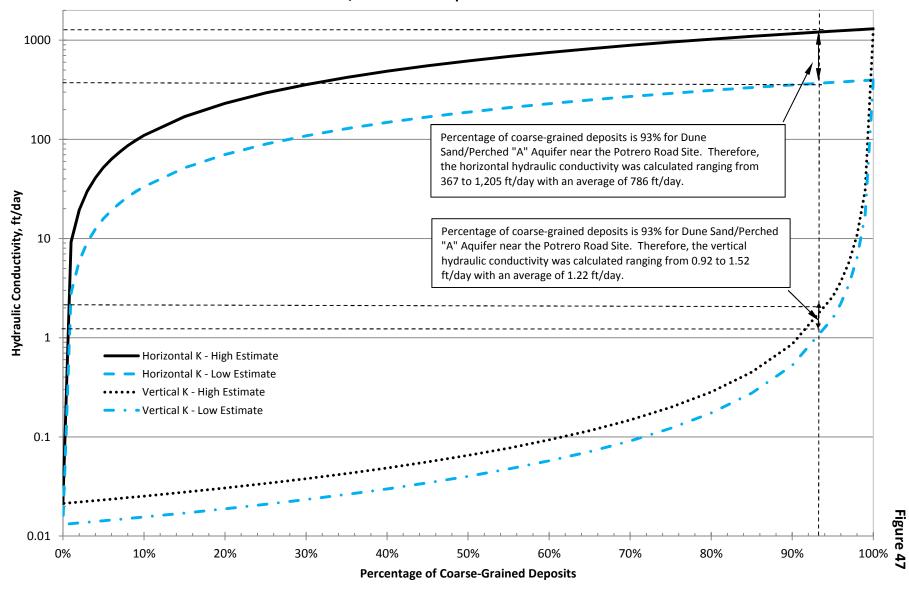


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Monterey Peninsula Water Supply Project Hydrogeologic Investigation

Attachment 1 - Technical Memorandum (TM 1) - Summary of Results - Exploratory Boreholes

Sediment Texture versus Horizontal and Vertical Hydraulic Conductivity Values Dune Sand/Perched "A" Aquifer near Potrero Road Site

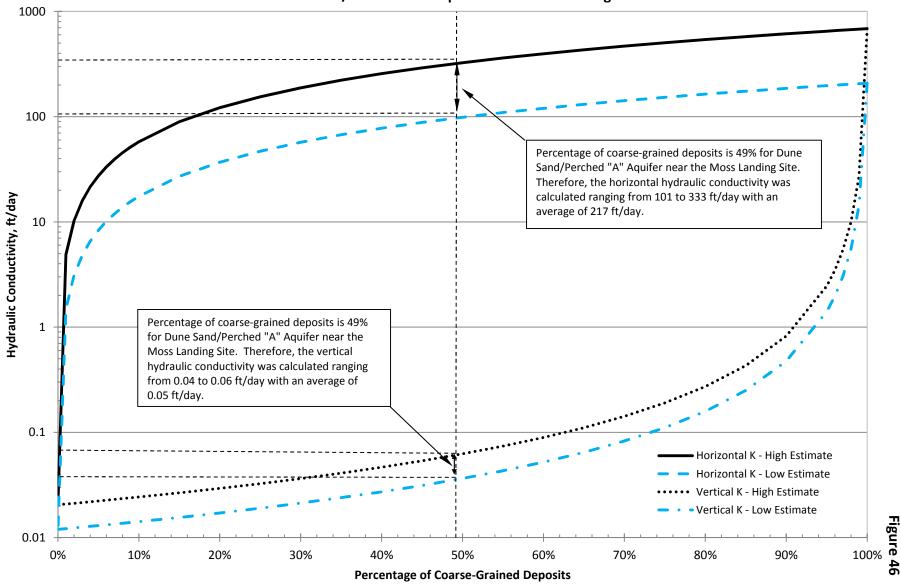


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Sediment Texture versus Horizontal and Vertical Hydraulic Conductivity Values Dune Sand/Perched "A" Aquifer near Moss Landing Site

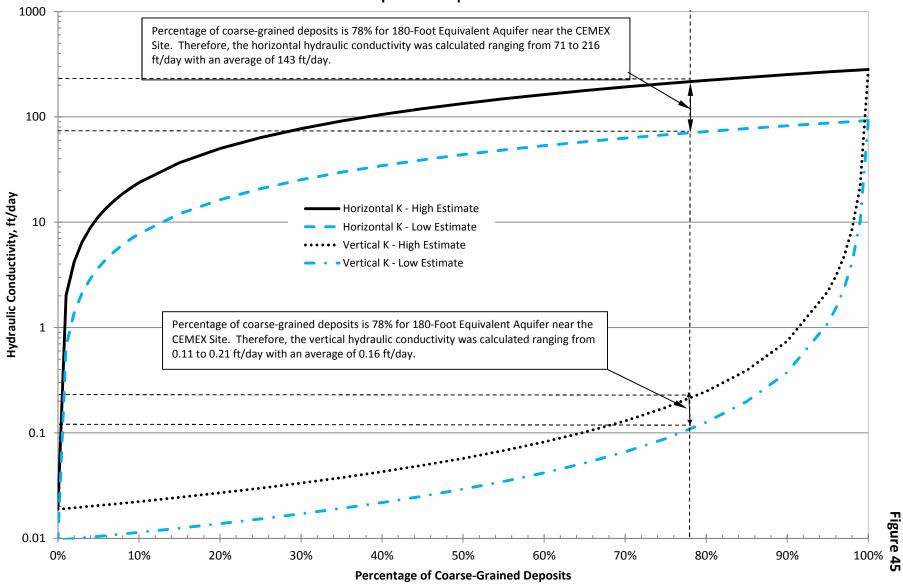


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Sediment Texture versus Horizontal and Vertical Hydraulic Conductivity Values 180-Foot Equivalent Aquifer near CEMEX Site

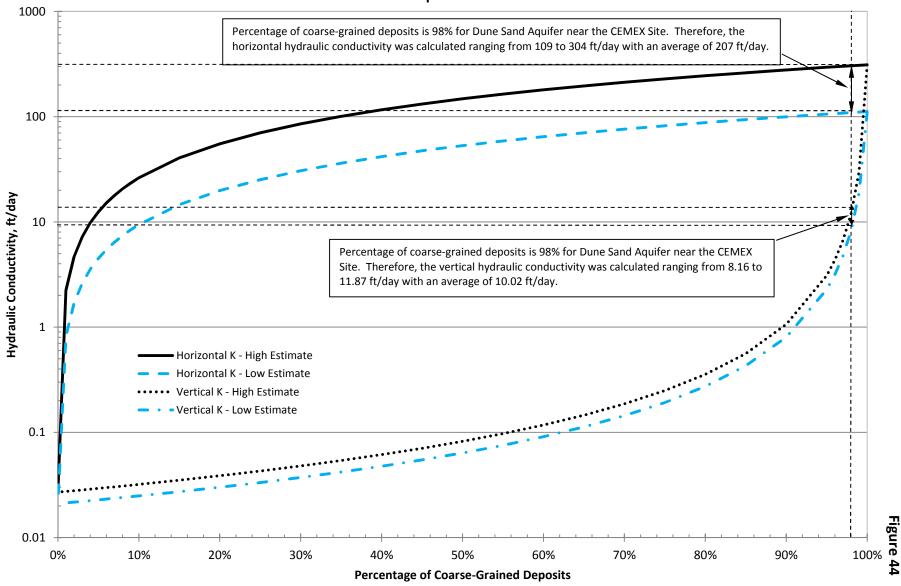


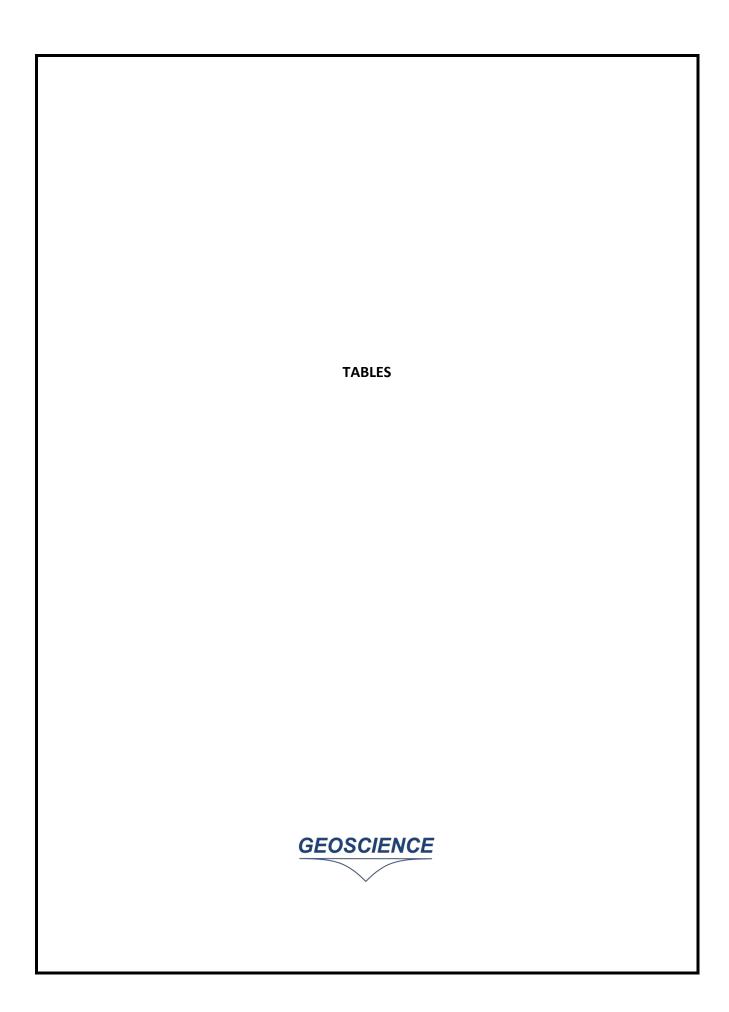
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Monterey Peninsula Water Supply Project Hydrogeologic Investigation

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Sediment Texture versus Horizontal and Vertical Hydraulic Conductivity Values Dune Sand Aquifer near CEMEX Site





Hydraulic Conductivity Calculations

Borehole	Interval [ft bgs]	Method	Sample Type	K Direction	Hydraulic Conductivity, K [ft/day]	Lithology
CX-B1	79-79.5	Hazen	MGA	Horizontal	86	SM: Silty Sand
CX-B1	79-79.5	Krumbein-Monk	MGA	Horizontal	45	SM: Silty Sand
CX-B1	79-79.5	Kozeny-Carman	MGA	Horizontal	130	SM: Silty Sand
				Average :	87	
CX-B1	88-88.5	Hazen	MGA	Horizontal	535	SW: Well-Graded Sand
CX-B1	88-88.5	Krumbein-Monk	MGA	Horizontal	491	SW: Well-Graded Sand
CX-B1	88-88.5	Kozeny-Carman	MGA	Horizontal	2,115	SW: Well-Graded Sand
				Average :	1,047	
CX-B1	104.5-105	Hazen	MGA	Horizontal	79	SM: Silty Sand
CX-B1	104.5-105	Krumbein-Monk	MGA	Horizontal	40	SM: Silty Sand
CX-B1	104.5-105	Kozeny-Carman	MGA	Horizontal	112	SM: Silty Sand
				Average :	77	
CX-B1	115-116	Hazen	MGA	Horizontal	351	SW: Well-Graded Sand
CX-B1	115-116	Krumbein-Monk	MGA	Horizontal	249	SW: Well-Graded Sand
CX-B1	115-116	Kozeny-Carman	MGA	Horizontal	624	SW: Well-Graded Sand
				Average :	408	
CX-B1	187-188	Hazen	MGA	Horizontal	150	SM: Silty Sand
CX-B1	187-188	Krumbein-Monk	MGA	Horizontal	127	SM: Silty Sand
CX-B1	187-188	Kozeny-Carman	MGA	Horizontal	344	SM: Silty Sand
				Average :	207	
CX-B1	245-245	Hazen	MGA	Horizontal	399	GW: Gravel
CX-B1	245-245	Krumbein-Monk	MGA	Horizontal	334	GW: Gravel
CX-B1	245-245	Kozeny-Carman	MGA	Horizontal	849	GW: Gravel
				Average :	527	
CX-B1	295-296	Hazen	MGA	Horizontal	176	SP: Sand with Gravel
CX-B1	295-296	Krumbein-Monk	MGA	Horizontal	176	SP: Sand with Gravel
CX-B1	295-296	Kozeny-Carman	MGA	Horizontal	549	SP: Sand with Gravel
				Average :	300	
CX-B2	53	Hazen	MGA	Horizontal	371	SW: Well-Graded Sand
CX-B2	53	Krumbein-Monk	MGA	Horizontal	292	SW: Well-Graded Sand
CX-B2	53	Kozeny-Carman	MGA	Horizontal	770	SW: Well-Graded Sand
				Average :	477	
CX-B2	116	Hazen	MGA	Horizontal	24	SM: Silty Sand
CX-B2	116	Krumbein-Monk	MGA	Horizontal	16	SM: Silty Sand
CX-B2	116	Kozeny-Carman	MGA	Horizontal	65	SM: Silty Sand
				Average :	35	
CX-B2	141	Hazen	MGA	Horizontal	117	SP: Sand
CX-B2	141	Krumbein-Monk	MGA	Horizontal	95	SP: Sand
CX-B2	141	Kozeny-Carman	MGA	Horizontal	241	SP: Sand
				Average :	151	
CX-B2	203	Hazen	MGA	Horizontal	102	SP: Sand

Borehole	Interval [ft bgs]	Method	Sample Type	K Direction	Hydraulic Conductivity, K [ft/day]	Lithology
CX-B2	203	Krumbein-Monk	MGA	Horizontal	72	SP: Sand
CX-B2	203	Kozeny-Carman	MGA	Horizontal	181	SP: Sand
				Average :	118	
CX-B2	273	Hazen	MGA	Horizontal	258	SW: Well-Graded Sand
CX-B2	273	Krumbein-Monk	MGA	Horizontal	206	SW: Well-Graded Sand
CX-B2	273	Kozeny-Carman	MGA	Horizontal	725	SW: Well-Graded Sand
				Average :	396	
CX-B3	45	Hazen	MGA	Horizontal	99	SP: Sand
CX-B3	45	Krumbein-Monk	MGA	Horizontal	74	SP: Sand
CX-B3	45	Kozeny-Carman	MGA	Horizontal	224	SP: Sand
				Average :	132	
CX-B3	121	Hazen	MGA	Horizontal	26	SM: Silty Sand
CX-B3	121	Krumbein-Monk	MGA	Horizontal	21	SM: Silty Sand
CX-B3	121	Kozeny-Carman	MGA	Horizontal	69	SM: Silty Sand
				Average :	39	
CX-B3	240	Hazen	MGA	Horizontal	191	SP: Sand
CX-B3	240	Krumbein-Monk	MGA	Horizontal	130	SP: Sand
CX-B3	240	Kozeny-Carman	MGA	Horizontal	509	SP: Sand
				Average :	277	
CX-B3	291	Hazen	MGA	Horizontal	373	SW: Well-Graded Sand
CX-B3	291	Krumbein-Monk	MGA	Horizontal	191	SW: Well-Graded Sand
CX-B3	291	Kozeny-Carman	MGA	Horizontal	829	SW: Well-Graded Sand
				Average :	464	
CX-B3	312	Hazen	MGA	Horizontal	258	SP: Sand
CX-B3	312	Krumbein-Monk	MGA	Horizontal	206	SP: Sand
CX-B3	312	Kozeny-Carman	MGA	Horizontal	725	SP: Sand
				Average :	396	
CX-B4	46-47	Hazen	MGA	Horizontal	374	SP: Sand
CX-B4	46-47	Krumbein-Monk	MGA	Horizontal	230	SP: Sand
CX-B4	46-47	Kozeny-Carman	MGA	Horizontal	628	SP: Sand
				Average :	411	
CX-B4	72-73	Hazen	MGA	Horizontal	45	SP: Sand
CX-B4	72-73	Krumbein-Monk	MGA	Horizontal	40	SP: Sand
CX-B4	72-73	Kozeny-Carman	MGA	Horizontal	102	SP: Sand
				Average :	62	
CX-B4	115-116	Hazen	MGA	Horizontal	31	SP: Sand
CX-B4	115-116	Krumbein-Monk	MGA	Horizontal	25	SP: Sand
CX-B4	115-116	Kozeny-Carman	MGA	Horizontal	74	SP: Sand
				Average :	43	
CX-B4	190-191	Hazen	MGA	Horizontal	121	SP: Sand
CX-B4	190-191	Krumbein-Monk	MGA	Horizontal	97	SP: Sand

Borehole	Interval [ft bgs]	Method	Sample Type	K Direction	Hydraulic Conductivity, K [ft/day]	Lithology
CX-B4	190-191	Kozeny-Carman	MGA	Horizontal	248	SP: Sand
				Average :	156	
CX-B4	248-249	Hazen	MGA	Horizontal	202	SP: Sand
CX-B4	248-249	Krumbein-Monk	MGA	Horizontal	163	SP: Sand
CX-B4	248-249	Kozeny-Carman	MGA	Horizontal	380	SP: Sand
				Average :	248	
MDW-1	22-23	Hazen	MGA	Horizontal	163	SP: Sand
MDW-1	22-23	Krumbein-Monk	MGA	Horizontal	135	SP: Sand
MDW-1	22-23	Kozeny-Carman	MGA	Horizontal	300	SP: Sand
				Average :	199	
MDW-1	59-60	Hazen	MGA	Horizontal	113	SP: Sand
MDW-1	59-60	Krumbein-Monk	MGA	Horizontal	90	SP: Sand
MDW-1	59-60	Kozeny-Carman	MGA	Horizontal	224	SP: Sand
				Average :	142	
MDW-1	70-71	Hazen	MGA	Horizontal	385	SP: Sand
MDW-1	70-71	Krumbein-Monk	MGA	Horizontal	250	SP: Sand
MDW-1	70-71	Kozeny-Carman	MGA	Horizontal	730	SP: Sand
				Average :	455	
MDW-1	153-154	Hazen	MGA	Horizontal	394	SP: Sand with Gravel
MDW-1	153-154	Krumbein-Monk	MGA	Horizontal	302	SP: Sand with Gravel
MDW-1	153-154	Kozeny-Carman	MGA	Horizontal	984	SP: Sand with Gravel
				Average :	560	
MDW-1	181-182	Hazen	MGA	Horizontal	202	SP: Sand
MDW-1	181-182	Krumbein-Monk	MGA	Horizontal	161	SP: Sand
MDW-1	181-182	Kozeny-Carman	MGA	Horizontal	553	SP: Sand
				Average :	305	
ML-1	52-53	Hazen	MGA	Horizontal	411	SP: Sand
ML-1	52-53	Krumbein-Monk	MGA	Horizontal	227	SP: Sand
ML-1	52-53	Kozeny-Carman	MGA	Horizontal	951	SP: Sand
				Average :	530	
ML-1	58-59	Hazen	MGA	Horizontal	75	SP: Sand
ML-1	58-59	Krumbein-Monk	MGA	Horizontal	51	SP: Sand
ML-1	58-59	Kozeny-Carman	MGA	Horizontal	124	SP: Sand
				Average :	83	
ML-1	65-66	Hazen	MGA	Horizontal	85	SP: Sand
ML-1	65-66	Krumbein-Monk	MGA	Horizontal	57	SP: Sand
ML-1	65-66	Kozeny-Carman	MGA	Horizontal	140	SP: Sand
				Average :	94	
ML-1	88-89	Hazen	MGA	Horizontal	185	SP: Sand
ML-1	88-89	Krumbein-Monk	MGA	Horizontal	134	SP: Sand
ML-1	88-89	Kozeny-Carman	MGA	Horizontal	521	SP: Sand

Borehole	Interval [ft bgs]	Method	Sample Type	K Direction	Hydraulic Conductivity, K [ft/day]	Lithology
				Average :	280	
ML-1	104-106	Hazen	MGA	Horizontal	125	SP: Sand
ML-1	104-106	Krumbein-Monk	MGA	Horizontal	93	SP: Sand
ML-1	104-106	Kozeny-Carman	MGA	Horizontal	312	SP: Sand
				Average :	177	
ML-1	108-109	Hazen	MGA	Horizontal	445	SP-SM: Sand with Silt and Gravel
ML-1	108-109	Krumbein-Monk	MGA	Horizontal	445	SP-SM: Sand with Silt and Gravel
ML-1	108-109	Kozeny-Carman	MGA	Horizontal	1,322	SP-SM: Sand with Silt and Gravel
				Average :	738	
ML-1	117-118	Hazen	MGA	Horizontal	469	SP: Sand with Gravel
ML-1	117-118	Krumbein-Monk	MGA	Horizontal	654	SP: Sand with Gravel
ML-1	117-118	Kozeny-Carman	MGA	Horizontal	1,175	SP: Sand with Gravel
				Average :	766	
ML-2	24-24.5	Hazen	MGA	Horizontal	497	SW: Well-Graded Sand
ML-2	24-24.5	Krumbein-Monk	MGA	Horizontal	383	SW: Well-Graded Sand
ML-2	24-24.5	Kozeny-Carman	MGA	Horizontal	1,090	SW: Well-Graded Sand
				Average :	656	
ML-2	50-50.5	Hazen	MGA	Horizontal	92	SP: Sand
ML-2	50-50.5	Krumbein-Monk	MGA	Horizontal	56	SP: Sand
ML-2	50-50.5	Kozeny-Carman	MGA	Horizontal	151	SP: Sand
				Average :	100	
ML-2	110.5-111	Hazen	MGA	Horizontal	517	SW: Well-Graded Sand with Gravel
ML-2	110.5-111	Krumbein-Monk	MGA	Horizontal	484	SW: Well-Graded Sand with Gravel
ML-2	110.5-111	Kozeny-Carman	MGA	Horizontal	949	SW: Well-Graded Sand with Gravel
				Average :	650	
ML-2	152-152.5	Hazen	MGA	Horizontal	21	SP: Sand
ML-2	152-152.5	Krumbein-Monk	MGA	Horizontal	12	SP: Sand
ML-2	152-152.5	Kozeny-Carman	MGA	Horizontal	53	SP: Sand
				Average :	29	
ML-2	188.5-189	Hazen	MGA	Horizontal	30	SP-SM: Sand with Silt
ML-2	188.5-189	Krumbein-Monk	MGA	Horizontal	18	SP-SM: Sand with Silt
ML-2	188.5-189	Kozeny-Carman	MGA	Horizontal	93	SP-SM: Sand with Silt
				Average :	47	
ML-3	109.5-110	Hazen	MGA	Horizontal	95	SP: Sand
ML-3	109.5-110	Krumbein-Monk	MGA	Horizontal	60	SP: Sand
ML-3	109.5-110	Kozeny-Carman	MGA	Horizontal	214	SP: Sand
				Average :	123	
ML-3	111.5-112	Hazen	MGA	Horizontal	337	SP: Sand
ML-3	111.5-112	Krumbein-Monk	MGA	Horizontal	273	SP: Sand
ML-3	111.5-112	Kozeny-Carman	MGA	Horizontal	914	SP: Sand
				Average :	508	

Borehole	Interval [ft bgs]	Method	Sample Type	K Direction	Hydraulic Conductivity, K [ft/day]	Lithology
ML-3	182.5-183	Hazen	MGA	Horizontal	446	SW-SC: Sand with Clay and Gravel
ML-3	182.5-183	Krumbein-Monk	MGA	Horizontal	452	SW-SC: Sand with Clay and Gravel
ML-3	182.5-183	Kozeny-Carman	MGA	Horizontal	1,511	SW-SC: Sand with Clay and Gravel
				Average :	803	
ML-3	189-189.5	Hazen	MGA	Horizontal	118	SP: Sand
ML-3	189-189.5	Krumbein-Monk	MGA	Horizontal	95	SP: Sand
ML-3	189-189.5	Kozeny-Carman	MGA	Horizontal	355	SP: Sand
				Average :	189	
ML-3	195-195.5	Hazen	MGA	Horizontal	192	SW: Well-Graded Sand with Gravel
ML-3	195-195.5	Krumbein-Monk	MGA	Horizontal	367	SW: Well-Graded Sand with Gravel
ML-3	195-195.5	Kozeny-Carman	MGA	Horizontal	480	SW: Well-Graded Sand with Gravel
				Average :	346	
ML-4	28-28.5	Hazen	MGA	Horizontal	164	SP: Sand
ML-4	28-28.5	Krumbein-Monk	MGA	Horizontal	171	SP: Sand
ML-4	28-28.5	Kozeny-Carman	MGA	Horizontal	468	SP: Sand
				Average :	268	
ML-4	71-71.5	Hazen	MGA	Horizontal	25	SP: Sand
ML-4	71-71.5	Krumbein-Monk	MGA	Horizontal	21	SP: Sand
ML-4	71-71.5	Kozeny-Carman	MGA	Horizontal	79	SP: Sand
				Average :	42	
ML-4	112-112.5	Hazen	MGA	Horizontal	152	SP: Sand
ML-4	112-112.5	Krumbein-Monk	MGA	Horizontal	129	SP: Sand
ML-4	112-112.5	Kozeny-Carman	MGA	Horizontal	345	SP: Sand
				Average :	208	
ML-4	152-152.5	Hazen	MGA	Horizontal	189	SP: Sand
ML-4	152-152.5	Krumbein-Monk	MGA	Horizontal	229	SP: Sand
ML-4	152-152.5	Kozeny-Carman	MGA	Horizontal	785	SP: Sand
				Average :	401	
ML-4	180-180.5	Hazen	MGA	Horizontal	89	SP: Sand
ML-4	180-180.5	Krumbein-Monk	MGA	Horizontal	63	SP: Sand
ML-4	180-180.5	Kozeny-Carman	MGA	Horizontal	296	SP: Sand
				Average :	149	
ML-6	94-94.5	Hazen	MGA	Horizontal	48	SP-SM: Sand with Silt
ML-6	94-94.5	Krumbein-Monk	MGA	Horizontal	49	SP-SM: Sand with Silt
ML-6	94-94.5	Kozeny-Carman	MGA	Horizontal	178	SP-SM: Sand with Silt
				Average :	91	
ML-6	104-104.5	Hazen	MGA	Horizontal	306	SW: Well-Graded Sand
ML-6	104-104.5	Krumbein-Monk	MGA	Horizontal	149	SW: Well-Graded Sand
ML-6	104-104.5	Kozeny-Carman	MGA	Horizontal	610	SW: Well-Graded Sand
				Average :	355	
ML-6	121-121.5	Hazen	MGA	Horizontal	37	SP: Sand

Borehole	Interval [ft bgs]	Method	Sample Type	K Direction	Hydraulic Conductivity, K [ft/day]	Lithology
ML-6	121-121.5	Krumbein-Monk	MGA	Horizontal	28	SP: Sand
ML-6	121-121.5	Kozeny-Carman	MGA	Horizontal	83	SP: Sand
				Average :	49	
ML-6	141-141.5	Hazen	MGA	Horizontal	36	SP: Sand
ML-6	141-141.5	Krumbein-Monk	MGA	Horizontal	29	SP: Sand
ML-6	141-141.5	Kozeny-Carman	MGA	Horizontal	88	SP: Sand
				Average :	51	
ML-6	166-166.5	Hazen	MGA	Horizontal	43	SP: Sand
ML-6	166-166.5	Krumbein-Monk	MGA	Horizontal	38	SP: Sand
ML-6	166-166.5	Kozeny-Carman	MGA	Horizontal	106	SP: Sand
				Average :	62	
PR-1	56-57	Hazen	MGA	Horizontal	271	SP: Sand
PR-1	56-57	Krumbein-Monk	MGA	Horizontal	165	SP: Sand
PR-1	56-57	Kozeny-Carman	MGA	Horizontal	396	SP: Sand
				Average :	277	
PR-1	66-67	Hazen	MGA	Horizontal	328	SP: Sand with Gravel
PR-1	66-67	Krumbein-Monk	MGA	Horizontal	302	SP: Sand with Gravel
PR-1	66-67	Kozeny-Carman	MGA	Horizontal	561	SP: Sand with Gravel
				Average :	397	
PR-1	76-77	Hazen	MGA	Horizontal	311	SM: Silty Sand with Gravel
PR-1	76-77	Krumbein-Monk	MGA	Horizontal	836	SM: Silty Sand with Gravel
PR-1	76-77	Kozeny-Carman	MGA	Horizontal	1,150	SM: Silty Sand with Gravel
				Average :	766	
PR-1	110-111	Hazen	MGA	Horizontal	699	SW: Well-Graded Sand with Gravel
PR-1	110-111	Krumbein-Monk	MGA	Horizontal	703	SW: Well-Graded Sand with Gravel
PR-1	110-111	Kozeny-Carman	MGA	Horizontal	1,148	SW: Well-Graded Sand with Gravel
				Average :	850	
PR-1	124-125	Hazen	MGA	Horizontal	1,055	SW: Well-Graded Sand
PR-1	124-125	Krumbein-Monk	MGA	Horizontal	9,561	SW: Well-Graded Sand
PR-1	124-125	Kozeny-Carman	MGA	Horizontal	2,579	SW: Well-Graded Sand
				Average :	4,398	
PR-1	188-189	Hazen	MGA	Horizontal	160	SM: Silty Sand
PR-1	188-189	Krumbein-Monk	MGA	Horizontal	160	SM: Silty Sand
PR-1	188-189	Kozeny-Carman	MGA	Horizontal	429	SM: Silty Sand
				Average :	249	
PR-1	197-198	Hazen	MGA	Horizontal	170	SM: Silty Sand
PR-1	197-198	Krumbein-Monk	MGA	Horizontal	132	SM: Silty Sand
PR-1	197-198	Kozeny-Carman	MGA	Horizontal	413	SM: Silty Sand
				Average :	238	

Summary of Horizontal and Vertical Permeability Test

Borehole	Interval [ft bgs]	Method	Sample Type	K Direction	Permeability, K [ft/day]	Lithology
CX-B1	66.5-67	EPA9100	Core	Vertical	0.782	SM: Silty Sand
CX-B1	66.5-67	EPA9100	Core	Horizontal	4.337	SM: Silty Sand
CX-B1	166.5-167	EPA9100	Core	Vertical	1.380	SM: Silty Sand
CX-B1	166.5-167	EPA9100	Core	Horizontal	1.729	SM: Silty Sand
CX-B1	257.5-258	EPA9100	Core	Vertical	0.005	CL: Clay
CX-B2	207.5-208	EPA9100	Core	Vertical	10.657	SP: Sand
CX-B2	207.5-208	EPA9100	Core	Horizontal	3.997	SP: Sand
CX-B2	259-259.5	EPA9100	Core	Vertical	0.005	CL: Clay
CX-B3	107.5-108	EPA9100	Core	Vertical	14.909	SP: Sand with Gravel
CX-B3	107.5-108	EPA9100	Core	Horizontal	14.512	SP: Sand with Gravel
CX-B3	129-129.5	EPA9100	Core	Vertical	0.008	CH: Fat Clay
CX-B3	197.5-198	EPA9100	Core	Vertical	0.283	SP: Sand
CX-B3	197.5-198	EPA9100	Core	Horizontal	1.797	SP: Sand
ML-1	76-76.5	EPA9100	Core	Vertical	0.014	CH: Fat Clay
ML-1	107.5-108	EPA9100	Core	Vertical	24.149	SP-SM: Sand with Silt and Gravel
ML-1	107.5-108	EPA9100	Core	Horizontal	17.744	SP-SM: Sand with Silt and Gravel
ML-1	147-147.5	EPA9100	Core	Vertical	0.006	CL: Clay
ML-2	87-87.5	EPA9100	Core	Vertical	0.283	CL: Clay
ML-2	117.5-118	EPA9100	Core	Vertical	0.133	SP-SM: Sand with Silt
ML-2	117.5-118	EPA9100	Core	Horizontal	0.312	SP-SM: Sand with Silt
ML-2	157.5-158	EPA9100	Core	Vertical	0.312	SP: Sand
ML-2	157.5-158	EPA9100	Core	Horizontal	9.099	SP: Sand
ML-3	106.5-107	EPA9100	Core	Vertical	5.300	SP: Sand
ML-3	106.5-107	EPA9100	Core	Horizontal	2.387	SP: Sand
ML-3	166.5-167	EPA9100	Core	Vertical	0.027	ML: Silt

Table 2

Summary of Horizontal and Vertical Permeability Test

Borehole	Interval [ft bgs]	Method	Sample Type	K Direction	Permeability, K [ft/day]	Lithology
ML-3	166.5-167	EPA9100	Core	Horizontal	0.021	ML: Silt
ML-4	76.5-77	EPA9100	Core	Vertical	2.690	SP: Sand
ML-4	76.5-77	EPA9100	Core	Horizontal	2.460	SP: Sand
ML-4	126.5-127	EPA9100	Core	Vertical	0.003	CH: Fat Clay
ML-4	146.5-147	EPA9100	Core	Vertical	17.290	SP: Sand
ML-4	146.5-147	EPA9100	Core	Horizontal	36.564	SP: Sand
ML-6	79.5-80	EPA9100	Core	Vertical	0.007	CL: Clay
ML-6	107.5-108	EPA9100	Core	Vertical	13.180	SW: Well-Graded Sand with Gravel
ML-6	107.5-108	EPA9100	Core	Horizontal	11.338	SW: Well-Graded Sand with Gravel
ML-6	167.5-168	EPA9100	Core	Vertical	0.205	SM: Silty Sand
ML-6	167.5-168	EPA9100	Core	Horizontal	0.368	SM: Silty Sand
PR-1	67-67.5	EPA 9100	Core	Vertical	0.259	SP: Sand with Gravel
PR-1	67-67.5	EPA 9100	Core	Horizontal	0.171	SP: Sand with Gravel
PR-1	145.5-146	EPA 9100	Core	Vertical	0.006	CL: Clay
PR-1	152-152.5	EPA 9100	Core	Vertical	0.006	CL: Clay
PR-1	200.5-201	EPA 9100	Core	Vertical	14.456	Not Determined
PR-1	200.5-201	EPA 9100	Core	Horizontal	0.774	Not Determined

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Property Property					ML-1 ML-2					MI 2								
Proceedings		Borehole:	PF		MI		M		M	1	M		М			T	T	,
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12,47 Temperspersoners				ND	ND	ND	ND						ND	ND	ND	ND	ND	ND
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1,3 Delichoramene ed 9gh	-				ND				ND	ND		ND	ND	ND				
1,3 Definengement		μg/L	4.6	4.8	4.7	4.8	4.6	7.81	9.69	10.1	4.8	8.06	4.6	4.8	5.3	4.9	5.0	5.1
3.3.5-Friendly-beneame	1,2-Dichloroethane	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
3,3 Getteshensemen		μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
1,3,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,	1,3,5-Trimethylbenzene	μg/L				ND		ND	ND	ND	ND			ND		ND		ND
3.50-bridge-proposed 1.50-bridge-proposed 1.50-bridge-proposed	1,3-Dichlorobenzene	μg/L			ND				ND			ND	ND					·
13-Directive Performence 14/L 5.2 5.1 5.6 5.3 4.6 5.0 5.1 5.5 5.3 4.7 5.0 5.5 4.7 5.0 5.1 4.7 5.0		μg/L																
1.4Decinforderseries	1 1 1																	
1462 PATIONED ROME 1874	,											_						
12-20-CM 16/4 NO				ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND				
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2-Butanone 1g/L ND ND ND ND ND ND ND N	*										†				•			+
2-Chlorotelyvinyl ether 14g/L - - - - - - - ND ND												_						
2-Chiorotoluene		-			-	-	-				-		-	-	-	-	-	
2-Hesnane			ND	ND	ND	ND	ND				ND		ND	ND	ND	ND	ND	ND
3-Hydroxycarbofuran 14g/L ND ND ND ND ND ND ND N	2-Hexanone	10,							ND				ND					
4,4°-DDD	3,5-Dichlorobenzoic acid	μg/L	-	-	-	-	-	-	ND	ND	-	ND	-	-	-	-	-	-
4,4°-DDE 1g/L	3-Hydroxycarbofuran	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
4,4°-DDT μg/L ND	4,4´-DDD	μg/L	-	-	-	-	-	-	ND	ND	-	ND	-	-	ND	ND	ND	ND
4-Chlorotoluene	4,4´-DDE	μg/L	-	-	-	-	-	-	ND	ND	-	ND	-	-		ND		ND
4-Methyl-2-pentanone μg/L ND	4,4´-DDT																	
Acetone rig/L ND ND ND ND ND ND ND N																		
Aciflurfen μg/L ND	4-Methyl-2-pentanone							ND	ND	ND		ND						
Alachlor μg/L ND	Acetone									-								
Aldicarb Sulfone IIII ND ND ND ND ND ND																		
Addicarb Sulfone μg/L ND																		<u> </u>
Addicarb Sulfoxide μg/L ND																		<u> </u>
Aldrin μg/L ND																		<u> </u>
Alkalinity as CaCO3 mg/L 190 150 330 320 750 180 210 190 460 200 560 410 158 176 149 118 alpha-BHC μg/L ND ND ND - ND ND - ND																		<u> </u>
alpha-BHC μg/L ND ND - ND																		
Aluminum μg/L ND 68 ND 150 82 ND 950 47 ND 17 52 ND 120 62 147 ND ND Ammonia as N, Dissolved mg/L 0.14 0.78 15 7.5 14 1.0 10 1.7 9.5 1.7 6.8 1.9 ND 3.22 3.40 ND ND AMPA μg/L 110 110 110 110 100 87 100 95 - 100 95 95 93 100 110 110 110 110 Aroclor 1221 μg/L ND	·	•					-											
Ammonia as N, Dissolved mg/L 0.14 0.78 15 7.5 14 1.0 10 1.7 9.5 1.7 6.8 1.9 ND 3.22 3.40 ND AMPA μg/L 110 110 110 110 100 87 100 95 - 100 95 93 100 110 110 110 110 Arcolor 1211 μg/L ND ND ND - ND ND - ND							82											
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	Aroclor 1221			-	-	-	-	-			†		-	-				· · · · · · · · · · · · · · · · · · ·
	Aroclor 1232		-	-	-	-	-	-			-		-	-				·

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	Borehole:	PF	R-1	M		MI		MI		MI		М	L-6		MD		
	Zone #:	1	2	1	2	1	2	1	2	1	2	1	2	1	2	3	4
Screen Inter		190 - 200	125 - 135	113.5 - 118.5	90 - 100	167 - 177	90 - 100	180 - 190	103 - 113	163.5 - 173.5	74.5 - 84.5	152 - 162	100 - 110	237 - 247	187 - 197	152 - 162	60 - 70
Constituent ¹	Units	24-Sep-13 Result	25-Sep-13 Result	5-Oct-13 Result	7-Oct-13 Result	17-Dec-13 Result	19-Dec-13 Result	11-Jan-14 Result	13-Jan-14 Result	5-Dec-13 Result	6-Dec-13 Result	22-Nov-13 Result	23-Nov-13 Result	1-May-14 Result	7-May-14 Result	8-May-14 Result	10-May-14 Result
Aroclor 1242	μg/L	-	- result	- Result	-	-	-	ND	ND	- result	ND	- result	- result	ND	ND	ND	ND
Aroclor 1248	μg/L	-	_	_	-	-	-	ND	ND	-	ND	_	-	ND	ND	ND	ND
Aroclor 1254	μg/L	-	_	_	-	-	-	ND	ND	-	ND	-	-	ND	ND	ND	ND
Aroclor 1260	μg/L	-	-	-	-	-	-	ND	ND	-	ND	-	-	ND	ND	ND	ND
Arsenic, Total	μg/L	ND	13	3.4	ND	ND	ND	1.0	5.1	ND	0.71	4.5	4.3	39	54	44	40
Atrazine	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Barium, Dissolved	μg/L	110	ND	160	270	74	380	150	92	84	340	ND	89	94	93	134	ND
Bentazon	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Benzene	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Benzo(a)pyrene	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
beta-BHC	μg/L	-	-	-	-	-	-	ND	ND	-	ND	-	-	ND	ND	ND	ND
Bicarbonate as CaCO3	mg/L	190	150	330	320	750	180	-	-	460	-	560	410	-	-	-	-
Bicarbonate as HCO3	mg/L	- ND	- ND	- ND	- ND	- ND	- ND	250	230 ND	- ND	240 ND	- ND	- ND	193	215 ND	182 ND	144 ND
Bis(2-ethylhexyl) adipate (DEHA) Bis(2-ethylhexyl) phthalate (DEHP)	μg/L μg/L	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND 4.0	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND
Boron, Dissolved	μg/L μg/L	ND ND	4300	2100	450	1700	400	500	450	1100	190	4000	3300	1570	3000	1680	2800
Bromacil	μg/L μg/L	ND ND	4300 ND	ND	ND	ND	400 ND	ND	ND	ND	ND	4000 ND	ND	ND	ND	ND	ND
Bromide, Dissolved	mg/L	0.80	65	43	5.7	45	14	13	7.7	43	16	68	59	54.0	52	40.0	32.4
Bromobenzene	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Bromochloromethane	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Bromodichloromethane	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Bromofluorobenzene	μg/L	4.9	5.0	5.0	4.9	51	7.70	8.54	9.13	51	9.69	52	53	50	51	52	53
Bromoform	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Bromomethane	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Butachlor	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Calcium, Dissolved	mg/L	50	400	590	180	620	460	391	254	850	730	570	600	1183	662	1012	264
Calcium, Total	mg/L	52	340	590	180	570	450	409	259	860	734	550	580	1211	676	973	257
Captan	μg/L	- ND	- ND	- ND	- ND	- ND	- ND	ND	ND	- ND	ND	- ND	- ND	- ND	- ND	- ND	- ND
Carbaturan	μg/L	ND	ND ND	ND	ND	ND	ND	ND ND	ND	ND ND	ND	ND ND	ND ND	ND	ND	ND	ND
Carbofuran Carbon Tetrachloride	μg/L μg/L	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND
Carbonate as CaCO3	mg/L	ND ND	ND ND	ND ND	ND	ND	ND ND	ND	ND	ND ND	ND ND	ND	ND ND	ND	ND	ND ND	ND ND
Chlordane	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Chloride, Dissolved	mg/L	250	19000	12000	1600	12000	3900	-	-	10000	-	19000	16000	16100	16600	13300	11200
Chloride, Total	mg/L	-	-	-	-	-	-	3700	2300	-	4600	-	-	-	-	-	-
Chlorobenzene	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Chloroethane	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Chloroform	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Chloromethane	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Chloropropham	μg/L	-	-	-	-	-	-	ND	ND	-	ND	-	-	-	-	-	=
Chlorothalonil	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
cis-1,2-Dichloroethene	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
cis-1,3-Dichloropropene	μg/L	ND 5.0	ND 30	ND	ND	ND	ND 10	ND	ND	ND	ND	ND	ND	ND	ND 50	ND 25	ND
Color	CU	5.0 1080	20 44440	250 29716	30 545	45 29650	10 9635	ND 10507	ND 6701	40 26437	ND 11141	20 40389	10 35246	23 36237	50 38793	25 31014	15 26662
Conductivity (Field) Copper, Total	μS/cm μg/L	ND	54	37	ND	38	15	10507	3.4	37	11141	58	58	210	201	219	152
Cyanazine	μg/L μg/L	- -	-	-	-	-	- 15	ND	ND	-	ND	-	-	-	-	- 219	-
Dalapon	μg/L μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND .	ND ND	ND	ND	ND	ND	ND	ND
DCPA	μg/L	-	-	-	-	-	-	ND	ND	-	ND	-	-	-	-	-	-
DCPAA	μg/L	71	63	46	48	49	47	-	-	47	-	47	46	42	62	66	64
Decachlorobiphenyl	μg/L	-	-	-	-	-	-	0.0228	0.0295	-	0.0788	-	-	39%	0.0206	0.00734	0.0650
Delta Oxygen-18	δ ¹⁸ O (‰)	-6.4	-0.5	-	-	-3.1	-5.3	-6.0	-6.4	-3.6	-5.2	-0.6	-1.3	-2.0	-1.0	-2.2	-2.5
delta-BHC	μg/L	-	-	-	-	-	-	ND	ND	-	ND	-	-	ND ND	ND	ND ND	ND ND
Delta-Deuterium	δ ² H (‰)	-42.0	-3.0	_	-	-19.2	-37.6	-40.1	-43.6	-24.5	-35.9	-5.5	-11.0	-13	-9	-16	-19
Diazinon	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
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				ML-1 ML-2													
	Borehole:	PF	R-1	MI				•	L-3		L-4	•	L-6			W-1	1
	Zone #:	1	2	1	2	1	2	1	2	1	2	1	2	1	2	3	4
Screen Inter		190 - 200	125 - 135	113.5 - 118.5	90 - 100	167 - 177	90 - 100	180 - 190	103 - 113	163.5 - 173.5	74.5 - 84.5	152 - 162	100 - 110	237 - 247	187 - 197	152 - 162	60 - 70
1	mple Date:	24-Sep-13	25-Sep-13	5-Oct-13	7-Oct-13	17-Dec-13	19-Dec-13	11-Jan-14	13-Jan-14	5-Dec-13	6-Dec-13	22-Nov-13	23-Nov-13	1-May-14	7-May-14	8-May-14	10-May-14
Constituent ¹	Units	Result	Result	Result	Result	Result	Result	Result	Result	Result	Result	Result	Result	Result	Result	Result	Result
Dibromochloromethane	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Dibromochloropropane (DBCP)	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Dibromomethane	μg/L	ND ND	ND ND	ND ND	ND	ND	ND	ND ND	ND	ND	ND	ND ND	ND	ND ND	ND ND	ND ND	ND ND
Dicamba Dichloroacetate	μg/L	10.6	539	108	ND 10.8	ND 100	ND 25.3	0.5	ND 0.505	ND 140	ND 0.48	132	ND 131	ND -	ND -	ND -	ND -
Dichlorodifluoromethane (Freon 12)	mg/L μg/L	ND	ND	ND	ND	ND	25.3 ND	ND	0.505 ND	ND	0.48 ND	ND	ND	- ND	- ND	- ND	- ND
Dichloromethane	μg/L μg/L	ND ND	ND ND	ND ND	ND	ND	ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND
Dichloroprop	μg/L μg/L	-	-	-	-	-	-	ND ND	ND ND	- ND	ND ND	-	-	IND -	-	-	-
Dieldrin	μg/L	ND	ND	ND	ND	ND	ND	ND ND	ND ND	ND	ND ND	ND	ND	ND	ND	ND	ND
Di-isopropyl ether (DIPE)	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Dimethoate	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Dinoseb	μg/L	ND	ND	ND	ND	ND	ND	ND ND	ND ND	ND	ND	ND ND	ND ND	ND	ND	ND	ND
Dioxin (2,3,7,8 TCDD)	pg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	-	ND	ND	ND	ND	ND	ND
Diphenamid	μg/L	-	-	-	-	-	-	ND	ND	-	ND	-	-	-	-	-	-
Diquat	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Dissolved Oxygen (Field)	mg/L	N/A	N/A	N/A	N/A	0	0	3.7	0.1	0	0.1	0.1	0.1	0.2	0.2	0.1	2.5
Disulfoton	μg/L	-	-	-	-	-	-	ND	ND	-	ND	-	-	-	-	-	-
Endosulfan I	μg/L	-	-	-	-	-	-	ND	ND	-	ND	-	-	ND	ND	ND	ND
Endosulfan II	μg/L	-	-	-	-	-	-	ND	ND	-	ND	-	-	ND	ND	ND	ND
Endosulfan sulfate	μg/L	-	-	-	-	-	-	ND	ND	-	ND	-	-	ND	ND	ND	ND
Endothall	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Endrin	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Endrin aldehyde	μg/L	-	-	-	-	-	-	ND	ND	-	ND	-	-	ND	ND	ND	ND
EPTC	μg/L	-	-	-	-	i	1	ND	ND	-	ND	-	-	-	-	-	-
Ethyl tert-Butyl Ether (ETBE)	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Ethylbenzene	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Ethylene Dibromide (EDB)	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Fluoride, Dissolved	mg/L	0.10	ND	0.12	0.20	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	0.6
gamma-BHC (Lindane)	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Glyphosate	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Hardness as CaCO3	mg/L	240	5300	4700	920	4800	2500	1020	647	6100	1830	6400	6000	8208	6658	6498	3887
Heptachlor	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Heptachlor Epoxide	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Hexachlorobenzene	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Hexachlorobutadiene	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Hexachlorocyclopentadiene	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Hydroxide as CaCO3	mg/L	ND	ND	ND	ND	ND 020	ND	ND 100	ND 200	ND 640	ND	ND 630	ND 200	ND	ND	ND	ND
lodide, Dissolved	μg/L	64 ND	ND	ND	180	920 ND	360	100	200	640	51	620	380	ND 205	ND 12050	ND	ND
Iron, Dissolved	μg/L	ND	ND 650	6000	ND 1800	ND 2000	140	ND 6000	1700	ND 1200	ND 10000	ND 2000	ND EGO	365	13059	20051	ND
Iron, Total	μg/L	200 ND	650	20000	1800	3000	500	6900	3500	1200	10000	3900	560	492	13532	26720	178
Isopropylbenzene Lithium	μg/L	ND 27	ND 150	ND 140	ND 34	ND 270	ND 78	ND 110	ND 86	ND 240	ND 01	ND 390	ND 330	ND 226	ND 153	ND 120	ND 142
	μg/L μg/L	ND	ND	ND	ND	ND	78 ND	110 ND	ND	ND ND	91 ND	390 ND	ND	ND	ND	ND	142 ND
m,p-Xylenes Magnesium, Dissolved	μg/L mg/L	27	1200	810	110	900	360	298	173	970	507	1200	1100	1211	1168	1020	796
Magnesium, Dissolved	mg/L mg/L	28	1100	780	110	820	340	310	173	960	512	1200	1100	1211	1207	988	796 788
Manganese, Dissolved	mg/L μg/L	180	1700	5200	790	2600	710	1400	1300	6400	5000	3900	3600	1605	4694	6512	ND
Manganese, Total	μg/L μg/L	190	1500	5300	790	2400	680	1500	1400	6400	5100	3800	3500	1653	4817	6303	ND ND
Mass Balance, Total	μg/L meg/L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Mass Balance-Dissolved Anions	meq/L	12	580	380	51	390	120	-	-	320	-	590	500	504	520	416	351
Mass Balance-Dissolved Cations	meq/L	11	570	360	50	380	120	-	-	340	-	550	480	497	507	452	370
MBAS (Surfactants)	mg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Methiocarb	μg/L	-	-	-	-	-	-	ND	ND	-	ND	-	-	ND	ND	ND	ND
Methomyl	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Methoxychlor	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Methyl tert-butyl ether (MTBE)	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
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	1				MI 2					MI C							
	Borehole:	PR		MI		MI			L-3	MI			L-6			W-1	ı
	Zone #:	1	2	1	2	1	2	1	2	1	2	1	2	1	2	3	4
Screen Interv		190 - 200	125 - 135	113.5 - 118.5	90 - 100	167 - 177	90 - 100	180 - 190	103 - 113	163.5 - 173.5	74.5 - 84.5	152 - 162	100 - 110	237 - 247	187 - 197	152 - 162	60 - 70
	nple Date:	24-Sep-13	25-Sep-13	5-Oct-13	7-Oct-13	17-Dec-13	19-Dec-13	11-Jan-14	13-Jan-14	5-Dec-13	6-Dec-13	22-Nov-13	23-Nov-13	1-May-14	7-May-14	8-May-14	10-May-14
Constituent ¹	Units	Result	Result	Result	Result	Result	Result	Result	Result	Result	Result	Result	Result	Result	Result	Result	Result
Metolachlor	μg/L	ND	ND	ND ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Metribuzin	μg/L	ND ND	ND ND	ND ND	ND ND	ND ND	ND	ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND
Molinate Naphthalene	μg/L	ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND
<u> </u>	μg/L	ND	ND ND	ND ND	ND ND	ND ND	ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND	ND ND
n-Butylbenzene Nitrate as NO3	μg/L mg/L	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND	2	18	8
Nitrate as NO3	mg/L	-	-	-	-	-	-	ND ND	ND ND	-	ND ND	-	-	ND ND	0.5	4.2	1.8
Nitrite as NO2-N, Dissolved	mg/L	ND	ND	ND	ND	ND	ND	-	-	ND	-	ND	ND	ND	ND	ND	ND
n-Propylbenzene	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Odor	TON	2.0	10	20	50	1.0	1.0	4.0	2.0	1.0	1.0	ND	ND	2	4	1	1
Orthophosphate as P, Dissolved	mg/L	0.14	0.042	ND	0.16	0.20	0.079	0.0039	0.012	0.12	0.077	0.14	0.14	ND	0.08	ND	0.06
Oxamyl	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Oxidation-Reduction Potential (Field)	mV	-50.5	-110.8	N/A	N/A	-99.2	30.1	-105.8	-151.4	-13.8	-92.8	-90.5	60.6	2.33	-106.0	-131.8	-10.1
o-Xylene	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
PCB Aroclor Screen	μg/L	ND	ND	ND	ND	ND	ND	-	-	ND	-	ND	ND	-	-	-	-
PCBs, Total	μg/L	-	-	-	-	-	-	ND	ND	-	ND	-	-	ND	ND	ND	ND
Pentachlorophenol	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Perylene-d12	μg/L	-	-	-	-	-	-	5.08	4.75	-	1.38	-	-	-	-	-	-
рН	pH Units	8.2	7.7	7.4	7.8	7.7	7.6	7.49	7.22	7.6	6.79	7.4	7.4	7.2	6.9	6.9	7.4
pH (Field)	pH Units	6.87	6.66	6.92	7.24	6.86	6.67	7.32	6.94	6.76	6.57	6.63	6.58	7.12	6.80	6.9	7.32
pH Temperature in °C	°C	21.7	21.9	21.6	21.3	20.1	19.9	-	-	21.9	-	21.4	21.0	-	-	-	-
Phosphorus, Dissolved	mg/L	0.11	ND	0.18	0.21	ND	ND	0.078	0.20	ND	0.047	ND	0.12	ND	0.08	ND	0.08
Picloram	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
p-Isopropyltoluene	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Potassium, Dissolved	mg/L	6.0	380	92	31	130	34	58	27	98	36	250	270	36	158	81	246
Potassium, Total	mg/L	-	-	-	-	-	-	60	27	-	37	-	-	-	-	-	-
Prometon	μg/L	-	-	-	-	-	-	ND	ND	-	ND	-	-	-	-	-	-
Prometryn	μg/L	-	-	-	-	-	-	ND	ND	-	ND	-	-	ND	ND	ND	ND
Propachlor	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Propoxur (Baygon)	μg/L	-	-	-	-	-	-	ND	ND	-	ND	-	-	ND	ND	ND	ND
QC Ratio TDS/SEC		-	-	-	-	-	-	-	-	-	-	-	-	0.70	0.67	0.70	0.66
sec-Butylbenzene	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Silica as SiO2, Dissolved	mg/L	30	25	26	35	34	38	36	40	34	40	32	32	32	30	34	15
Simazine	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Sodium, Dissolved	mg/L	140	10000	6000	710	6200	1500	1600	1000	5000	1400	9400	8100	7758	8588	7254	6541
Sodium, Total	mg/L	-	-	-	-	-	-	1700	1000	-	1400	-	-	-	-	-	-
Specific Conductance (EC)	μmhos/cm	1200	43000	30000	4900	31000	11000	12000	7800	29000	13000	43000	38000	44180	45230	38100	32970
Specific Conductance (EC) (Field)	μS/cm	1296	53620	35169	647	34730	11508	11704	7439	30671	12933	48132	42650	42787	45875	37546	32173
Strontium, Dissolved	μg/L	400	7400	7100	1600	7900	4100	3100	1900	8600	5300	12000	10000	9880 ND	8490	8936	4369
Styrene Sulfate as SOA Disselved	μg/L	ND 24	ND 3500	ND	ND	ND	ND 340	ND	ND 100	ND 060	ND 430	ND 2000	ND	ND 2208	ND 2270	ND 1700	ND 1560
Sulfate as SO4, Dissolved TCMX	mg/L	24	2500 2.2	1400 2.4	21	1000	340	370 0.0783	190	960 3.5	420 0.0877	2000 4.6	1900	2208	2270 0.0961	1790 0.0770	1560 0.0796
	μg/L °C	2.3 16.3	15.4	16.9	1.2 16.8	4.9 17.3	5.1	19.7	0.104 19.8	3.5 17.8	17.7	4.6 16.5	4.5 15.9	- 17.0		15.9	
Temperature (Field) Terbacil	μg/L	16.3				17.3	16.4		19.8 ND	17.8	17.7 ND			17.0	16.8		16
tert-Amyl Methyl Ether (TAME)		- ND	- ND	- ND	- ND	- ND	- ND	ND ND	ND ND	- ND	ND ND	- ND	- ND	- ND	- ND	- ND	- ND
tert-Amyl Methyl Ether (TAME)	μg/L	ND ND	ND ND	ND ND	ND ND	ND ND	- -	- ND	ND -	ND ND	ND -	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND
tert-Butyl alcohol (TBA)	μg/L μg/L	ND	ND ND	ND ND	ND ND	ND ND	- ND	- ND	- ND	ND ND	- ND	ND ND	ND ND	ND ND	ND ND	ND ND	ND ND
Tetrachloroethene (PCE)	μg/L μg/L	ND	ND	ND ND	ND	ND	ND	ND ND	ND ND	ND	ND ND	ND ND	ND	ND	ND	ND	ND ND
Tetrachloro-meta-xylene (TCMX)	μg/ L %	150	146	165	79	111	115	78	104	80	92	103	103	87	101	81	84
Thiobencarb	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Toluene	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND ND
Total Anions	meg/L	-	-	-	-	-	-	120	73	-	140	-	-	-	-	-	-
Total Cations	meq/L	11	120	-	-	-	-	120	73	-	140	-	-	520	522	437	368
Total Dissolved Solids	mg/L	630	34000	22000	3200	19000	8100	7400	4200	21000	8600	34000	28000	31000	30200	26600	21900
Total Dissolved Solids (Field)	mg/L	845	34853	22847.5	422.5	23616.4	7826.8	7942.4	5059.2	20855.6	8799.2	31284.5	29002	29097.2	31198.4	25513.6	21875.1

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	Borehole:	PR	k-1	М	L-1	ML	-2	М	L-3	M	L-4	MI	L-6		MD	W-1	
	Zone #:	1	2	1	2	1	2	1	2	1	2	1	2	1	2	3	4
Screen Interv	val (ft bgs):	190 - 200	125 - 135	113.5 - 118.5	90 - 100	167 - 177	90 - 100	180 - 190	103 - 113	163.5 - 173.5	74.5 - 84.5	152 - 162	100 - 110	237 - 247	187 - 197	152 - 162	60 - 70
Sai	mple Date:	24-Sep-13	25-Sep-13	5-Oct-13	7-Oct-13	17-Dec-13	19-Dec-13	11-Jan-14	13-Jan-14	5-Dec-13	6-Dec-13	22-Nov-13	23-Nov-13	1-May-14	7-May-14	8-May-14	10-May-14
Constituent ¹	Units	Result	Result	Result	Result	Result	Result	Result	Result	Result	Result	Result	Result	Result	Result	Result	Result
Total Kjehldahl Nitrogen, Dissolved	mg/L	ND	ND	16	8.1	14	1.5	9.7	1.6	11	0.15	7.3	2.3	ND	3.3	3.6	ND
Total Oxidizable Nitrogen, as N	mg/L	ND	ND	ND	ND	ND	ND	ı	-	ND	1	ND	ND	-	-	-	-
Total Trihalomethanes	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Toxaphene	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
trans-1,2-Dichloroethene	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
trans-1,3-Dichloropropene	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Trichloroethene (TCE)	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Trichlorofluoromethane	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Trifluralin	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Triphenyl phosphate	μg/L	-	-	-	-	-	-	6.30	6.10	-	5.24	-	-	-	-	-	-
Trithion	μg/L	-	-	-	-	-	-	ND	ND	-	ND	-	-	-	-	-	-
Tritium	pCi/L	-68.2 ± 108 (199)	38.7 ± 122 (212)	47.5 ± 127 (220)	-17.9 ± 117 (210)	-4.86±115 (204)	32.8±122 (212)	-2.52 ± 125 (221)	58.9 ± 121 (207)	-118±123 (231)	-110±130 (240)	10.3±129 (226)	-15.7±129 (230)	-	-	-	-
Tritium, prec. est. ²	TU	-	-	pending	pending	pending	pending	pending	pending	pending	pending	pending	pending	pending	pending	pending	pending
Turbidity	NTU	0.67	5.1	150	19	6.0	2.7	160	11	6.6	2.8	6.5	1.6	0.85	9.7	150	0.60
Turbidity (Field)	NTU	0.89	1.56	0.7	2.52	1.68	0.72	65.2	0.99	0.48	0.94	1.26	1.73	2.33	0.64	0.84	0.83
Vinyl Chloride	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Xylenes, Total	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Zinc, Total	μg/L	ND	ND	ND	ND	ND	ND	240	31	ND	29	ND	ND	ND	ND	ND	ND

Notes:

 $\begin{tabular}{ll} $^\circ C$ & = Degrees Celsius \\ CU & = Color Units \\ $\delta^{18}O\left(\%\right)$ & = Delta Oxygen-18 \\ $\delta^{2}H\left(\%\right)$ & = Delta-Deuterium \\ meq/L & = Milliequivalents per Liter \\ \end{tabular}$

mg/L = Milligrams per Liter

mV = Millivolts

NTU = Nephelometric Turbidity Units

pCi/L = Pico Curies per Liter
pg/L = Picograms per Liter
TON = Threshold Odor Number
TU = Tritium Units

 $\begin{array}{ll} \mu g/L &= Micorgrams \ per \ Liter \\ \mu mhos/cm &= Micromhos \ per \ Centimeter \\ \mu S/cm &= MicroSiemens \ per \ Centimeter \end{array}$

ND = NOT DETECTED at or above the Reporting Limit or Practical Quantitation Limit. If J-value reported, then NOT DETECTED at or above the Method Detection Limit (MDL)

¹ See laboratory water quality reports in Appendix G for method numbers, dilution factors, Method Detection Limits, and Reporting Limits.

² Laboratory water quality results pending.

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	Borehole:			СХ-В	1WO				СХ-В	2WO				CX-B4		
	Zone #:	1	2	3	4	5	6	1	2 2	3	4	1	2	3	4	5
Screen Interv	_	274 - 284	237 - 247		134 - 144	5 84 - 94	_	215 - 225	_	104 - 114	55 - 65	306 - 316	248 - 258		•	58 - 68
	· • -	18-Feb-14	19-Feb-14	182 - 192 21-Feb-14	22-Feb-14	23-Feb-14	51 - 61 25-Feb-14	8-Mar-14	161 - 171 10-Mar-14	104 - 114 11-Mar-14	12-Mar-14	5-Apr-14	6-Apr-14	155 - 165 8-Apr-14	110 - 120 9-Apr-14	10-Apr-14
	mple Date:												· ·		•	
Constituent ¹	Units	Result	Result	Result	Result	Result	Result	Result	Result	Result	Result	Result	Result	Result	Result	Result
1,1,1,2-Tetrachloroethane	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
1,1,1-Trichloroethane	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
1,1,2,2-Tetrachloroethane	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
1,1,2-Trichloro-1,2,2-trifluoroethane	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
1,1,2-Trichloroethane	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
1,1-Dichloroethane	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
1,1-Dichloroethene	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
1,1-Dichloropropene	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
1,2,3-Trichlorobenzene	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
1,2,3-Trichloropropane	μg/L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1,2,4-Trichlorobenzene	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
1,2,4-Trimethylbenzene	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
1,2-Dichlorobenzene	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
1,2-Dichlorobenzene-d4	μg/L	5.0	4.8	4.9	5.0	4.8	4.8	5.0	4.9	4.8	4.6	4.9	4.7	4.8	5.2	5.0
1,2-Dichloroethane	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
1,2-Dichloropropane	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
1,3,5-Trimethylbenzene	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
1,3-Dichlorobenzene	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
1,3-Dichloropropane	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
1,3-Dichloropropene, Total	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
1,3-Dimethyl-2-nitrobenzene	μg/L	5.0	5.3	5.6	5.1	5.5	5.4	5.0	4.8	5.2	5.0	5.4	5.2	4.1	4.3	5.0
1,4-Dichlorobenzene	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
1-Br-2-Nitrobenzene	μg/L	-	3.7	3.8	3.7	3.9	2.2	2.4	2.3	0.60	0.64	0.49	0.49	0.44	0.42	0.43
2,2-Dichloropropane	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
2,4,5-T	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
2,4,5-TP (Silvex)	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
2,4-D	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
2,4-DB	μg/L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
2,4-DCAA	μg/L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
2-Butanone	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
2-Chloroethyl vinyl ether	μg/L	-	-	ı	1	-	-	ı	ı	-	-	-	-	-	ı	-
2-Chlorotoluene	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
2-Hexanone	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
3,5-Dichlorobenzoic acid	μg/L	-	-	-	=	-	-	-	-	-	-	-	-	-	-	-
3-Hydroxycarbofuran	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
4,4´-DDD	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
4,4´-DDE	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
4,4´-DDT	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
4-Chlorotoluene	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
4-Methyl-2-pentanone	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Acetone	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Acifluorfen	μg/L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Alachlor	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Aldicarb	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Aldicarb Sulfone	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Aldicarb Sulfoxide	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND

Cal Am / RBF
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Technical Memorandum (TM 1) - Summary of Results - Exploratory Boreholes

	Borehole:			СХ-В	1140				СХ-В	214/0	1			CX-B4		
	-	1	2	3 3	4	5	6	1	2 2	3	4	1	2	3	4	5
Screen Inter	Zone #:		237 - 247	182 - 192	134 - 144	84 - 94	_			-	55 - 65		248 - 258			58 - 68
	mple Date:	274 - 284 18-Feb-14	19-Feb-14	21-Feb-14	22-Feb-14	23-Feb-14	51 - 61 25-Feb-14	215 - 225 8-Mar-14	161 - 171 10-Mar-14	104 - 114 11-Mar-14	12-Mar-14	306 - 316 5-Apr-14	6-Apr-14	155 - 165	110 - 120	10-Apr-14
	r											· · · · · · · · · · · · · · · · · · ·	 	8-Apr-14	9-Apr-14	· · ·
Constituent ¹	Units	Result	Result	Result	Result	Result	Result	Result	Result	Result	Result	Result	Result	Result	Result	Result
Allerin	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Alkalinity as CaCO3	mg/L	118	132	167	96	126	103	147	129	102	104	112	118	103	98	62
alpha-BHC	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND 30
Aluminum	μg/L	77	ND	ND	ND	ND	ND	84	74	156	204	ND	ND	ND	31	20
Ammonia as N, Dissolved	mg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	0.1	ND	ND	ND	ND	ND
AMPA	μg/L	110	100	110	98	89	110	120	98	100	76	98	110	110	96	110
Aroclor 1016	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Aroclor 1221	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Aroclor 1232	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Aroclor 1242	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Aroclor 1248	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Aroclor 1254	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Aroclor 1260	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND -
Arsenic, Total	μg/L	38	ND	ND	ND	ND	ND	46	28	59	55	33	32	27	26	5
Atrazine	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Barium, Dissolved	μg/L	138	210	ND	120	ND	100	109	346	85	90	174	123	84	179	222
Bentazon	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Benzene	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Benzo(a)pyrene	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
beta-BHC	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Bicarbonate as CaCO3	mg/L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Bicarbonate as HCO3	mg/L	144	161	204	117	154	126	179	157	124	127	137	144	126	120	76
Bis(2-ethylhexyl) adipate (DEHA)	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Bis(2-ethylhexyl) phthalate (DEHP)	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Boron, Dissolved	μg/L	700	730	1540	2880	2800	2400	1540	860	2580	2360	600	1840	1400	1310	260
Bromacil	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Bromide, Dissolved	mg/L	41	24	49.6	38	41	38	38	23	45	44	43	39	29	31	6.1
Bromobenzene	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Bromochloromethane	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Bromodichloromethane	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Bromofluorobenzene	μg/L	52	50	51	52	50	48	51	51	51	48	50	49	49	52	51
Bromoform	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Bromomethane	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Butachlor	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Calcium, Dissolved	mg/L	2718	1558	2018	502	656	709	1948	1141	732	886	3158	1557	911	1164	277
Calcium, Total	mg/L	2718	1581	2090	505	674	710	1961	1181	712	896	3125	1516	938	1081	261
Captan	μg/L	-	-	=	-	-	-	-	-	-	-	-	-	-	-	-
Carbaryl	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Carbofuran	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Carbon Tetrachloride	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Carbonate as CaCO3	mg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Chlordane	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Chloride, Dissolved	mg/L	14184	8796	17995	14050	14755	13675	13026	7408	14099	14464	14013	13566	10128	11044	2045
Chloride, Total	mg/L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Chlorobenzene	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Chloroethane	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND

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	_															
	Borehole:		T		1WQ					2WQ				CX-B4		
	Zone #:	1	2	3	4	5	6	1	2	3	4	1	2	3	4	5
Screen Inter	· • · •	274 - 284	237 - 247	182 - 192	134 - 144	84 - 94	51 - 61	215 - 225	161 - 171	104 - 114	55 - 65	306 - 316	248 - 258	155 - 165	110 - 120	58 - 68
Sa	mple Date:	18-Feb-14	19-Feb-14	21-Feb-14	22-Feb-14	23-Feb-14	25-Feb-14	8-Mar-14	10-Mar-14	11-Mar-14	12-Mar-14	5-Apr-14	6-Apr-14	8-Apr-14	9-Apr-14	10-Apr-14
Constituent ¹	Units	Result														
Chloroform	μg/L	ND														
Chloromethane	μg/L	ND														
Chloropropham	μg/L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Chlorothalonil	μg/L	ND														
cis-1,2-Dichloroethene	μg/L	ND														
cis-1,3-Dichloropropene	μg/L	ND														
Color	CU	7	14	ND	10	5	4	21	7	ND	23	23	4	9	16	14
Conductivity (Field)	μS/cm	32361	20869	41546	34907	35167	30803	31029	18875	34532	34162	34754	34291	25663	26466	6208
Copper, Total	μg/L	15	ND	150	136	107	140	111	90	18						
Cyanazine	μg/L	=	-	-	-	=	-	-	=	-	-	-	-	=	=	-
Dalapon	μg/L	ND														
DCPA	μg/L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
DCPAA	μg/L	48	51	42	43	45	41	45	56	47	47	53	55	56	59	58
Decachlorobiphenyl	μg/L	0.00769	0.0667	0.0149	0.0690	0.0727	71%	0.0277	0.0308	0.0727	0.0680	0.0205	0.0504	0.0417	0.0364	0.0585
Delta Oxygen-18	$\delta^{18}O$ (‰)	-2.6	-4.3	-0.8	-2.0	-1.6	-2.1	-2.3	-3.7	-1.8	-1.4	-3.0	-2.8	-4.3	-4.0	-5.9
delta-BHC	μg/L	ND														
Delta-Deuterium	δ^{2} H (‰)	-18.4	-29.1	-6.2	-14.0	-12.0	-15.1	-18.0	-29.2	-13.3	-12.6	-19	-17	-28	-26	-40
Diazinon	μg/L	ND														
Dibromochloromethane	μg/L	ND														
Dibromochloropropane (DBCP)	μg/L	ND														
Dibromomethane	μg/L	ND														
Dicamba	μg/L	ND														
Dichloroacetate	mg/L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Dichlorodifluoromethane (Freon 12)	μg/L	ND														
Dichloromethane	μg/L	ND														
Dichloroprop	μg/L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Dieldrin	μg/L	ND														
Di-isopropyl ether (DIPE)	μg/L	ND														
Dimethoate	μg/L	ND														
Dinoseb	μg/L	ND														
Dioxin (2,3,7,8 TCDD)	pg/L	ND														
Diphenamid	μg/L	-	-	ı	-	ı	ī	ı	ı	ı	-	-	-	-	ı	-
Diquat	μg/L	ND														
Dissolved Oxygen (Field)	mg/L	1	1	0.1	3.6	3.6	3.5	0.9	1.4	5.7	4.7	0.6	2.5	4.5	5.1	28.3
Disulfoton	μg/L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Endosulfan I	μg/L	ND														
Endosulfan II	μg/L	ND														
Endosulfan sulfate	μg/L	ND														
Endothall	μg/L	ND														
Endrin	μg/L	ND														
Endrin aldehyde	μg/L	ND														
EPTC	μg/L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Ethyl tert-Butyl Ether (ETBE)	μg/L	ND														
Ethylbenzene	μg/L	ND														
Ethylene Dibromide (EDB)	μg/L	ND														
Fluoride, Dissolved	mg/L	0.2	0.1	ND	ND	0.4	0.3	ND	0.2	0.5	0.5	ND	ND	ND	ND	0.2

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	Borehole:			СХ-В	1WO				СХ-В	214/0				CX-B4		
	Zone #:	1	2	3 3	4	5	6	1	2 2	3	4	1	2	3	4	5
Screen Interv	_	274 - 284	237 - 247		134 - 144	84 - 94	_			104 - 114	55 - 65		248 - 258		•	+
	· • -	18-Feb-14	19-Feb-14	182 - 192 21-Feb-14	22-Feb-14	23-Feb-14	51 - 61 25-Feb-14	215 - 225 8-Mar-14	161 - 171 10-Mar-14	104 - 114 11-Mar-14	12-Mar-14	306 - 316 5-Apr-14	6-Apr-14	155 - 165 8-Apr-14	110 - 120 9-Apr-14	58 - 68 10-Apr-14
4	mple Date:												· '	·		· · ·
Constituent ¹	Units	Result	Result	Result	Result	Result	Result	Result	Result	Result	Result	Result	Result	Result	Result	Result
gamma-BHC (Lindane)	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Glyphosate	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Hardness as CaCO3	mg/L	11070	6723	9880	5350	6748	5561	8776	5486	5995	6405	12494	7768	5950	5928	1278
Heptachlor	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Heptachlor Epoxide	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Hexachlorobenzene	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Hexachlorobutadiene	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Hexachlorocyclopentadiene	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Hydroxide as CaCO3	mg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
lodide, Dissolved	μg/L	ND	ND	190	ND	160	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Iron, Dissolved	μg/L	362	2539	1780	814	171	57	246	148	ND	121	775	ND	151	130	148
Iron, Total	μg/L	362	2643	1928	922	178	162	367	238	138	164	878	241	205	389	185
Isopropylbenzene	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Lithium	μg/L	218	120	140	120	170	140	149	75	173	164	191	127	63	31	5
m,p-Xylenes	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Magnesium, Dissolved	mg/L	1041	683	1078	981	1215	928	936	605	1056	1015	1146	988	839	845	162
Magnesium, Total	mg/L	1040	674	1132	993	1230	920	942	616	1024	1012	1139	967	876	784	152
Manganese, Dissolved	μg/L	127	166	361	349	ND	172	ND	ND	ND	ND	657	133	204	172	345
Manganese, Total	μg/L	134	187	382	387	78	131	ND	ND	ND	ND	650	128	210	164	320
Mass Balance, Total	meq/L	-	-	-	-	_	-	-	-	-	-	-	-	-	-	-
Mass Balance-Dissolved Anions	meq/L	439.7	271.9	567.6	436.9	458.5	424.8	405.7	226.8	439	449	432.7	422.8	313.2	342	64.9
Mass Balance-Dissolved Cations	meq/L	423.3	261.6	564.9	458.9	464.6	387.0	399.0	215.5	418	418	464.8	459.7	331.6	349	70.3
MBAS (Surfactants)	mg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Methiocarb	μg/L	_	-	-	-	_	-	ND	ND	ND	ND	ND	ND	ND	ND	ND
Methomyl	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Methoxychlor	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Methyl tert-butyl ether (MTBE)	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Metolachlor	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Metribuzin	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Molinate	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Naphthalene	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
n-Butylbenzene	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Nitrate as NO3	mg/L	ND	ND	ND	2	2	3	ND	2	2	ND	ND	2	3	4	21
Nitrate+Nitrite as N	mg/L	ND	0.2	ND	0.4	0.4	0.8	ND	0.6	0.5	ND	ND	0.3	0.7	0.9	4.9
Nitrite as NO2-N, Dissolved	mg/L	ND	ND	ND	ND	ND	ND	0.4	0.2	ND	ND	ND	ND	ND	ND	0.2
n-Propylbenzene	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Odor	TON	1	1	1	1	1	1	1	2	1	1	2	3	1	1	4
Orthophosphate as P, Dissolved	mg/L	0.05	0.09	0.08	0.07	0.07	ND	ND	ND	ND	0.05	ND	ND	ND	ND	ND ND
Oxamyl	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND ND	ND	ND	ND	ND
Oxidation-Reduction Potential (Field)	μg/ L mV	61.1	-32.4	-253.3	-56.6	7.9	-67.3	49	30.9	45.6	16.2	-38.4	36.8		74.9	6.5
, ,			-32.4 ND	-253.3 ND							16.2 ND			34 ND	74.9 ND	
o-Xylene	μg/L	ND			ND	ND	ND	ND	ND	ND		ND	ND			ND
PCB Aroclor Screen	μg/L	- ND	- ND	- ND	- ND	- ND	- ND	- ND	- ND	- ND	- ND	- ND	- ND	- ND	- ND	- ND
PCBs, Total	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Pentachlorophenol	μg/L	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Perylene-d12	μg/L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
рН	pH Units	6.7	6.9	6.9	6.9	7.2	7.3	7.0	7.4	7.2	7.2	6.8	6.9	6.9	6.6	7.1

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Technical Memorandum (TM 1) - Summary of Results - Exploratory Boreholes

	Borehole:			СХ-В	1WQ				СХ-В	2WQ				CX-B4		
	Zone #:	1	2	3	4	5	6	1	2	3	4	1	2	3	4	5
Screen Inter	val (ft bgs):	274 - 284	237 - 247	182 - 192	134 - 144	84 - 94	51 - 61	215 - 225	161 - 171	104 - 114	55 - 65	306 - 316	248 - 258	155 - 165	110 - 120	58 - 68
Sa	mple Date:	18-Feb-14	19-Feb-14	21-Feb-14	22-Feb-14	23-Feb-14	25-Feb-14	8-Mar-14	10-Mar-14	11-Mar-14	12-Mar-14	5-Apr-14	6-Apr-14	8-Apr-14	9-Apr-14	10-Apr-14
Constituent ¹	Units	Result														
pH (Field)	pH Units	6.54	6.79	6.79	6.82	7.05	7.18	6.71	6.69	6.96	7.12	6.61	6.66	6.75	6.63	6.92
pH Temperature in °C	°C	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Phosphorus, Dissolved	mg/L	0.06	0.10	0.08	0.07	0.07	ND	ND	ND	ND	0.05	ND	0.09	ND	ND	ND
Picloram	μg/L	ND														
p-Isopropyltoluene	μg/L	ND														
Potassium, Dissolved	mg/L	53	35	34	256	221	186	55	73	201	226	52	67	56	98	9.6
Potassium, Total	mg/L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Prometon	μg/L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Prometryn	μg/L	-	-	-	-	-	-	ND								
Propachlor	μg/L	ND														
Propoxur (Baygon)	μg/L	-	-	-	-	-	-	ND								
QC Ratio TDS/SEC		0.68	0.59	0.73	0.67	0.67	0.67	0.72	0.73	0.66	0.66	0.78	0.71	0.78	0.80	0.70
sec-Butylbenzene	μg/L	ND														
Silica as SiO2, Dissolved	mg/L	34	ND	25	27	19	18.0	34	30	20	19	34	32	30	27	28
Simazine	μg/L	ND														
Sodium, Dissolved	mg/L	4612	2914	8612	7968	7500	6219	5135	2437	6643	6536	4864	6747	4958	5041	987
Sodium, Total	mg/L		_	_	-	-	_	_	_	-	-	-	-	-	-	-
Specific Conductance (EC)	μmhos/cm	36940	24570	48770	39610	40900	37260	36680	22060	40720	40270	38270	38210	26270	29810	6910
Specific Conductance (EC) (Field)	μS/cm	36601	23705	47112	39592	41336	35952	35199	21620	40173	39657	37688	38354	28707	29933	6988
Strontium, Dissolved	μg/L	16834	11,000	12000	9400	10000	9500	13328	8621	9020	9966	17696	11232	8713	10508	2167
Styrene	μg/L	ND														
Sulfate as SO4, Dissolved	mg/L	1760	991	2688	1832	1882	1748	1674	713	1855	1822	1663	1789	1202	1358	269
TCMX	μg/L	0.0677	0.110	0.0753	0.0752	0.0796	_	0.112	0.111	0.112	0.0770	0.0855	0.0933	0.0960	0.100	0.0943
Temperature (Field)	°C	18.9	18.7	18.8	18.8	17.2	17.5	18.8	18.3	17.6	17.8	20.9	19.4	19.4	18.9	19.1
Terbacil	μg/L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
tert-Amyl Methyl Ether (TAME)	μg/L	ND														
tert-Butyl alcohol (TBA)	μg/L	ND														
tert-Butylbenzene	μg/L	ND														
Tetrachloroethene (PCE)	μg/L	ND														
Tetrachloro-meta-xylene (TCMX)	%	71	115	79	79	84	111	117	116	118	81	90	98	102	105	99
Thiobencarb	μg/L	ND														
Toluene	μg/L	ND														
Total Anions	meq/L	-	_	_	-	-	_	_	_	-	-	-	_	-	_	-
Total Cations	meq/L	424.7	262.0	596.2	463.6	463.4	387.9	406.1	222.0	407	415	463.4	450.4	347.4	319	64.0
Total Dissolved Solids	mg/L	25200	14600	35600	26500	27400	24800	26500	16200	26800	26700	29800	27200	20500	24000	4815
Total Dissolved Solids (Field)	mg/L	24888	16122.8	32034.8	26921.2	28111.2	24452.8	23936	14708.4	27315.6	26968.3	25629.2	26084.8	19522.8	20352.4	4760
Total Kjehldahl Nitrogen, Dissolved	mg/L	ND	0.4	0.3	0.4	0.5	ND	ND	ND	ND ND	ND	ND	ND ND	ND	ND ND	ND
Total Oxidizable Nitrogen, as N	mg/L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Total Trihalomethanes	μg/L	ND														
Toxaphene	μg/L	ND														
trans-1,2-Dichloroethene	μg/L	ND														
trans-1,3-Dichloropropene	μg/L μg/L	ND	ND	ND	ND ND	ND	ND ND	ND	ND ND	ND ND	ND	ND ND	ND	ND	ND	ND
Trichloroethene (TCE)	μg/L μg/L	ND ND	ND ND	ND	ND ND	ND ND										
Trichlorofluoromethane	μg/L μg/L	ND ND	ND ND	ND	ND	ND ND	ND ND									
Trifluralin	μg/L μg/L	ND ND	ND	ND ND	ND ND	ND ND	ND ND	ND	ND ND							
			-		-	-	- ND	-	- ND							
Triphenyl phosphate	μg/L	-	-	-		-	-	-	<u> </u>	-	-	-	-	-	-	-

Cal Am / RBF Monterey Peninsula Water Supply Project Hydrogeologic Investigation Technical Memorandum (TM 1) - Summary of Results - Exploratory Boreholes

Summary of Isolated Aquifer Zone Testing Field and Laboratory Water Quality Results - CEMEX - Marina, CA

	Borehole:			CX-B	1WQ		•		CX-B	2WQ				CX-B4		
	Zone #:	1	2	3	4	5	6	1	2	3	4	1	2	3	4	5
Scree	Interval (ft bgs):	274 - 284	237 - 247	182 - 192	134 - 144	84 - 94	51 - 61	215 - 225	161 - 171	104 - 114	55 - 65	306 - 316	248 - 258	155 - 165	110 - 120	58 - 68
	Sample Date:	18-Feb-14	19-Feb-14	21-Feb-14	22-Feb-14	23-Feb-14	25-Feb-14	8-Mar-14	10-Mar-14	11-Mar-14	12-Mar-14	5-Apr-14	6-Apr-14	8-Apr-14	9-Apr-14	10-Apr-14
Constituent ¹	Units	Result	Result	Result	Result	Result	Result									
Trithion	μg/L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Tritium	pCi/L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Tritium, prec. est. ²	TU	0.35 ± 0.09	0.04 ± 0.09	0.01 ± 0.09	0.50 ± 0.09	0.48 ± 0.09	0.81 ± 0.09	0.10 ± 0.09	0.18 ± 0.09	0.44 ± 0.09	0.62 ± 0.09	pending	pending	pending	pending	pending
Turbidity	NTU	1.6	2.9	0.70	4.6	0.75	0.45	0.40	0.65	0.65	1.5	0.20	1.3	0.65	1.0	1.4
Turbidity (Field)	NTU	0.57	1.20	0.25	0.24	0.47	0.33	0.91	0.49	0.57	0.63	0.54	1.46	0.18	0.85	1.12
Vinyl Chloride	μg/L	ND	ND	ND	ND	ND	ND									
Xylenes, Total	μg/L	ND	ND	ND	ND	ND	ND									
Zinc, Total	μg/L	99	ND	ND	ND	ND	ND	218	217	384	356	ND	ND	ND	38	ND

Notes:

°C = Degrees Celsius CU = Color Units $\delta^{18}O(\%) = Delta Oxygen-18$ $\delta^{2}H(\%) = Delta-Deuterium$

meq/L = Milliequivalents per Liter mg/L = Milligrams per Liter

mV = Millivolts

NTU = Nephelometric Turbidity Units pCi/L = Pico Curies per Liter

pg/L = Picograms per Liter

TON = Threshold Odor Number

TU = Tritium Units

μg/L = Micorgrams per Liter

μmhos/cm = Micromhos per Centimeter
μS/cm = MicroSiemens per Centimeter

ND = NOT DETECTED at or above the Reporting Limit or Practical Quantitation Limit. If J-value reported, then NOT DETECTED at or above the Method Detection Limit (MDL)

¹ See laboratory water quality reports in Appendix G for method numbers, dilution factors, Method Detection Limits, and Reporting Limits.

² Laboratory water quality results pending.

Hydraulic Conductivity for Geologic Units at CEMEX

	Borehole		CX-B1				CX-B2				СХ-ВЗ				CX-B4		
\mathbf{Q}_{od}	Weighed average K for each soil Type ¹	% thickness	Lithology	Min K [ft/day]	Max [ft/day]	% thickness	Lithology	Min K [ft/day]	Max [ft/day]	% thickness	Lithology	Min K [ft/day]	Max [ft/day]	% thickness	Lithology	Min K [ft/day]	Max [ft/day]
∙vod	each son Type	1.00	SM: Silty Sand	45	130	1.00	SW: Well- Graded Sand	292	770	1.00	SP: Sand	74	224	1.00	SP: Sand	135	365
	Total K value [ft/day]			45	130			292	770			74	224			135	365
	Borehole		CX-B1				CX-B2				СХ-ВЗ				CX-B4		
		% thickness	Lithology	Min K [ft/day]	Max [ft/day]	% thickness	Lithology	Min K [ft/day]	Max [ft/day]	% thickness	Lithology	Min K [ft/day]	Max [ft/day]	% thickness	Lithology	Min K [ft/day]	Max [ft/day]
	Weighed average K for	0.25	GW: Gravel	334	849	0.67	SP: Sand	16	65	0.50	SP: Sand	21	69	1.00	SP: Sand	95	234
Q _t	each soil Type ¹	0.38	SW: Well- Graded Sand	330	1,121	0.33	SM: Silty Sand	83	211	0.50	SM: Silty Sand	130	509				
		0.38	SM: Silty Sand	98	266												
	Total K value [ft/day]			244	732			38	114			76	289			95	234

¹ For each soil type, an average is calculated for each method (Hazen, Krumbein-Monk, and Kozeny-Carman) with a weighed factor of thickness. The min K and max K for each soil type is the minimum and maximum among these three weighed average K value.

Attachment 1 - Technical Memorandum (TM 1) - Summary of Results - Exploratory Boreholes

Hydraulic Conductivity for Geologic Units at MOSS LANDING

	Borehole		MDV	V-1			ML	-1			ML	2			MI	3	
		% thickness	Lithology	Min K [ft/day]	Max [ft/day]	% thickness	Lithology	Min K [ft/day]	Max [ft/day]	% thickness	Lithology	Min K [ft/day]	Max [ft/day]	% thickness	Lithology	Min K [ft/day]	Max [ft/day]
Dune Sand	Weighed average K for each soil Type ¹	1.00	SP: Sand	135	300					1.00	SW: Well- Graded Sand	383	1,090				
	Total K value [ft/day]			135	300							383	1,090				
	Borehole		MDV				ML				ML				MI		
		% thickness	Lithology	Min K [ft/day]	Max [ft/day]	% thickness	Lithology	Min K [ft/day]	Max [ft/day]	% thickness	Lithology	Min K [ft/day]	Max [ft/day]	% thickness	Lithology	Min K [ft/day]	Max [ft/day]
		1.00	SP: Sand	170	477	0.13	SP: Sand with Gravel	469	1,175	0.33	SW: Well- Graded Sand with Gravel	484	949	1.00	SP: Sand	166	564
	Weighed average K for					0.13	SP-SM: Sand with Silt and Gravel	445	1,322	0.67	SP: Sand	34	102				
Perched "A" Aquifer	each soil Type ¹					0.75	SP: Sand	109	393								
		_								_				_			
	Total K value [ft/day]			170	477			196	607			184	385			166	564

¹ For each soil type, an average is calculated for each method (Hazen, Krumbein-Monk, and Kozeny-Carman) with a weighed factor of thickness. The min K and max K for each soil type is the minimum and maximum among these three weighed average K value.

Hydraulic Conductivity for Geologic Units at MOSS LANDING

	Borehole		MI	L-4			MI	6			PR-	-1	
	Weighed average K for each soil Type ¹	% thickness	Lithology	Min K [ft/day]	Max [ft/day]	% thickness	Lithology	Min K [ft/day]	Max [ft/day]	% thickness	Lithology	Min K [ft/day]	Max [ft/day]
Dune Sand		1.00	SP: Sand	164	468								
	Total K value [ft/day]			164	468								
	Borehole		MI				MI				PR-		
		% thickness	Lithology	Min K [ft/day]	Max [ft/day]	% thickness	Lithology	Min K [ft/day]	Max [ft/day]	% thickness	Lithology	Min K [ft/day]	Max [ft/day]
		1.00	SP: Sand	75	212	0.60	SP: Sand	32	92	0.20	SW: Well- Graded Sand with Gravel	699	1,148
						0.20	SW: Well- Graded Sand	149	610	0.20	SM: Silty Sand with Gravel	311	1,150
Perched "A" Aquifer	Weighed average K for each soil Type ¹					0.20	SP-SM: Sand with Silt	48	178	0.20	SP: Sand with Gravel	302	561
										0.20	SP: Sand	165	396
										0.20	SW: Well- Graded Sand	1,055	9,561
	Total K value [ft/day]			75	212			59	213			506	2563

CEMEX Area - Maximum K Values

Well		Dune :	Sand Aquifer	•			180-Foot Aqı	uifer (or Equi	valent)	
weii	Thickness [ft]	% Coarse	% Fine	Kc [ft/d]	Kf [ft/d]	Thickness [ft]	% Coarse	% Fine	Kc [ft/d]	Kf [ft/d]
CX-B1	86	1.00	0.00	270	na	160	0.81	0.18	508	0.0149
CX-B2	91	0.98	0.02	373	0.0270	148	0.77	0.23	152	0.0190
CX-B3	91	0.95	0.05	308	0.0270	164	0.77	0.23	277	0.0185
CX-B4	90	1.00	0.00	295	na	195	0.77	0.23	190	0.0227
Average	90	0.98	0.02	311	0.0270	167	0.78	0.22	282	0.0188

CEMEX Area - Minimum K Values

Well		Dune	Sand Aquifer			_	180-Foot Aqı	uifer (or Equi	valent)	
weii	Thickness [ft]	% Coarse	% Fine	Kc [ft/d]	Kf [ft/d]	Thickness [ft]	% Coarse	% Fine	Kc [ft/d]	Kf [ft/d]
CX-B1	86	1.00	0.00	96	na	160	0.81	0.18	156	0.0043
CX-B2	91	0.98	0.02	136	0.0210	148	0.77	0.23	52	0.0100
CX-B3	91	0.95	0.05	110	0.0210	164	0.77	0.23	90	0.0092
CX-B4	90	1.00	0.00	105	na	195	0.77	0.23	71	0.0150
Average	90	0.98	0.02	112	0.0210	167	0.78	0.22	92	0.0096

Monterey Peninsula Water Supply Project Hydrogeologic Investigation
Attachment 1 - Technical Memorandum (TM 1) - Summary of Results - Exploratory Boreholes

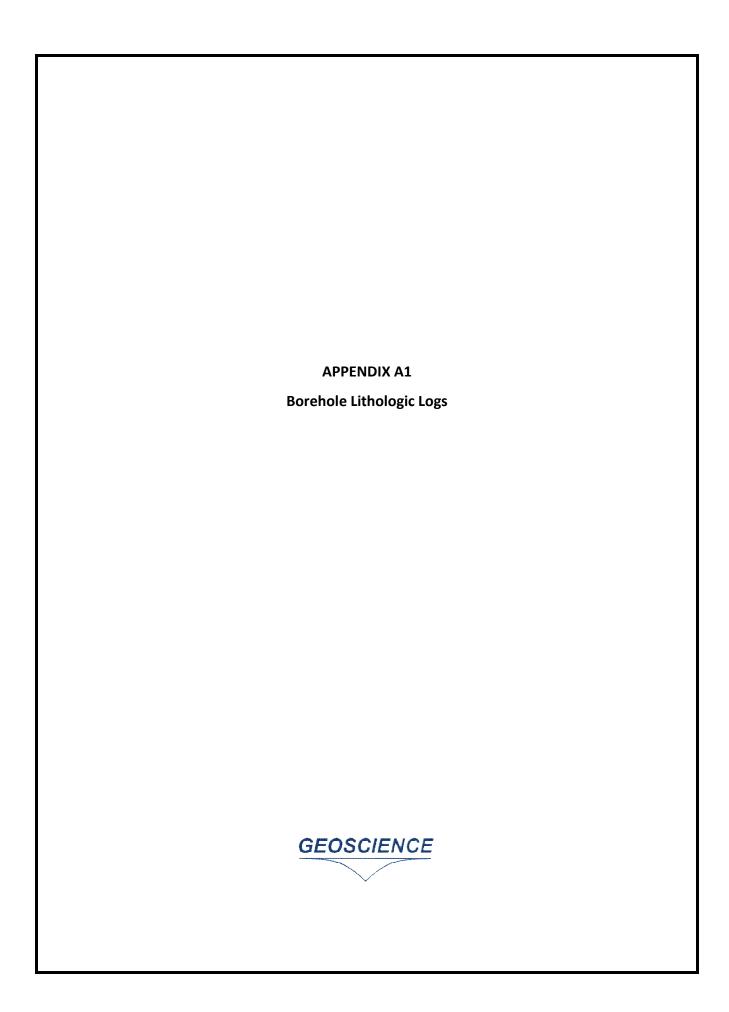
Moss Landing Area - Maximum K Values

Well	Dur	ne Sand Aqui	fer/ Perched	"A" Aquifer	
vveii	Thickness [ft]	% Coarse	% Fine	Kc [ft/d]	Kf [ft/d]
ML-1	146	0.32	0.68	485	0.0222
ML-2	200	0.65	0.35	783	0.0199
ML-3	200	0.30	0.70	841	0.0201
ML-4	201	0.63	0.37	618	0.0183
ML-6	200	0.64	0.36	704	0.0220
Average	189	0.51	0.49	686	0.0205
PR-1	139	0.93	0.07	1303	0.0213

Monterey Peninsula Water Supply Project Hydrogeologic Investigation
Attachment 1 - Technical Memorandum (TM 1) - Summary of Results - Exploratory Boreholes

Moss Landing Area - Minimum K Values

Well	Dune Sand Aquifer/ Perched "A" Aquifer									
vveii	Thickness [ft]	% Coarse	% Fine	Kc [ft/d]	Kf [ft/d]					
ML-1	146	0.32	0.68	166	0.0144					
ML-2	200	0.65	0.35	228	0.0112					
ML-3	200	0.30	0.70	235	0.0114					
ML-4	201	0.63	0.37	0.37 200						
ML-6	200	0.64	0.36	210	0.0140					
Average	189	0.51	0.49	208	0.0120					
					·					
PR-1	139	0.93	0.07	397	0.0131					



APPENDIX A1:

BOREHOLE LITHOLOGIC LOGS

CONTENTS

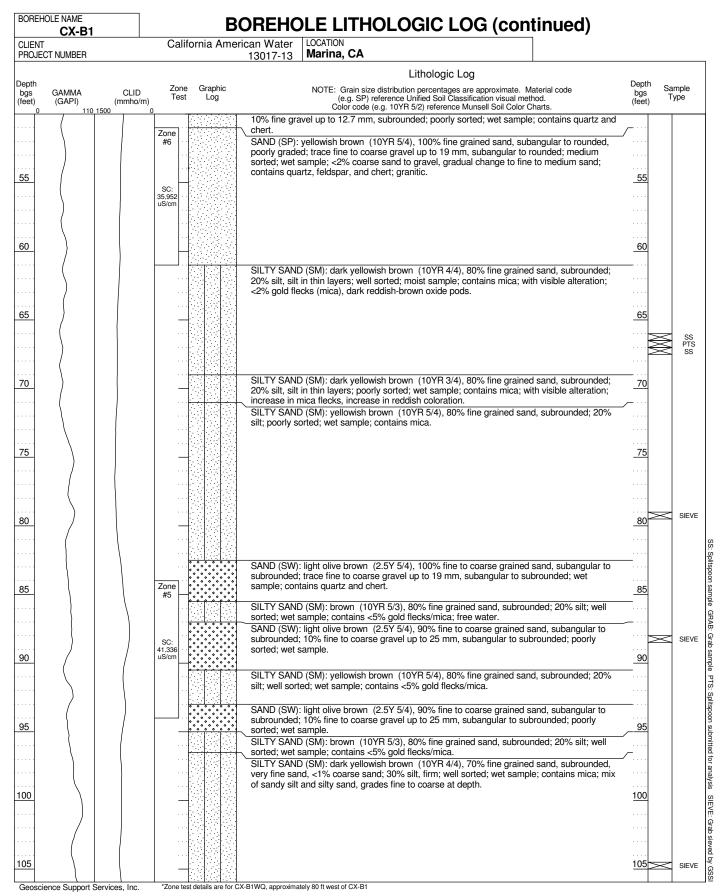
Description	Page
Borehole CX-B1	A1-1
Borehole CX-B2	A1-7
Borehole CX-B3	A1-13
Borehole CX-B4	A1-20
Borehole MDW-1	A1-27
Borehole ML-1	A1-33
Borehole ML-2	A1-37
Borehole ML-3	A1-41
Borehole ML-4	A1-45
Borehole ML-6	A1-49
Borehole PR-1	A1-53



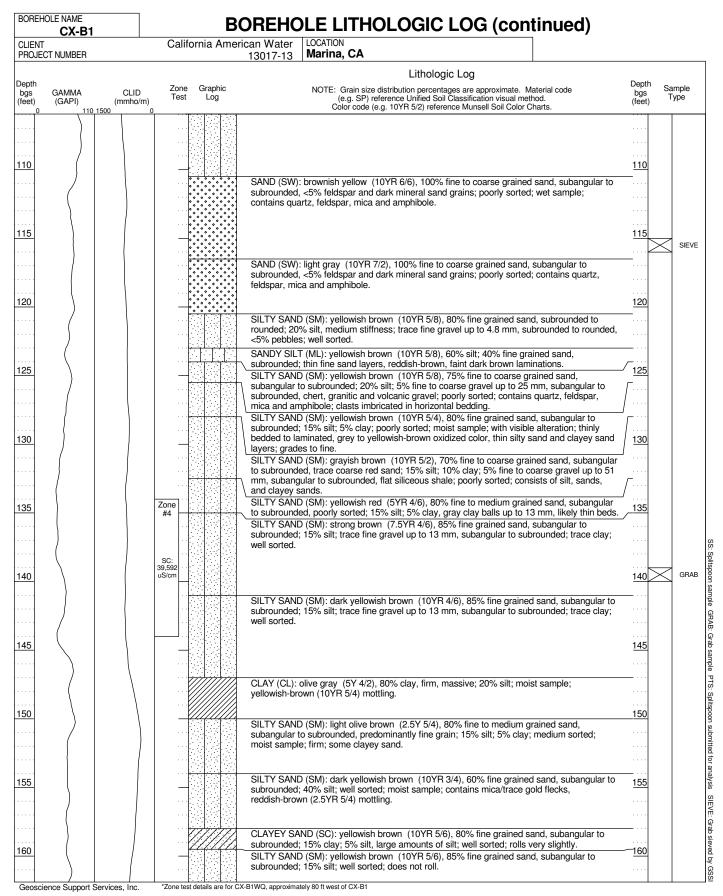


BOREHOLE NAME CX-B	1			ВС	REHO	LE LITHOL	OGIC LO	à		
CLIENT PROJECT NUMBER	-	Calif	fornia Amer	rican Water 13017-13	LOCATION Marina, C					
REPORT DATE				7/8/2014		apis Plant 5", -121°48'21.2364"	Geographic NAD83			
DRILLING CONTRAC DRILLER	TOR		Jos	ade Drilling se Munguia	B. Villalok					
DRILLING RIG TYPE	Proson	nic 600T	DRILLING METHOD		Sonic	START DATE	10/22/13	BOREHOLE DIAMETER		9 in/8 in
SURFACE ELEVATION		28.0 ft	TOTAL DEPTH		306 ft bgs	FINISH DATE	10/29/13	CORE SIZE		6 in
Depth bgs GAMMA (feet) (GAPI)	CLID (mmho/ 0 1500				(e.g. 8	SP) reference Unified Soi	gic Log ages are approximate. M I Classification visual met ence Munsell Soil Color C	nod.	Depth bgs (feet)	Sample Type
				grained sand	d, subrounded,	poorly graded, <5% of	h brown (10YR 4/2), 1 dark mineral sand grair ns feldspar and amphik	ns; trace silt,		
5									5	
10									10	
·····)							fine grained sand, sub ed; dry sample; contair			
15									15	
				SAND (SP):	yellowish brow	rn (10YR 5/4), 100% i	fine to medium grained; dry sample; contains	d sand, subrounded;		
				amphibole.			fine to medium grained		_	
20		/ -				•	eldspar and amphibole		20	
		/				e; contains quartz, felo		oana, a aoo om, a aoo		
25		_		CAND (OD)	.,	(50)/5(4) 4000/			<u>25</u>	G
					d grains, <0.5%		dium grained sand, sul well sorted; wet sampl			oo. opiiispoon
				SAND (SP):	yellowish brow	n (10YR 5/8), 100% sand grains; well sorte	medium grained sand, ed; wet sample; contain	subrounded, poorly		
30				and amphibe	ole.				30	
										ا ا ا
35									35	
				graded, bed	s of medium to	coarse sand; trace fir	medium grained sand, ne gravel up to 12.7 m	m, subrounded; trace		anijae onno, orau salipie rio, opiisyooli suuliiteo ioi alaysis oteve, orau sievo, uy ooo
				silt, brown a	nd gray streaks		n sorted; wet sample;			
40									40	Supplier
										lalysis .
45				SAND (SD).	gravieh brown	(2.5V.5/2), 100°/ ~~	dium to coarse graine	d sand subrounded	45	ן מות מות
				to rounded;	trace fine grave		ounded to rounded; po			Gi &C
				23		, aa o, gra				eved by
50 Geoscience Support	Services Inc	*Zone te	st details are for C	SAND (SP): X-B1WQ, approxima			nedium to coarse grain	ed sand, subrounded;	50	G

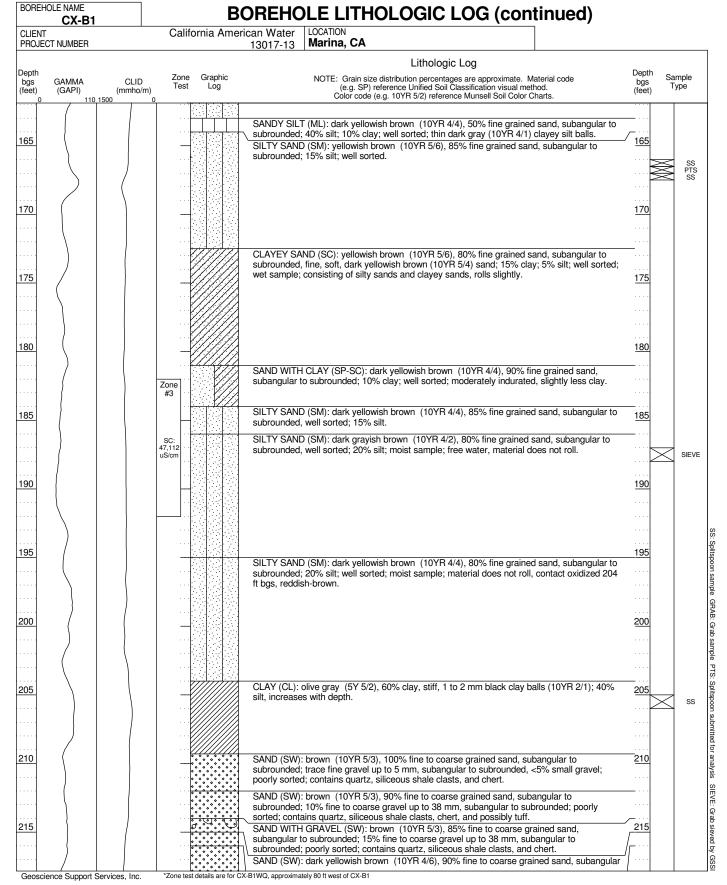
Telephone: (909) 451-6650 Fax: (909) 451-6638



Telephone: (909) 451-6650 Fax: (909) 451-6638



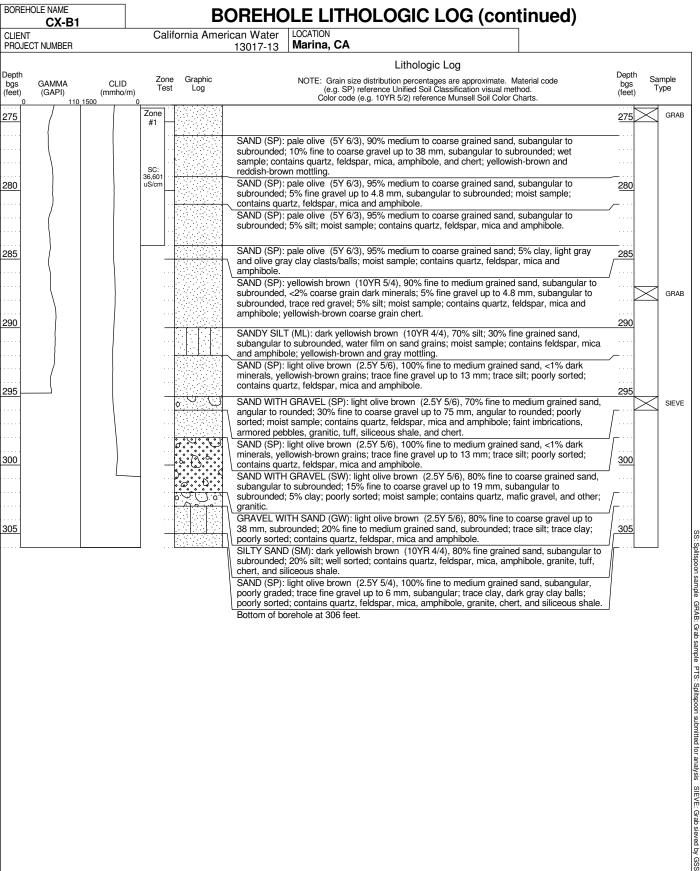
Telephone: (909) 451-6650 Fax: (909) 451-6638 www.gssiwater.com



BOREH	OLE NAME CX-B1			В	OREHO	DLE LITHOLOGIC LOG (continued)			
CLIENT		1	Calif	fornia Amer	ican Water 13017-13	LOCATION Marina, CA			
Danth						Lithologic Log	Danth		
Depth bgs (feet)	GAMMA (GAPI)	CLID (mmho/n	Zone Test			NOTE: Grain size distribution percentages are approximate. Material code (e.g. SP) reference Unified Soil Classification visual method. Color code (e.g. 10YR 5/2) reference Munsell Soil Color Charts.	Depth bgs (feet)	Sample Type	,
220					SAND (SW)	ed; 10% fine to coarse gravel up to 38 mm, subangular to subrounded; poorly ains quartz; oxidized layer. clive (5Y 5/3), 90% fine to coarse grained sand, subangular to subrounded; coarse gravel up to 38 mm, subangular to subrounded; poorly sorted; contains	220		
					CLAY (CL): massive.	light olive brown (2.5Y 5/3), 80% clay, medium plasticity; 20% silt; firm,			
225					alteration; ve	light olive brown (2.5Y 5/4), 80% clay, medium plasticity; 20% silt; with visible ary faint laminations, gray and yellowish-brown slicken sides, 1 to 3 mm balls of an oxide stains (vertical).	225		
230							230		
235			Zone		yellow, very		235		
240			#2			light yellowish brown (10YR 6/4), 100% fine to coarse grained sand, o subrounded, 5% coarse grains; poorly sorted; wet sample; contains quartz, d chert.	240		
245			SC: 23,705 · · · uS/cm		ODAVEL (O	MAN Fight cells with house (40VD C/A) 000/ Fig. to accompany to the 75 years.	245		
243					subrounded sample; con SILT (ML): c	W): light yellowish brown (10YR 6/4), 90% fine to coarse gravel up to 75 mm, 10% medium to coarse grained sand, subrounded; poorly sorted; moist tains quartz; basal gravel. live yellow (2.5Y 6/8), 80% silt; 20% clay; yellowish-brown and light gray ly laminated, very stiff.		SIE	:VE
250						pale olive (5Y 6/4), 80% clay; 20% silt; with visible alteration; oxidized, thinly	250		os. opiispoori sampie
					massive.	very dark greenish gray (5GY 3/1), 100% clay, high plasticity; moist sample; dark olive gray (5Y 3/2), 100% clay, high plasticity; moist sample.			on sample
255			_			very dark greenish gray (5GY 3/1), 100% clay, high plasticity; moist sample;	<u>255</u>		
					CLAY (CL): laminated.	pale olive (5Y 6/4), 80% clay; 20% silt; with visible alteration; oxidized, thinly		≥ P1	TS Fig
260					30% mediun	Y (CL): olive (5Y 5/3), 70% clay, stiff, massive, oxidized clay balls, 1 to 2 mm; n to coarse grained sand; contains evaporites, gypsum, with visible alteration; own mottling; compression slicken sides.	260		GNAD. Grad sarriple F13. Spirispoor submitted for analysis
265						Y (CL): olive (5Y 5/3), 70% clay, stiff; 30% medium to coarse grained sand, o subrounded, <2% coarse grains, predominantly quartz.	265		or ici
					SAND (SP): graded; 10%	o subtothided, <276 coarse grains, predominantly quality. olive gray (5Y 5/2), 90% medium to coarse grained sand, subangular, poorly fine to coarse gravel up to 25 mm, subangular, granitic; trace silt; trace clay; artz, feldspar and mica.			analysis oleve.
270			_			olive (5Y 5/3), 85% clay, low plasticity; 15% silt; moist sample. pale olive (5Y 6/3), 100% medium to coarse grained sand, subangular to	270		Graboso
Casasi	ence Support Se	nyione Inc	*7one to	st details are for C	subrounded subangular t chert; yellow	trace dark minerals, water film on sand grains; trace fine gravel up to 4.8 mm, o subrounded; wet sample; contains quartz, feldspar, mica, amphibole, and ish-brown and reddish-brown mottling.			SIEVE: GIAD SIEVED DY GSSI



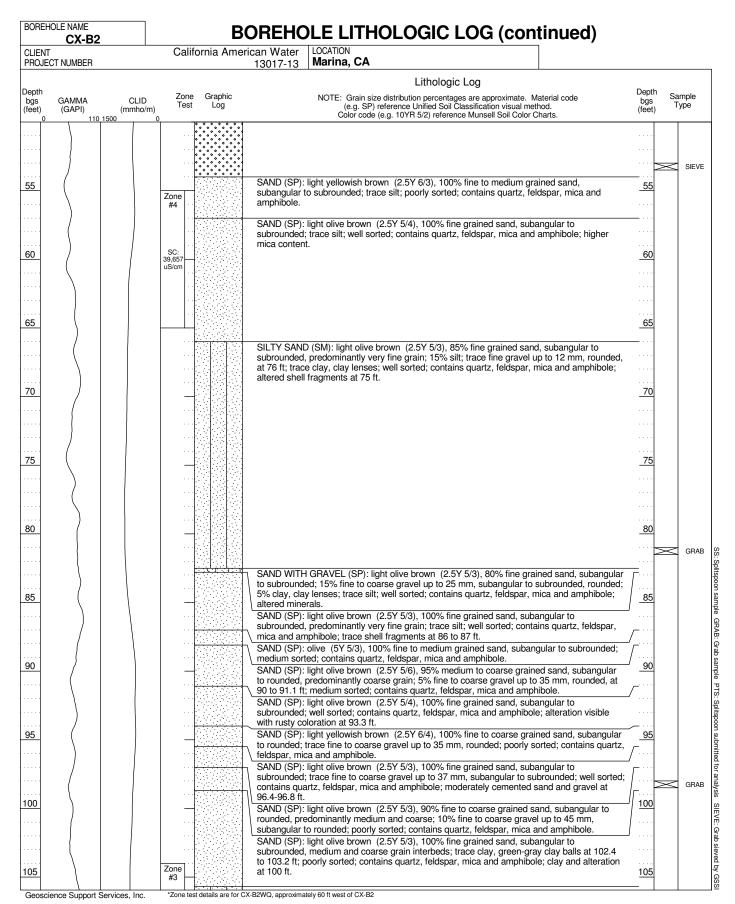
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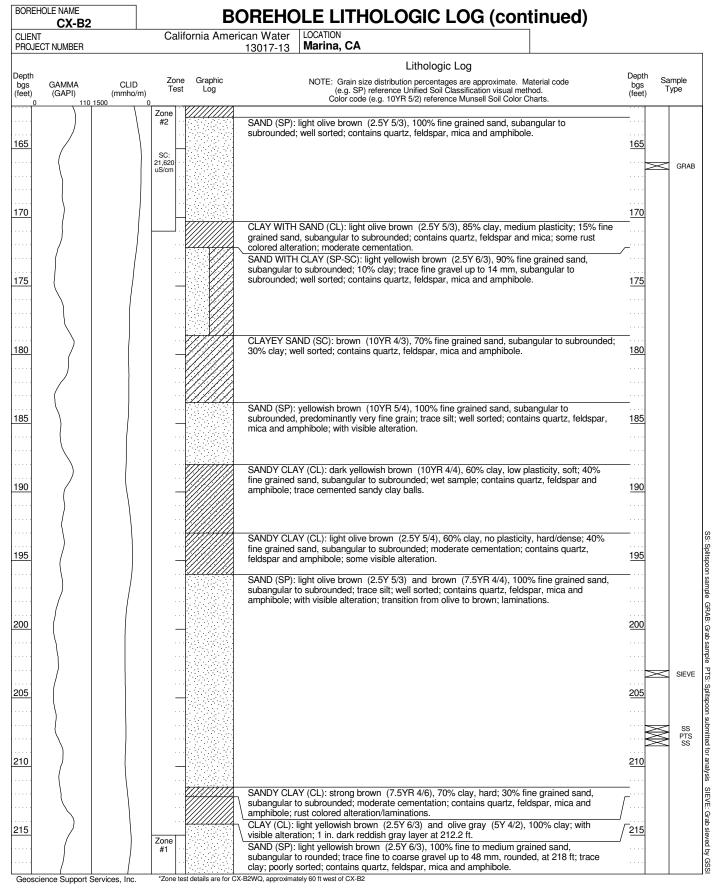


CX-B2 CLIENT PROJECT NUMBER		Cali	fornia Ame	rican Water 13017-13	Marina, C	A apis Plant	LOGIC LOG			
REPORT DATE DRILLING CONTRACT	OR		Caso	7/8/2014 ade Drilling	36° 42' 46.2630 LOGGED BY	5", -121°48' 13.4316"	Geographic NAD83			
DRILLER	On		Jo	se Munguia	N. Reyno					
ORILLING RIG TYPE	Prosoni	c 600T	DRILLING METHOD		Sonic	START DATE	11/04/13	BOREHOLE DIAMETER		6.25 in
SURFACE ELEVATION		32.0 ft	TOTAL DEPTH		307 ft bgs	FINISH DATE	11/07/13	CORE SIZE		4 in
						Litholo	ogic Log			
epth ogs GAMMA eet) (GAPI)	CLID (mmho/m	Zone Test			NOTE: Grair (e.g. S Color co	size distribution perce SP) reference Unified S ode (e.g. 10YR 5/2) refe	ntages are approximate. M ioil Classification visual met erence Munsell Soil Color C	aterial code hod. harts.	Depth bgs (feet)	Sample Type
							fine to medium grained m, rounded; trace silt; p			
				quartz, felds	par and amphi	bole; shell fragments		<u> </u>	<i></i>	
				subrounded	; moderate cen	nentation; decompos	sing minerals, shell fragr fine to medium grained s	nents.	<u> </u>	
5 \		_		subrounded			orted; contains quartz, fe		_ 5	
				amphibole.						
\										
0							edium grained sand, sul		10	
							quartz, feldspar and amp 00% fine to medium gra			
}							medium sorted; contain			
				аттріпроте.						
5									15	
							ım grained sand, subanç ı, feldspar and amphibol			
									20	
						5Y 5/3), 70% silt; 30° lartz, feldspar and a	% fine to medium graine mphibole: interbed.	ed sand, subangular		
				SAND (SP):	light yellowish	brown (2.5Y 6/4), 1	00% fine to medium grantains quartz, feldspar a		·	
				interbeds.	io subrouriaca,	medium sorted, cor	nama quanz, reidapar ar	ia ampilibole, gray		
5 /		_							_25	
) 		predominant	tly fine; well so	ted; contains quartz	ım grained sand, subanç ı, feldspar and amphibol	e.		
0 \		_		\ silt; medium	sorted; dry sai	nple; contains quart	ained sand, subangular z, feldspar and amphibo	le; ; powdery.	<u>_30</u>	
				SAND (SP): subrounded	light yellowish ; medium sorte	brown (2.5Y 6/4), 1 d; contains quartz, f	00% medium grained sa eldspar and amphibole.	and, subangular to		
		,								
5 \							100% fine to coarse grai se; poorly sorted; contain		35	
)		-		mica and an	nphibole.	•				
(
<u> </u>		_							40	
(
									45	
<u>. </u>									45	
60				X-B2WQ, approxima					50	

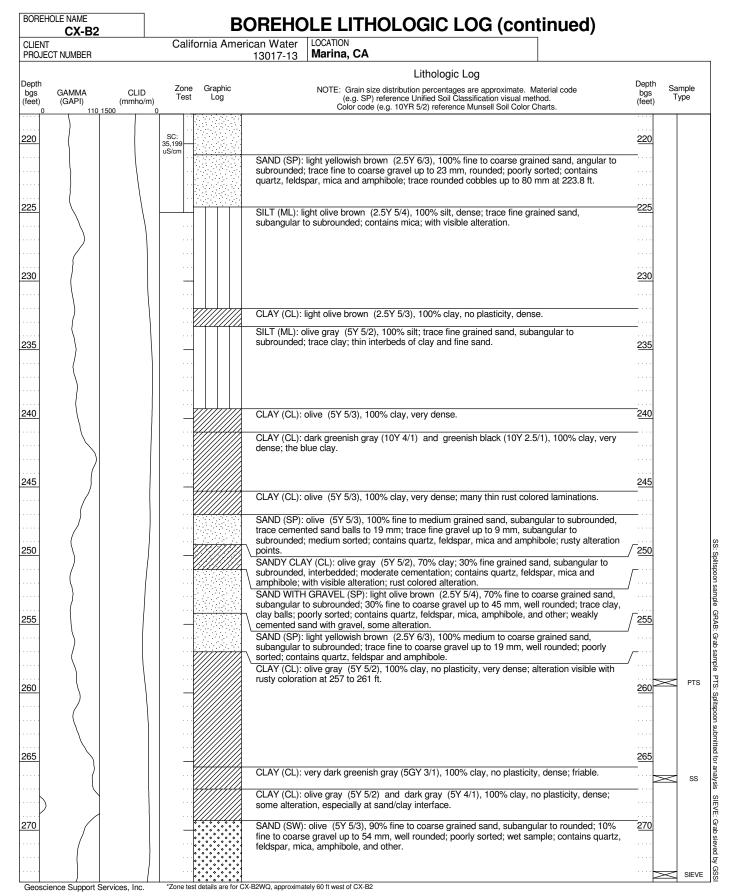
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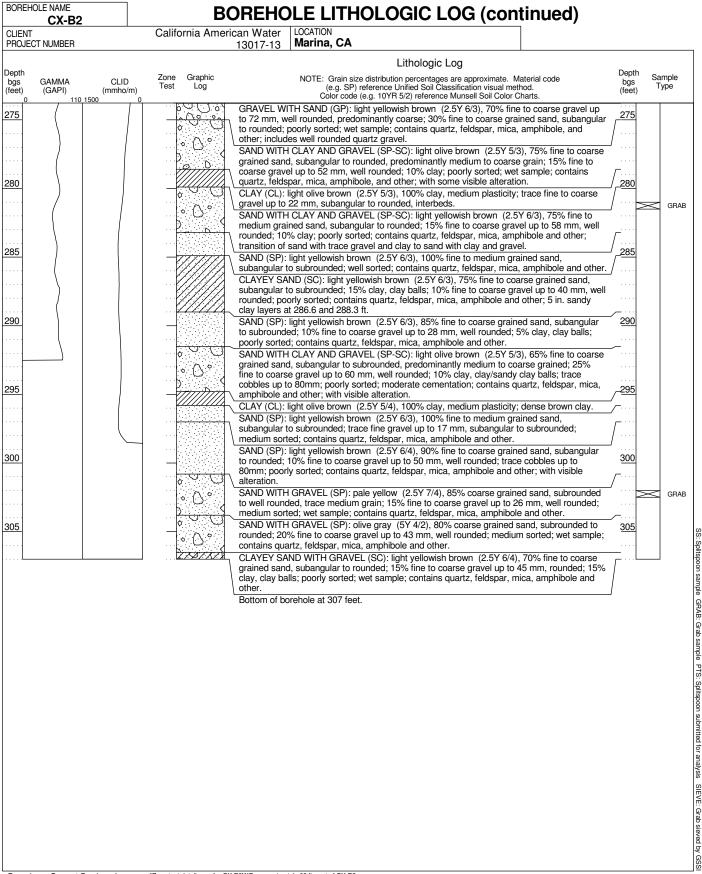


BOKEH	OLE NAME CX-B2			B	OREHOLE LITHOLOGIC LOG (continued)			
CLIENT	CT NUMBER	1	Califo		ican Water LOCATION Marina, CA			
HOOL	JI NOWIDEN				Lithologic Log			
Depth bgs feet)	GAMMA (GAPI)	CLID (mmho/m)	Zone Test	Graphic Log	NOTE: Grain size distribution percentages are approximate. Material code (e.g. SP) reference Unified Soil Classification visual method. Color code (e.g. 10YR 5/2) reference Munsell Soil Color Charts.	Depth bgs (feet)		mple ype
110			SC: 40.173 uS/cm		SILTY SAND (SM): light olive brown (2.5Y 5/3), 85% fine grained sand, subangular to subrounded, very fine grain; 15% silt; well sorted; contains quartz, feldspar, mica and amphibole; shell fragments at 114.2 and 115.8 ft.	110		
15						115		
		\					=	SIEVE
20					SAND WITH GRAVEL (SP): olive brown (2.5Y 4/4), 70% fine to coarse grained sand, subangular to rounded; 30% fine to coarse gravel up to 30 mm, rounded; poorly sorted; contains quartz, feldspar, mica and amphibole. CLAY (CL): olive (5Y 5/3), 100% clay, high plasticity; trace coarse gravel up to 55 mm, at 119-120 ft; alteration visible with rusty coloration at 121 to 121.6 ft.	/ 		
					119-120 II, alteration visible with rusty coloration at 121 to 121.6 II.			
25			· · · · · · · · · · · · · · · · · · ·	//////	SAND (SP): light yellowish brown (2.5Y 6/3), 100% fine to medium grained sand, subangular to subrounded; medium sorted; contains quartz, feldspar, mica and amphibole.	125		
30						130		
							\times	GRAE
35						135		
40			-		SAND (SP): light yellowish brown (2.5Y 6/4), 100% fine grained sand, subangular to subrounded; well sorted; contains quartz, feldspar, mica and amphibole.	140	~	SIEVE
			2	7/7//	CLAYEY SAND (SC): light yellowish brown (2.5Y 6/4), 75% fine grained sand, subangular to subrounded; 25% clay, clay lenses; well sorted; weak cementation; contains quartz, leldspar, mica and amphibole; with visible alteration.			O.E.T.
45					SILTY SAND (SM): light olive brown (2.5Y 5/4), 85% fine grained sand, subangular to subrounded; 15% silt; trace fine to coarse gravel up to 55 mm, well rounded, at 143.8 ft; trace clay, clay lenses; well sorted; contains quartz, feldspar, mica and amphibole.	145		
50				1//	SAND WITH CLAY (SP-SC): light olive brown (2.5Y 5/3), 85% fine to medium grained sand, subangular to subrounded, trace coarse; 10% clay, clay chips; 5% fine gravel up to 19 mm, subangular to subrounded; medium sorted; contains quartz, feldspar, mica and amphibole; with visible alteration; complex sample.	_150		
					SAND (SP): light olive brown (2.5Y 5/3), 100% fine grained sand, subangular to subrounded; well sorted; contains quartz, feldspar, mica and amphibole; trace 40 mm cemented sand piece at 149.8 ft.	<u> </u>		
55					SAND (SP): light olive brown (2.5Y 5/4), 100% fine grained sand, subangular to subrounded; well sorted; contains quartz, feldspar, mica and amphibole. SAND (SP): dark yellowish brown (10YR 4/6), 100% fine grained sand, subangular to	155	\times	GRA
~					subrounded, cemented sand balls; trace clay; well sorted; contains quartz, feldspar, mica and amphibole; alteration visible with rusty coloration at 153.3 ft.			
50					SILTY SAND (SM): yellowish brown (10YR 5/4), 70% fine grained sand, subangular to subrounded; 30% silt; well sorted; contains quartz, feldspar and amphibole.	160		
		\			CLAY (CL): light olive brown (2.5Y 5/3), 100% clay, high plasticity; very dense.			



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ROHEHO	LE NAME CX-B3				BC	PREHO	LE LITI	HOLOGIC LO	j		
CLIENT PROJEC	T NUMBER	1	Cali	fornia Amei	rican Water 13017-13	LOCATION Marina, C	A				
REPORT					7/8/2014	CEMEX L	apis Plant 6", -121° 47' 59.	9316" Geographic NAD83			
ORILLING ORILLER	CONTRACTO)R			ade Drilling se Munguia	N. Reyno	lds				
ORILLING		Proson	nic 600T	DRILLING METHOD	oc Mangaia	Sonic	START DATE	11/09/13	BOREHOLE DIAMETER		6.25 in
SURFACI ELEVATION	E		39.0 ft	TOTAL DEPTH		347 ft bgs	FINISH DATE	11/14/13	CORE		4 in
ELEVAIN	OIN		00.0 11	DEFIN		017 11 2go		ithologic Log	SIZE		
epth bgs feet) 0	GAMMA (GAPI)	CLID (mmho/				NOTE: Graii (e.g. Color c	n size distribution SP) reference Ur	percentages are approximate. M ified Soil Classification visual met /2) reference Munsell Soil Color C	aterial code hod. harts.	Depth bgs (feet)	Sample Type
5		500			SAND (SP): subrounded amphibole. SAND (SP): rounded, pri amphibole. SILT WITH dry sample/	c dark brown (1 edominantly fin first 7 ft disturb c pale yellow (2 pale yellow (2 predominantly c light olive browedominantly fin SAND (ML): lig powdery.	OYR 3/3), 95% e grained; 5% ed sample. 2.5Y 7/4), 100% y fine grained; wn (2.5Y 5/3), e grained; med; htt gray (5Y 7/4), 100%	of fine to medium grained sand silt; medium sorted; contains of fine to medium grained sand medium sorted; contains quart 100% fine to medium grained lium sorted; contains quartz, if 2), 85% silt; 15% fine grained of fine grained sand, subangul.	I, subangular to quartz, feldspar and I, subangular to tz, feldspar and sand, subangular to eldspar and sand, subangular to eldspar and sand, subrounded;		
30					SAND (SP): rounded, pro amphibole.	led; 5% silt; me : light olive brovedominantly fin	vn (2.5Y 5/3), e grained; med	5/4), 95% fine to medium grain ontains quartz, feldspar and a 100% fine to medium grained lium sorted; contains quartz, i trace fine grained sand; dry s	mphibole. sand, subangular to eldspar and	30	
40					SAND (SP): subrounded	light yellowish to rounded; m	brown (2.5Y 6 edium sorted; 6 brown (2.5Y 6	5/3), 100% fine to medium grazontains quartz, feldspar and fine to medium grazontains quartz, feldspar and fine grained sand, sorted; contains quartz, feldsp	ined sand, amphibole. subangular to	40	
50	nce Support Se	anda !			amphibole.					45	SIEVE

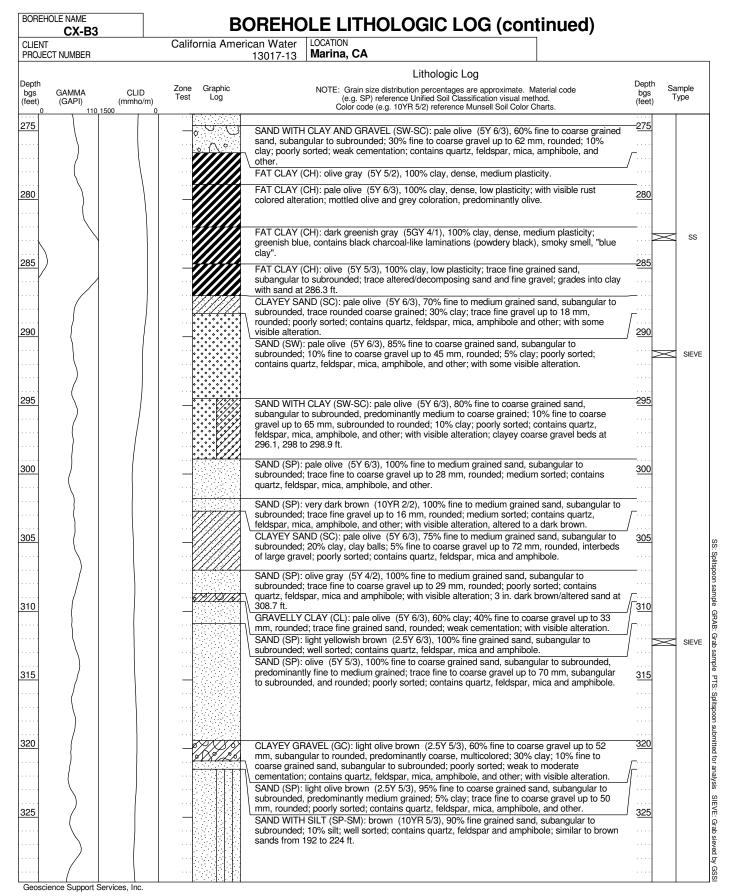
BOREHO	CX-B3		B	OREHOLE LITHOLOGIC LOG (continued)		
CLIENT PROJEC	T NUMBER	Califo	ornia Amer	rican Water LOCATION 13017-13 Marina, CA		
TIOULO	TNOWDER			Lithologic Log		
epth ogs	GAMMA CL		Graphic Log	NOTE: Grain size distribution percentages are approximate. Material code (e.g. SP) reference Unified Soil Classification visual method.	Depth bgs	Sample Type
eet)	(GAPI) (mmh	0		Color code (e.g. 10YR 5/2) reference Munsell Soil Color Charts.	(feet)	.,,,,,
				SAND (SW): light yellowish brown (2.5Y 6/4), 100% fine to coarse grained sand, subangular		
	\			to rounded; poorly sorted; contains quartz, feldspar, mica and amphibole.		
				SAND (SP): light olive brown (2.5Y 5/3), 100% fine grained sand, subangular to subrounded; well sorted; contains quartz, feldspar, mica and amphibole.		
55_	\				_55	
	/					
				SAND (SP): light yellowish brown (2.5Y 6/4), 100% fine to medium grained sand, subangular to subrounded, predominantly fine grained; medium sorted; contains quartz,		
	}			feldspar, mica and amphibole.		
60_				SAND (SP): light yellowish brown (2.5Y 6/3), 100% fine to coarse grained sand, subrounded to rounded, predominantly medium to coarse grained; trace fine gravel up to 15 mm,	60	
				rounded; poorly sorted; contains quartz, feldspar, mica, amphibole, and other. SAND (SP): light olive brown (2.5Y 5/4), 100% fine grained sand, subangular to	/[
				subrounded; well sorted; contains quartz, feldspar, mica and amphibole.	/r	
 35	}			SAND (SW): light yellowish brown (2.5Y 6/3), 100% fine to coarse grained sand, subrounded to rounded; trace fine gravel up to 15 mm, rounded; poorly sorted; contains	65	
)			quartz, feldspar, mica, amphibole, and other. SAND (SP): light olive brown (2.5Y 5/4), 100% fine grained sand, subangular to	1	
				subrounded, trace medium grained; medium sorted; contains quartz, feldspar, mica and		
)			amphibole; higher mica content. SAND (SP): light olive brown (2.5Y 5/3), 95% fine grained sand, subrounded, very fine	ا	
0				grained; 5% silt; well sorted; contains quartz, feldspar, mica and amphibole; higher mica content.	70	
)			Control in		
<u>'5</u>)				75	
)					
	{					
80		-			_80	
						S GRA
35_					_85	
	\					
				SAND (SP): olive yellow (2.5Y 6/6), 95% fine to medium grained sand, subrounded to		
00) \			rounded; 5% silt; poorly sorted; contains quartz, feldspar, mica, amphibole, and other.	90	
	(
	\		,	SAND WITH GRAVEL (SP): light yellowish brown (2.5Y 6/4), 75% medium to coarse grained sand, subrounded to rounded, trace fine grained; 20% fine to coarse gravel up to 32		
	}		$\circ \circ \circ$	mm, rounded; 5% clay, sandy clay balls; poorly sorted; contains quartz, feldspar, mica,		
5			00	amphibole, and other.	95	
	}		유위	SAND WITH SILT (SP-SM): light yellowish brown (2.5Y 6/4), 90% fine grained sand,		
	\		50()0	subangular to subrounded; 10% silt, silty sand balls; well sorted; contains quartz, feldspar, mica and amphibole; with visible alteration.		
				GRAVEL WITH SAND (GP): light yellowish brown (2.5Y 6/4), 60% fine to coarse gravel up	/ ::::	
00	/			to 48 mm, rounded; 40% medium to coarse grained sand, subrounded to rounded; poorly sorted; contains quartz, feldspar, mica, amphibole, and other.	100	
				SAND (SW): light yellowish brown (2.5Y 6/4), 100% fine to coarse grained sand,		
	(subrounded to rounded; trace fine gravel up to 10 mm, subrounded; poorly sorted; contains		
				quartz, feldspar, mica, amphibole, and other.	<u>_</u>	S GRA
05	1 1 1	1 1	4 1 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	SAND (SP): light olive brown (2.5Y 5/4), 100% fine grained sand, subangular to	105	1

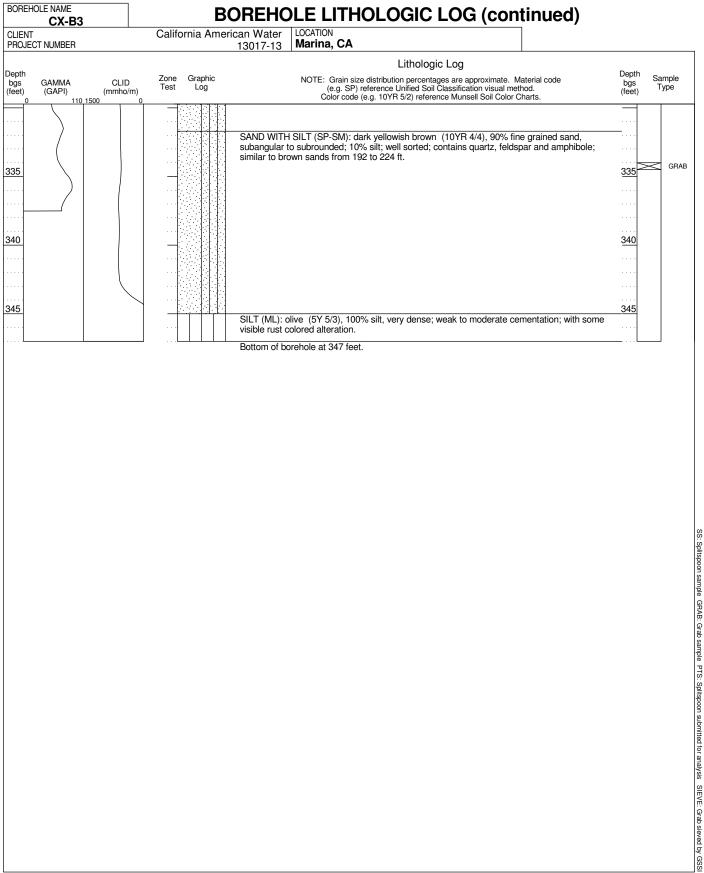
OREHOLE NA C	X-B3	B	OREHOLE LITHOLOGIC LOG (continued)			
CLIENT ROJECT NUM		California Amer	ican Water LOCATION Marina, CA			
HOULGT NOW	IDEN		10017 10 7			
epth		7 O	Lithologic Log	Depth	0	
ogs GAM eet) (GA		Zone Graphic Test Log	NOTE: Grain size distribution percentages are approximate. Material code (e.g. SP) reference Unified Soil Classification visual method. Color code (e.g. 10YR 5/2) reference Munsell Soil Color Charts.	bgs (feet)		mple /pe
			visible alteration.			
		0 0	SAND WITH GRAVEL (SP): light yellowish brown (2.5Y 6/4), 80% fine to coarse grained sand, subangular to rounded, predominantly medium to coarse grained; 20% fine to coarse		\approx	SS PT
	\	· O °	gravel up to 58 mm, subrounded to rounded; trace clay; poorly sorted; contains quartz,		$\widehat{}$	SS
0	/		feldspar, mica, amphibole, and other.	110		
·· /						
1		0 0				
'	\					
5		00		115		
			SILTY SAND (SM): light olive brown (2.5Y 5/3), 85% fine grained sand, subrounded, very			
.] ['		fine grained; 15% silt; well sorted; contains quartz, feldspar, mica and amphibole.			
. '	\					
0				100		
4				120		
) \				\sim	SIE
1	{ \					
	\ \					
5				125		
)		SAND WITH SILT AND GRAVEL (SP-SM): light olive brown (2.5Y 5/3), 75% fine grained	<u></u>		
		//////	sand, subrounded; 15% fine to coarse gravel up to 27 mm, rounded, multi-colored; 10% silt; well sorted; contains quartz, feldspar, mica and amphibole; with visible alteration.	<i> </i>		
	/ \		SILTY SAND (SM): light olive brown (2.5Y 5/3), 85% fine grained sand, subrounded, very	1		
0	/ \		fine grained; 15% silt; well sorted; contains quartz, feldspar, mica and amphibole. FAT CLAY (CH): dark gray (5Y 4/1), 100% clay, medium plasticity, dense/hard.	130	\sim	PΊ
			SILT (ML): pale olive (5Y 6/3), 100% silt, dense; visible alteration/rust colored laminations.	_		
	1		SAND (SP): light olive brown (2.5Y 5/4), 100% fine grained sand, subrounded, very fine	-:::		
			\ grained; well sorted; contains quartz, feldspar, mica and amphibole; with visible alteration.	<i></i>		
_		2 2 2 2 2 2 2 2	SILT (ML): olive gray (5Y 5/2), 100% silt; with visible alteration. SAND (SP): light yellowish brown (2.5Y 6/4), 95% fine to medium grained sand, subangular			
<u>5</u>			to subrounded, grades to predominantly medium grained sand at 135 ft; 5% silt; poorly	135		
			sorted; contains quartz, feldspar, mica and amphibole.	<u></u>		
1			SILT (ML): olive (5Y 5/3), 100% silt; visible alteration/rust colored laminations.			
	/					
<u>o</u> (SAND (SP): pale olive (5Y 6/3), 100% fine to medium grained sand, subangular to	140		
. \			subrounded, predominantly medium grained; medium sorted.			
)					
	1					
5	\		CLAYEY SAND (SC): pale olive (5Y 6/3), 70% fine to coarse grained sand, subangular to rounded; 20% clay; 10% fine to coarse gravel up to 40 mm, well rounded, especially at 144.5	145		
			to 145 ft; poorly sorted; contains quartz, feldspar, mica, amphibole, and other, visible rust			
	/		\ colored alteration. \ FAT CLAY (CH): pale olive (5Y 6/3), 100% clay, dense; medium plasticity.	J		
	′		CLAYEY SAND (SC): pale olive (57 6/3), 70% fine to coarse grained sand, subrounded to	⁷		
<u>.</u> }			rounded; 30% clay; trace fine to coarse gravel up to 25 mm, subangular; poorly sorted; with visible alteration; contains guartz, feldspar, amphibole, and other.			
<u> </u>			visiono arteration, contamo quartz, retospar, amprilidote, arto otrier.	150		
1)			SANDY FAT CLAY (CH): pale olive (5Y 6/3), 70% clay, medium plasticity; 30% fine to			
			medium grained sand, subangular to subrounded; contains quartz, feldspar, amphibole, and other; some visible alteration with rusty coloration.			
. \			FAT CLAY (CH): pale olive (5Y 6/3), 100% clay, medium plasticity; visible alteration/rust			
5 (colored laminations.	<u>155</u>		
. \		111111	SILTY SAND (SM): pale olive (5Y 6/3), 85% fine grained sand, subrounded to rounded; 15% silt; well sorted; contains quartz, feldspar and amphibole.	<i>_</i>		
			FAT CLAY (CH): olive (5Y 5/3), 100% clay, low plasticity; trace fine grained sand,	′		
			\ subangular to subrounded; some rust colored alterations.	<i>]</i> ·····		
0)		SAND WITH SILT (SP-SM): pale olive (5Y 6/3), 90% fine grained sand, subangular to subrounded, altered sand layers, rust and white coloration; 10% silt; trace fine to coarse	160		
	(gravel up to 38 mm, rounded; trace clay, clay balls; well sorted; contains quartz, feldspar,	[
1	1	[[조단성(중단]	mica, amphibole, and other.]		

JUI ILII	OLE NAME CX-B3	B	OREHO	LE LITHOLOGIC LOG (con	tinued)			
CLIENT	CT NUMBER	California Amer		LOCATION Marina, CA				
NOJE	OT NOWIDEN		13017-13	Lithologic Log				
epth		Zone Graphic		LITHOLOGIC LOG NOTE: Grain size distribution percentages are approximate. M	aterial code	Deptl		ample
ogs feet) 0	GAMMA CLID (GAPI) (mmho/m)	Test Log		(e.g. SP) reference Unified Soil Classification visual met Color code (e.g. 10YR 5/2) reference Munsell Soil Color C	hod.	bgs (feet	т	ype
		000		I CLAY AND GRAVEL (SW-SC): yellowish brown (10YR 5 led sand, subangular to rounded; 15% fine to coarse grave				
)		rounded; 10°	% clay; poorly sorted; contains quartz, feldspar and amphil		<u> </u>		
65	/	-, $-$	of sands. SAND (SP):	strong brown (7.5YR 5/8), 85% medium to coarse grained	d sand, subrounded to	<u>165</u>		
				edominantly coarse grained; 10% fine to coarse gravel up torly sorted; contains quartz, feldspar, amphibole, and other				
			alteration.		· •][
	/			I CLAY AND GRAVEL (SP-SC): pale olive (5Y 6/3), 75% r d, subangular to rounded; 15% fine to coarse gravel up to 3				
70	\	-		sorted; contains quartz, feldspar, amphibole, and other; co		<u> 170</u>		
			gravel up to	light yellowish brown (2.5Y 6/4), 95% clay, low plasticity; 5 42 mm, subrounded to rounded, interbedded; trace mediu				
		000	SAND (SP):	to rounded. pale olive (5Y 6/3), 100% fine to medium grained sand, si	ibangular to][
		000	subrounded;	trace fine to coarse gravel up to 40 mm, subrounded to ro	unded; trace clay;			
75			poorly sorted weakly ceme	d; contains quartz, feldspar, amphibole, and other, with visi ented sands.	ble alteration; trace	175		
				GRAVEL (CL): pale olive (5Y 6/3), 85% clay; 10% fine to angular to rounded: 5% fine grained sand, subangular to su		1		
		000	alteration of	minerals/rock.	<u> </u>][\approx	SS PTS SS
		1 P101		ND WITH GRAVEL (SC): pale olive (5Y 6/3), 70% fine to to subrounded; 15% fine to coarse gravel up to 75 mm, rou		<u></u>		SS
30)		balls; poorly	sorted; well graded; contains quartz, feldspar, amphibole,		<u>180</u>		
				minerals/rock. AY (CL): pale olive (5Y 6/3), 70% clay; 25% fine to coarse	grained sand,	JI		
			subangular t	to subrounded; 5% fine to coarse gravel up to 25 mm, subrartz, feldspar, amphibole, and other, visible alteration with r	ounded to rounded;			
			CLAYEY SA	ND WITH GRAVEL (SC): pale olive (5Y 6/3), 70% fine to	coarse grained sand,	4		
35				to subrounded; 15% fine to coarse gravel up to 33 mm, sub porly sorted; well graded; contains quartz, feldspar, amphib		185		
			moderately of	cemented sand layer at 178.2-178.7 ft.]		
			up to 70 mm	SILT (ML): light yellowish brown (2.5Y 6/3), 60% silt; 30%, rounded, coarse grained at 179.6 ft; 10% fine grained sa	nd, subangular to	<u> [</u>		
				; moderately cemented sand and gravel layer at 180.8-181 uphibole, and other.	.8 ft; contains quartz,	lr		
90)		SAND (SP):	light yellowish brown (2.5Y 6/4), 100% fine to medium gra		190		
	/			to subrounded, predominantly medium grained; trace fine good ce clay, clay lens; medium sorted; contains quartz, feldspa		I		
				olored alteration of sands at 186.8 to 187.3 ft. olive (5Y 5/3), 100% clay, low plasticity; trace fine grained	cand cubangular to	1		
			subrounded;	some alteration visible with rusty coloration.]		
95				AY (CL): pale olive (5Y 6/3), 70% clay, low plasticity; 30% figular to subrounded; trace fine to coarse gravel up to 30 m		195		
			subrounded;	contains quartz, feldspar, mica, amphibole, and other, wit	h visible alteration.]		
			alteration.	olive (5Y 5/3), 100% clay, low plasticity, dense; with visible	e rust colored	<u> </u> г	\cong	SS PTS
				yellowish brown (10YR 5/4), 95% fine grained sand, suba sorted; contains quartz, feldspar and amphibole.	ngular to subrounded;			
00			SAND (SP):	dark yellowish brown (10YR 4/4), 95% fine grained sand,		200		
)		subrounded;	; 5% silt; well sorted; contains quartz, feldspar and amphibe	ole.			
								GRA
)						\frown	GRA
)5	/			brown (7.5YR 4/3), 95% fine grained sand, subangular to contains quartz, feldspar and amphibole.	subrounded; 5% silt;	205		
	/							
0				dark brown (10YR 3/3), 95% fine grained sand, subangular	ar to subrounded; 5%	<u>–210</u>		
			Siit, well soft	ed; contains quartz, feldspar and amphibole.				
_ _)							
15	\					215		
	/							
			SAND (SP):	dark grayish brown (10YR 4/2), 95% fine grained sand, sa	ubangular to			

	CX-B3			OREHOLE LITHOLOGIC LOG (continued)			
ROJE	CT NUMBER	Califo	ornia Ameri	ican Water LOCATION 13017-13 Marina, CA			
				Lithologic Log			
epth ogs	GAMMA CI	LID Zone		NOTE: Grain size distribution percentages are approximate. Material code	Depth bgs	Sai	mple
eet)		ho/m) Test	Log	(e.g. SP) reference Unified Soil Člassification visual method. Color code (e.g. 10YR 5/2) reference Munsell Soil Color Charts.	(feet)	Ту	/pe
	110 1500			subrounded; 5% silt; well sorted; contains quartz, feldspar and amphibole; with some visible			
20)			alteration; cementation at 219 and 224 ft.	220		
		1					
	/						
25		\		SILT (ML): dark brown (10YR 3/3), 95% silt; 5% fine grained sand, subangular to	225		
		/		subrounded.			
		/		CLAY (CL): olive (5Y 5/3), 100% clay, no plasticity, dense; alteration visible with rust			
		\		colored laminations below 230 ft.			
		\					
30)				230		
			///////	SAND (SP): pale olive (5Y 6/3), 90% fine to coarse grained sand, subangular to			
	(subrounded, predominantly medium grained; 10% fine to coarse gravel up to 70 mm,			
	\			rounded, interbedded; poorly sorted; contains quartz, feldspar, mica and amphibole; gravel layers at 237, 237.8, and 238.6 to 239.7 ft.			
5					235		
	\						
10					240		SIE
	\		·	SAND WITH GRAVEL (SW): pale olive (5Y 6/3), 85% fine to coarse grained sand,			JIL
				subangular to rounded; 15% fine to coarse gravel up to 68 mm, rounded; poorly sorted;			
)	\		contains quartz, feldspar, mica, amphibole, and other; with visible alteration.			
45	/			SAND (SP): dark grayish brown (2.5Y 4/2), 100% fine grained sand, subrounded; trace silt, cemented brown silt at 246.6 ft; well sorted; contains quartz, feldspar, amphibole, and other.	245		
				η,			
				SANDY SILT (ML): olive (5Y 5/3), 70% silt; 30% fine grained sand, subangular to			
)			subrounded; with some visible rust colored alteration.			
50			•••••	SAND (SW): pale olive (5Y 6/3), 85% fine to coarse grained sand, subangular to	250		
)			subrounded; 10% fine to coarse gravel up to 42 mm, rounded; 5% clay; poorly sorted; contains quartz, feldspar, mica, amphibole, and other; with some visible alteration; thin			
				sandy clay layers.			
 55		.			255	\sim	GR
		\		FAT CLAY (CH): pale olive (5Y 6/3), 100% clay, low plasticity, very dense; some darker fine			
)	\		laminations.			
		\					
 30		\			260		
0	\	\					
	/						
	[]	_		SILT (ML): pale olive (5Y 6/3), 100% silt; trace fine grained sand, subangular to			
]	_		subrounded; trace clay; silt with fine sand and altered sand and trace clay clasts from 262.8 to 263.9 ft; high mica content.	005		
35	(SAND (SP): olive (5Y 5/3), 100% fine to medium grained sand, subangular to subrounded;	265		
• • •	\			trace fine to coarse gravel up to 33 mm, rounded; medium sorted; contains quartz, feldspar, mica, amphibole, and other; visible rust colored alteration of sands at 268.5 ft(3in.).			
	\						
)			SAND (SP): pale olive (5Y 6/3), 90% medium to coarse grained sand, subangular to			
70	(subrounded; 10% fine to coarse gravel up to 50 mm, rounded; poorly sorted; contains quartz, feldspar, mica, amphibole, and other.	270		
	\			gaare, cooper, mou, ampinoon, and other.			
	/						
	\	1 1				\sim	GRA

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BOREHOLE NAME CX-B4				ВС	DREHO	LE LITHO	LOGIC LO	3			
CLIENT PROJECT NUMBER		Cali	fornia Ame	rican Water 13017-13	LOCATION Marina, C	Α					
REPORT DATE				7/8/2014	CEMEX L		' Geographic NAD83				
DRILLING CONTRACTO)R			ade Drilling	LOGGED BY		Geographic NAD65				
DRILLER DRILLING	Droconi	io COOT	DRILLING	se Munguia	N. Reyno	START	2/20/14	BOREHOLE			8 in
RIG TYPE SURFACE	Prosoni		METHOD TOTAL		Sonic	DATE	3/20/14	DIAMETER			
ELEVATION		39.0 ft	DEPTH		350 ft bgs	DATE	4/10/14	SIZE			6 in
Depth bgs GAMMA feet) (GAPI)	CLID (mmho/n	Zone Test			(e.g. \$	n size distribution perce SP) reference Unified	logic Log entages are approximate. M Soil Classification visual met ference Munsell Soil Color C	hod.	Depth bgs (feet)		nple pe
0 110 1 5 110 1	500		6 \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	fine to medi mm, subang amphibole; SAND (SP) rounded; 59 bgs; well so SAND (SP) subrounded and other.	H GRAVEL (SP um grained sar guar to rounder trace cobbles; to very dark gray silt; trace fine rited; contains of the pale yellow (5 lt; trace silt, tr): light olive brown id, subangular to ro d; 5% silt; medium s trace organics/roots ish brown (10YR 3 to coarse gravel up uartz, feldspar, am Y 7/4), 100% fine to e silt balls; medium	(2.5Y 5/3) and pale yell unded; 30% fine to coars sorted; contains quartz, for the contains quartz, for the contains quartz, for the contains quarts, for the contains quarts, for the contains quarts, for medium grained sand, sorted; contains quartz, medium grained sand, so	ow (2.5Y 7/3), 65% se gravel up to 70 eldspar and nd, subrounded to to rounded, at 8.5 ft subangular to feldspar, amphibole			
20				SAND (SP) subrounded	: pale yellow (5 l; medium sorte	Y 7/4), 100% fine tod; contains quartz,	o medium grained sand, feldspar, amphibole and	other. The state of the state o	20	>	GRAI
30							feldspar, amphibole and		30		
							fine grained sand, subar quartz, feldspar, mica and				
35							100% fine to medium gra ntains quartz, feldspar, a		_35		
40				subrounded	I, trace fine grai and other; trace	ned; trace silt; med	100% medium grained sa ium sorted; contains qua olive silty sand layer from	rtz, feldspar, mica,	40		
				subrounded olive/gray h	l; trace silt; well orizontal silt ler	sorted; contains quases at 42.1 ft bgs.	100% fine grained sand, uartz, feldspar, mica and 100% fine to medium gra	amphibole; trace thin	 		
45				subangular,	predominantly	medium grained, tr	rou% fine to medium gra race coarse grained; trace artz, feldspar, mica, amp	e fine gravel up to 10	45		SIEVI
50	ervices Inc								50		

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BOREHOLE NAME **BOREHOLE LITHOLOGIC LOG (continued)** CX-B4 LOCATION California American Water Marina, CA PROJECT NUMBER 13017-13 Lithologic Log Depth Depth Zone Graphic NOTE: Grain size distribution percentages are approximate. Material code (e.g. SP) reference Unified Soil Classification visual method. Sample bgs (feet) GAMMA CLID (mmho/m) bgs (feet) Log Туре (GAPI) Color code (e.g. 10YR 5/2) reference Munsell Soil Color Charts 110 1500 SAND (SP): light olive brown (2.5Y 5/3), 100% fine grained sand, subangular to subrounded, trace medium grained; well sorted; contains quartz, feldspar, mica and 55 55 SAND (SP): light yellowish brown (2.5Y 6/3), 100% fine to medium grained sand, subangular to rounded, trace coarse grained; medium sorted; contains quartz, feldspar, SS SAND (SP): olive (5Y 5/3), 100% fine grained sand, subangular to subrounded, fine to Zone medium grained at 59 to 59.7 ft bgs; trace silt; well sorted; contains quartz, feldspar, mica 60 and amphibole; higher mica content. GRAB SAND (SP): olive (5Y 5/3), 100% fine to coarse grained sand, subangular to subrounded, SC: 6,988 predominantly coarse grained; poorly sorted; contains quartz, feldspar, mica and amphibole; higher mica content. 65 65 SAND (SP): olive (5Y 5/3), 100% fine to medium grained sand, subangular to subrounded; trace silt; medium sorted; contains quartz, feldspar, mica and amphibole; higher mica SAND (SP): olive (5Y 5/3), 100% fine to coarse grained sand, subangular to subrounded, predominantly coarse grained; poorly sorted; contains quartz, feldspar, mica and amphibole; higher mica content. SAND (SP): olive (5Y 5/3), 100% fine to coarse grained sand, subangular to subrounded, 70 70 predominantly fine to medium grained, fine sand at 66.5 to 67 ft bgs; poorly sorted; contains quartz, feldspar, mica and amphibole. SAND (SP): olive (5Y 5/3), 95% fine grained sand, subangular to subrounded, very fine grained, trace fine to medium grained interbeds; 5% silt; well sorted; contains quartz, SIEVE feldspar, mica and amphibole; higher mica content; trace thin pink horizontal laminations. 75 75 80 80 SAND (SP): olive (5Y 5/3), 100% fine to coarse grained sand, subangular to subrounded; 85 85 poorly sorted; contains quartz, feldspar, mica and amphibole; very high mica content. SAND (SP): olive gray (5Y 5/2), 95% fine grained sand, subangular to subrounded, very fine grained; 5% silt; well sorted; contains quartz, feldspar, mica and amphibole. SAND (SP): light olive brown (2.5Y 5/6), 100% fine to medium grained sand, subangular to subrounded; trace fine gravel up to 11 mm, rounded; poorly sorted; contains quartz, feldspar, mica, amphibole and other; orange colored alteration. 90 90 SAND (SP): light yellowish brown (2.5Y 6/4), 95% medium to coarse grained sand, subangular to rounded, trace fine grained; 5% fine to coarse gravel up to 30 mm, rounded; trace silt; poorly sorted; contains quartz, feldspar, mica, amphibole and other; free water. 95 95 SAND WITH GRAVEL (SP): pale yellow (2.5Y 7/3) and light yellowish brown (2.5Y 6/4), 80% fine to coarse grained sand, subangular to rounded, predominantly medium to coarse grained; 15% fine to coarse gravel up to 43 mm, rounded; 5% silt; poorly sorted; contains quartz, feldspar, mica, amphibole and other; chert, many mineral types; free water. Ö Ó GRAB 100 100 0 .0 O 105 105 SAND (SP): pale olive (5Y 6/3), 100% fine to medium grained sand, subangular to subrounded; trace fine to coarse gravel up to 23 mm, rounded; poorly sorted; contains Geoscience Support Services, Inc.

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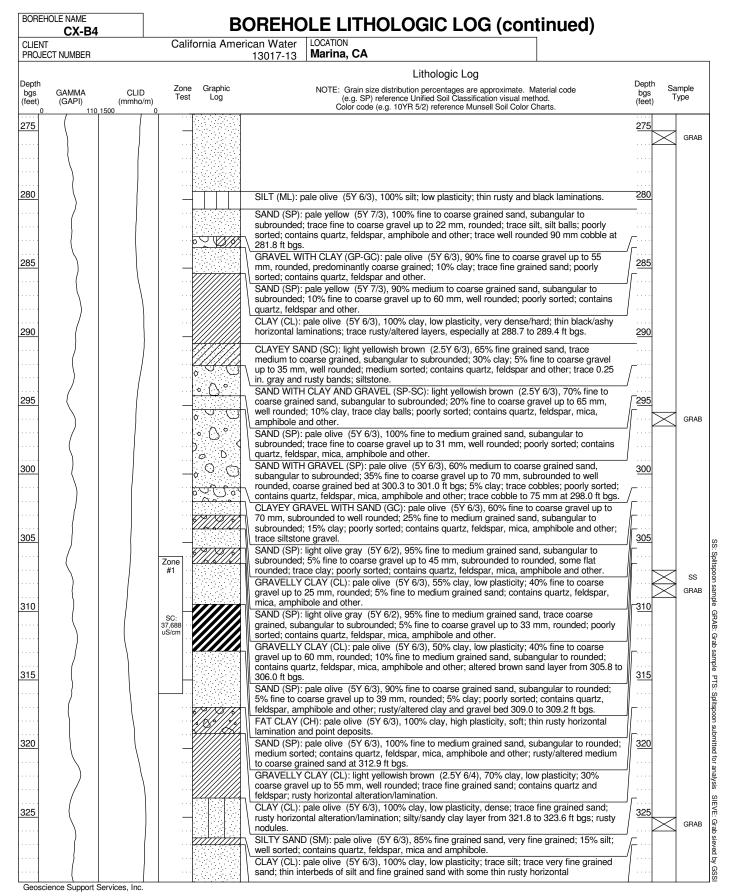
BOREHOLE NAME BOREHOLE LITHOLOGIC LOG (continued) CX-B4 California American Water Marina, CA PROJECT NUMBER 13017-13 Lithologic Log Depth Depth NOTE: Grain size distribution percentages are approximate. Material code (e.g. SP) reference Unified Soil Classification visual method. Color code (e.g. 10YR 5/2) reference Munsell Soil Color Charts. Zone Graphic Sample bgs (feet) GAMMA CLID (mmho/m) bgs (feet) Log Туре (GAPI) 110 1500 quartz, feldspar, mica, amphibole and other. SAND (SP): light yellowish brown (2.5Y 6/3), 90% fine to coarse grained sand, subangular to rounded; 10% fine to coarse gravel up to 30 mm, rounded; poorly sorted; contains quartz, feldspar, mica, amphibole and other. 110 110 SAND (SP): light olive brown (2.5Y 5/4), 100% fine grained sand, subangular to Zone subrounded; well sorted; contains quartz, feldspar, mica and amphibole. SAND (SP): light olive brown (2.5Y 5/4), 95% fine grained sand, subangular to subrounded, very fine grained; 5% silt; well sorted; contains quartz, feldspar, mica and amphibole. 115 115 SIEVE 120 120 SAND (SP): olive (5Y 5/3), 100% fine grained sand, subangular to subrounded; well sorted; contains quartz, feldspar, mica and amphibole; increase in olive coloration. SILT (ML): pale olive (5Y 6/3), 95% silt; 5% fine grained sand, subangular to subrounded, 125 125 highly altered, rust, tan and black from 124.1 to 124.9 ft bgs; low plasticity; thin rusty and black horizontal alteration/lamination. SAND WITH SILT AND GRAVEL (SP-SM): pale olive (5Y 6/3), 75% fine grained sand, subangular to subrounded, fine grained grading to medium to coarse grained silty gravelly sand; 15% fine to coarse gravel up to 41 mm, rounded; 10% silt; poorly sorted; contains quartz, feldspar, mica and amphibole; highly altered at 127.5 ft bgs. 130 130 CLAY (CL): dark gray (5Y 4/1), 100% clay, medium plasticity, dense; trace thin rust colored horizontal lamination; highly altered at 129.2 ft bgs. SILT WITH SAND (ML): olive (5Y 5/3), 80% silt, silt bed from 132.2 to 132.7 ft bgs; 20% fine grained sand, subangular to subrounded, very fine grained; contains quartz, feldspar and mica; trace thin rust colored horizontal alteration/lamination. SAND (SP): pale olive (5Y 6/3), 100% fine grained sand, subangular to subrounded, grades 135 135 to fine to medium grained; trace silt; poorly sorted; contains quartz, feldspar, mica and SAND (SP): olive (5Y 5/3), 100% fine grained sand, subangular to subrounded; well sorted; contains quartz, feldspar, mica and amphibole; highly altered/rust colored at 137.1 ft bgs. FAT CLAY (CH): olive gray (5Y 5/2), 100% clay, high plasticity, dense; trace black and rust colored lamination; trace black ashy deposits. SANDY CLAY (CL): pale olive (5Y 6/3), 60% clay, no plasticity; 40% fine grained sand, 140 140 subangular to subrounded; contains quartz and feldspar; thin black and rust colored lamination FAT CLAY (CH): pale olive (5Y 6/3), 100% clay, high plasticity, dense; thin black and rust SAND (SP): pale yellow (2.5Y 7/3), 100% fine grained sand, subangular to subrounded; well sorted; contains quartz, feldspar and amphibole; trace rust colored alteration. 145 145 SS 150 150 SANDY CLAY (CL): pale olive (5Y 6/3), 60% clay, no plasticity; 40% fine grained sand, subangular to subrounded; contains quartz and feldspar; thin black and rust colored SAND (SP): pale olive (5Y 6/3), 95% fine to medium grained sand, subangular to subrounded; 5% silt; trace fine to coarse gravel up to 22 mm, subangular; poorly sorted; 155 155 Zone contains quartz, feldspar, mica and amphibole; 2.5 in. horizontal rusty/altered band at 154 ft #3 SAND WITH GRAVEL (SP): pale olive (5Y 6/3), 80% fine to coarse grained sand, subangular; rusty/altered from 160.4 to 160.7 ft bgs; 15% fine to coarse gravel up to 52 mm, 0 Ø. subrounded to rounded; 5% clay; poorly sorted; contains quartz, feldspar, amphibole and 0 160 160

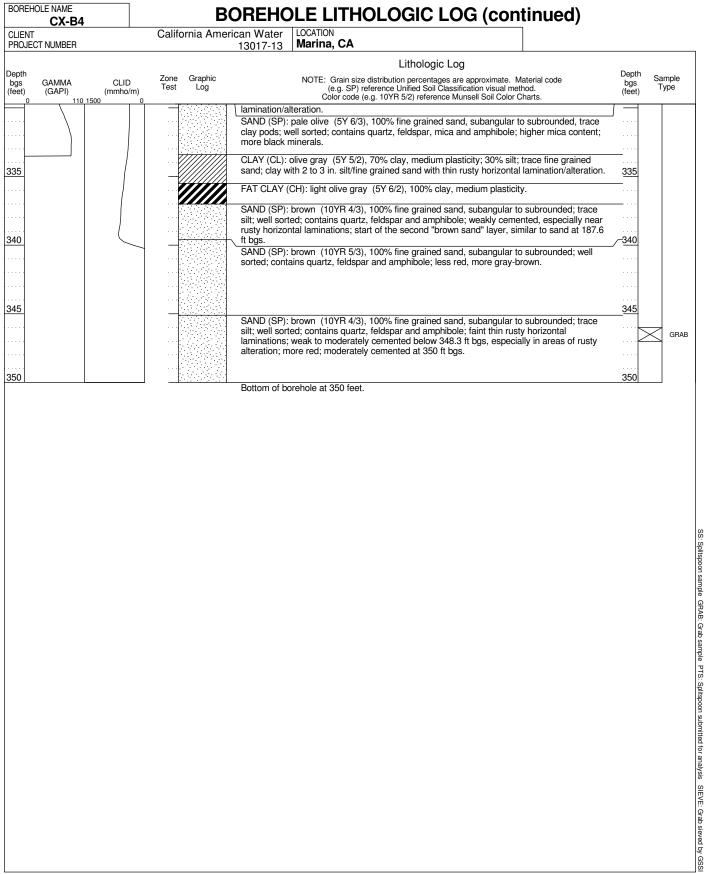
	LE NAME CX-B4				DLE LITHOLOGIC LOG (continued)		
CLIENT PROJECT	ΓNUMBER		California Ame	rican Water 13017-13	LOCATION Marina, CA		
onth					Lithologic Log	Donth	
epth ogs eet)	GAMMA (GAPI)	CLID (mmho/m)	Zone Graphic Test Log		NOTE: Grain size distribution percentages are approximate. Material code (e.g. SP) reference Unified Soil Classification visual method. Color code (e.g. 10YR 5/2) reference Munsell Soil Color Charts.	Depth bgs (feet)	Sample Type
65				up to 60 mm 10% clay; tr	ITH CLAY AND SAND (GP-GC): pale olive (5Y 6/3), 60% fine to coarse gran, subrounded to rounded; 30% medium to coarse grained sand, subangular ace cobbles; poorly sorted; contains quartz, feldspar, amphibole and other; tes up to 85 mm at 163 to 166 ft bgs; many mineral types; trace rusty alterations.	race 165	GRAE
70						170	
				SILT (ML): o	olive (5Y 5/3), 100% silt, very dense; friable; rust colored alteration and		
75			 —			175	
	}				D (SM): pale olive (5Y 6/3), 85% fine grained sand, subangular to subround m 177.3 to 177.6 ft bgs; no plasticity; well sorted; contains quartz, feldspar a	ed; ···· nd / ····	
80				grades to fir	light olive gray (5Y 6/2), 100% fine grained sand, subangular to subrounde to medium grained; trace fine gravel up to 18 mm, rounded; well sorted; artz, feldspar, mica and amphibole; rusty alteration at 177.6 ft bgs.	d, <u>180</u>	
35				grained sand contains qua	I SAND (CL): pale olive (5Y 6/3), 85% clay, low plasticity; 10% fine to mediud, subangular to subrounded; 5% fine to coarse gravel up to 36 mm, roundeartz, mica and amphibole; clay with sand and gravel interbeds; weakly cemeavel at 183.5 ft bgs; trace rusty alteration/nodules.	d; 195	
				subrounded SAND (SP):	olive gray (5Y 5/2), 100% fine to medium grained sand, subangular to ; medium sorted; contains quartz, feldspar, mica and amphibole. yellowish brown (10YR 5/6), 100% fine grained sand, subangular to ; well sorted; contains quartz, feldspar and amphibole; start of "the brown sa		
90						190	SIEVE
95						195	
					dark yellowish brown (10YR 4/6), 100% fine grained sand, subangular to; well sorted; contains quartz, feldspar and amphibole; redder coloration than	 	
00						200	
05				subrounded	dark yellowish brown (10YR 3/4), 95% fine grained sand, subangular to ; 5% silt; well sorted; contains quartz, feldspar and amphibole; trace weakly ands and sand nodules; mottled coloration.	205	
10					brown (10YR 4/3), 100% fine grained sand, subangular to subrounded; we	I 210	
				sortea; cont	ains quartz, feldspar and amphibole.		GRAE
15					strong brown (7.5YR 4/6), 100% fine grained sand, subangular to subround contains quartz, feldspar and amphibole; faint thin rusty horizontal lamination		
	\						

BOREHOLE NAME

CX-B4	C	alifornia Ameri			
PROJECT NUMBER			13017-13 Marina, CA		
epth ogs GAMMA leet) (GAPI)	(mmho/m)	one Graphic Test Log	Lithologic Log NOTE: Grain size distribution percentages are approximate. Material code (e.g. SP) reference Unified Soil Classification visual method. Color code (e.g. 10YR 5/2) reference Munsell Soil Color Charts.	Depth bgs (feet)	Sample Type
220			SAND (SP): grayish brown (2.5Y 5/2), 95% fine grained sand, subangular to subrounded; 5% silt; well sorted; contains quartz, feldspar and amphibole; weakly cemented sand and sand nodules at 220.0 to 220.3 ft bgs. SAND (SP): olive brown (2.5Y 4/4), 100% fine grained sand, subangular to subrounded; well sorted; contains quartz, feldspar and amphibole; trace thin reddish horizontal laminations. SAND (SP): dark olive brown (2.5Y 3/3), 100% fine grained sand, subangular to subrounded; well sorted; contains quartz, feldspar and amphibole; darker color/more black minerals. SILT (ML): pale olive (5Y 6/3), 100% silt, very dense; less dense from 233.4 to 234.1 ft bgs; low plasticity; rusty/highly altered at 228.6 to 229.3 ft bgs; trace thin black horizontal lamination especially at 232.5 to 233.4 ft bgs.	220	
	Zone #2 SC: 38,35- uS/cm	0 U \	SAND (SP): olive (5Y 5/3), 95% fine to medium grained sand, subangular to subrounded; 5% fine to coarse gravel up to 26 mm, well rounded; trace silt, siltstone; poorly sorted; contains quartz, feldspar, mica, amphibole and other; high mica content. SAND (SP): dark grayish brown (2.5Y 4/2), 95% medium to coarse grained sand, trace fine grained, subangluar to subrounded; 5% fine to coarse gravel up to 26 mm, well rounded; trace silt, siltstone; poorly sorted; contains quartz, feldspar, mica, amphibole and other; altered to a dark brown. SAND (SP): pale olive (5Y 6/3), 90% fine to medium grained sand, subangular to subrounded; 10% fine to coarse gravel up to 65 mm, subrounded to rounded, coarse grained gravel bed at 238.4 ft bgs; poorly sorted; contains quartz, feldspar, mica, amphibole and other; includes flat siltstone and granite. SAND (SP): dark brown (7.5YR 3/3), 90% fine to coarse grained sand, predominantly medium to coarse grained, subangular to subrounded; 10% fine to coarse gravel up to 26 mm, subrounded to rounded; trace silt; poorly sorted; contains quartz, feldspar, mica, amphibole and other; altered to a dark brown. SAND (SP): light yellowish brown (2.5Y 6/3), 90% medium to coarse grained sand, subangular to subrounded; 10% fine to coarse gravel up to 72 mm, rounded; poorly sorted; contains quartz, feldspar, mica, amphibole and other; trace weakly cemented silt chips; siltstones; many mineral types. SAND (SP): pale olive (5Y 6/3), 95% fine to medium grained sand, subangular to subrounded; 5% fine to coarse gravel up to 30 mm, subangular to subrounded; poorly sorted; contains quartz, feldspar, mica, amphibole and other; medium to coarse sand and gravelly interbeds; many mineral types. SAND WITH GRAVEL (SP): pale olive (5Y 6/3), 70% fine to coarse grained sand, subangular to subrounded; 30% fine to coarse gravel up to 45 mm, well rounded; poorly sorted; contains quartz, feldspar, mica, amphibole and other; trace 70 mm clay ball at 252.3 ft bgs; siltstone; many mineral types. GRAVEL WITH CLAY AND	235 240 245 250 255 260	SIEVI
270			CLAY (CL): olive gray (5Y 5/2), 100% clay, low plasticity, dense. SILT (ML): pale olive (5Y 6/3), 100% silt, dense; trace thin ashy black colored horizontal laminations; trace small rusty globular deposits. SILT (ML): pale olive (5Y 6/3), 90% silt, less dense than above; 10% fine grained sand, subangular to subrounded, very fine grained; silt with interbedded very fine grained sands; high mica content. SAND (SP): light olive gray (5Y 6/2), 90% fine to coarse grained sand, subangular to subrounded, predominantly medium to coarse grained; 10% fine to coarse gravel up to 50 mm, subrounded to rounded, coarse gravel deposit at 279.4 ft bgs; trace silt, flat/round	265	SS SS

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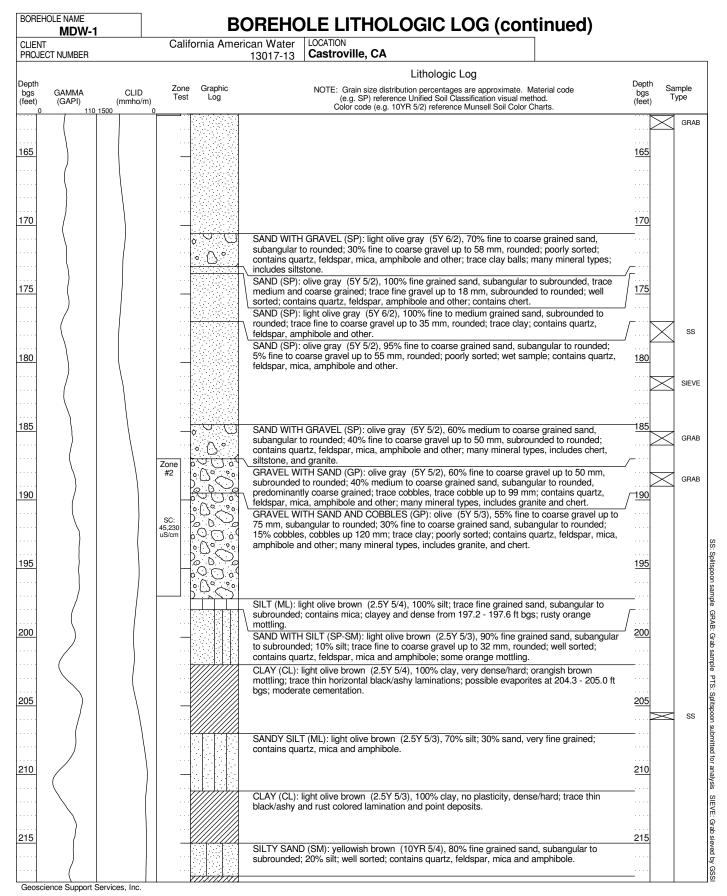




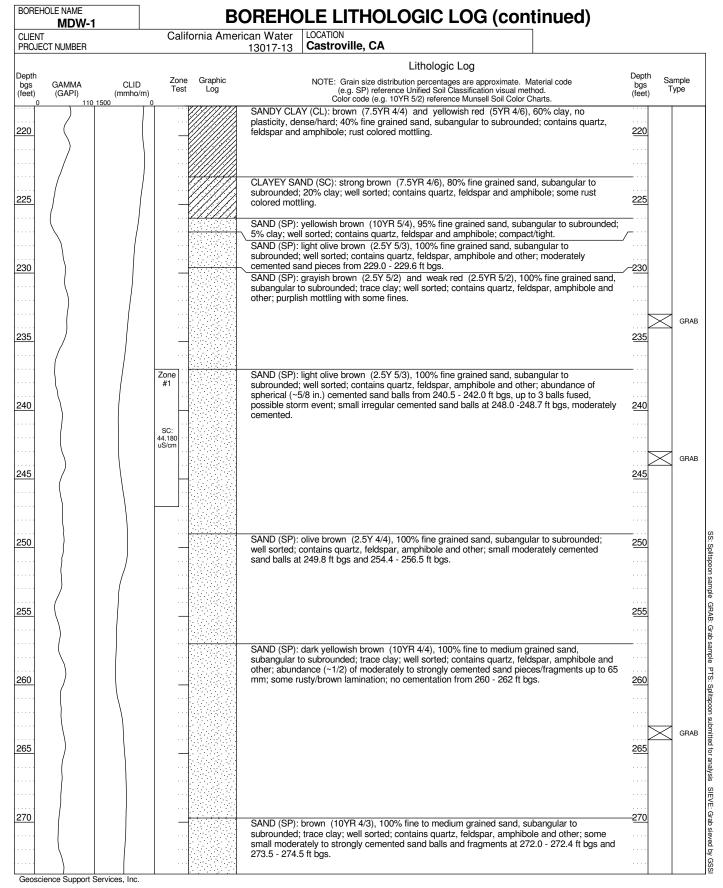
	OLE NAME MDW-1						LE LITH	HOLOGIC LO	į.			
CLIENT PROJEC	CT NUMBER		Cali	fornia Ame	erican Water 13017-13	LOCATION Castrovill	•					
EPORT	T DATE				7/8/2014		iver State Be 8", -121° 47' 41.4					
RILLIN	G CONTRACT	OR			cade Drilling ose Munquia	N. Reyno	lds					
RILLIN		Proson	nic 600T	DRILLING METHOD	oo mangana	Sonic	START DATE	4/23/14	BOREHOLE DIAMETER		8	3 in
URFAC	Œ		20.0 ft	TOTAL DEPTH		300 ft bgs	FINISH DATE	4/27/14	CORE			3 in
LLVAI	ION			DEITII				thologic Log	OIZL			
epth ogs eet) 0	GAMMA (GAPI)	CLID (mmho/				Color c	n size distribution p SP) reference Unif	percentages are approximate. M fied Soil Classification visual met 2) reference Munsell Soil Color C	aterial code hod. charts.	Depth bgs (feet)	Samp Type	
	1	/			NO SAMPL NO SAMPL	E: asphalt. E: gravel road l	base.			-/		
					SAND (SP):	: dark grayish b	rown (2.5Y 4/2)), 100% fine grained sand, s reldspar and amphibole.	ubangular to			
5			_		subrounded	; well sorted; co	ontains quartz, f	(3), 100% fine grained sand, feldspar and amphibole.	· ·	_ 5		
								Y 3/2), 100% fine grained sa ieldspar and amphibole.	nd, subangular to			
<u></u>										10		
					:							
5			_		SAND (SP):	: light olive brow	vn (2.5Y 5/3), 1	00% fine grained sand, suba	angular to	15		
								eldspar and amphibole.				
)										_20		
											<u> </u>	SIEV
										25		
5										25		
						to subrounded;		dark gray (5Y 4/1), 80% fin orted; contains quartz, feldsp				
0		,	/ -		sorted; cont	ains quartz, fel	dspar and amph			30		
					SAND (SP): subrounded	dark greenish , trace medium	gray (10Y 4/1), grained; well so	100% fine grained sand, sub orted; contains quartz, feldsp	pangular to par and amphibole.			
					abundance	of horizontal bl	ack/ashy deposi	100% clay, medium plasticity its between 34.5 - 36.4 ft bgs				
5			_		wnite flakes	(shells?); bluis	in coloration.			35		
)											
		\										
)					SILT (ML): o horizontal b present.	dark greenish g lack/ashy lamir	ray (10Y 4/1), 1 nations; trace wh	00% silt; no to low plasticity; nite ashy deposits from 39.5	clayey interbeds with -40.0 ft bgs; mica	40		SS
5_		\			horizontal b	lack/ashy depo	nish gray (10Y 3 sits; 5% fine gra tz, feldspar and	3/1), 95% clay, medium plasi ained sand, subangular to su amphibole.	ticity, soft, trace brounded,	45		
							461					
0	ence Support S							95% fine grained sand, suba ay, clayey interbeds at 52.8 -		50		

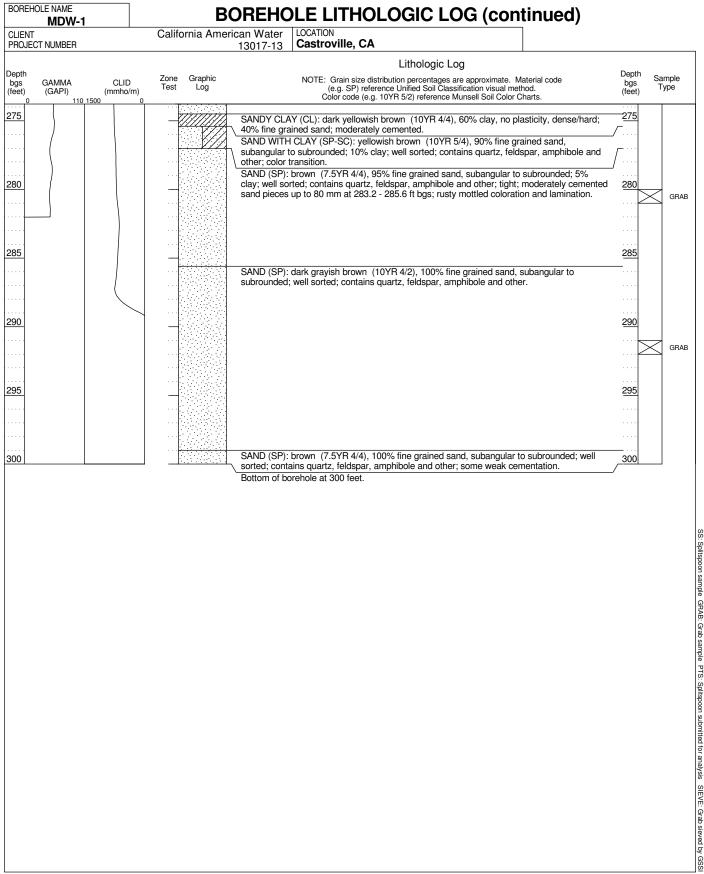
	OLE NAME MDW-1		0 "			OLE LITHOLOGIC LOG (continued)			
PROJEC	CT NUMBER		Calif	ornia Amei	rican Water 13017-13	LOCATION Castroville, CA			
						Lithologic Log			
epth ogs eet)	GAMMA (GAPI)	CLID (mmho/m)	Zone Test	Graphic Log		NOTE: Grain size distribution percentages are approximate. Material code (e.g. SP) reference Unified Soil Classification visual method. Color code (e.g. 10YR 5/2) reference Munsell Soil Color Charts.	Depti bgs (feet	Sa	mple ype
					- 54.8 ft bgs	; well sorted; contains quartz, feldspar and amphibole.			
								$\stackrel{\sim}{-}$	GRAE
)								
5_			_		SAND (SP):	pale olive (5Y 6/3), 100% fine to medium grained sand, subangular to	55		
					subrounded	, predominantly fine grained; medium sorted; contains quartz, feldspar, mica, and other; trace gray mottling.			
)				ampiniono	and other, trade gray metang.			
									SIEV
-			Zone				_60	\bigcap	SIEV
			#4						
					CAND (CD)	light collection because (0.5V.C/A), 1000/ fine to copyright and conditional conditions			
5	{		SC:		to rounded;	light yellowish brown (2.5Y 6/4), 100% fine to coarse grained sand, subrounded trace fine to coarse gravel up to 50 mm, subrounded to rounded; poorly sorted;	_65		
			32,970 uS/cm		contains qua at 64.8 - 65.	artz, feldspar, mica, amphibole and other; trace shell fragments; orange interbed 5 ft bgs.			
)				SAND (SP):	dark gray (5Y 4/1), 100% fine to medium grained sand, subrounded to			
	(rounded, tai	n mottling; trace fine gravel up to 12 mm, rounded; poorly sorted; contains spar, mica, amphibole and other; trace shell fragments.	<i></i>	Δ	SS
)				SAND (SP):	light yellowish brown (2.5Y 6/4), 100% fine to coarse grained sand,			
						tly medium grained, subrounded to rounded; trace fine gravel up to 17 mm, orly sorted; contains quartz, feldspar, mica, amphibole and other; contains shells		\sim	SIEV
					and shell fra	agments. very dark greenish gray (5GY 3/1), 95% silt; 5% sand, very fine grained,			
)				∖ subangular	to subrounded; trace clay; contains quartz, feldspar and mica; trace shell	<i></i>		
<u>-</u>			-		SILTY SANI	nd black/ashy point deposits. D (SM): very dark greenish gray (5GY 3/1), 85% fine grained sand, subangular	<u>75</u> _		
-	}				to subround shell fragme	led; 15% silt; well sorted; contains quartz and feldspar; abundance of shells and ents.	/		
	1			<i>,,,,,</i>	SILT (ML): v	very dark greenish gray (5GY 3/1), 90% silt; 10% fine grained sand, subangular led; trace clay, no to low plasticity; trace shell fragments.			
					TAT CLAY	(CH): very dark greenish gray (5GY 3/1), 100% clay, high plasticity, soft; trace	 		
1	(lack/ashy laminations. T (ML): dark greenish gray (5GY 4/1), 70% silt; 30% sand, very fine grained,			
)					to subrounded; contains quartz and mica; trace thin clay layers; trace horizontal deposits; trace shell fragments.			
.	/				SILTY SANI	D (SM): dark greenish gray (10Y 4/1), 85% sand, very fine to fine grained,	J		
	/				ft bgs and 8	to subrounded; 15% silt; trace clay, trace clay layers, clayey beds at 82.8 - 83.3 9.5 - 90.2 ft bgs; well sorted; contains quartz, feldspar and mica; trace horizontal	85		
					black/ashy o	deposits; higher mica content; trace shell fragments.			
	}								
4	(CLAV (OL)	dayl, granaigh gray (FOV A/4) 4000/ alay granafilms 1 12 2 1 2	90		
-	\				horizontal b	dark greenish gray (5GY 4/1), 100% clay, medium plasticity; trace silt; lack/ashy laminations; trace shell fragments and possible organic matter.			
						dark greenish gray (10Y 4/1), 100% silt; trace sand, very fine grained, to subrounded; trace clay; contains mica; trace horizontal black/ashy			
	\	\			laminations.				
-	(\	-			dark greenish gray (5GY 4/1), 100% clay, medium to high plasticity; trace silt; ntal and point black/ashy deposits; trace organic matter.	<u>95</u>		
)	\				and the control of th			
.		\							
.	}						100		
						dark greenish gray (5GY 4/1), 100% silt; trace sand, very fine grained, to subrounded; trace mica.	<u>100</u>		
	(CLAY (CL):	dark greenish gray (10Y 4/1), 100% clay, medium plasticity, dense; trace silt, 1 -			
	}					ds between 102 - 103.7 ft bgs; trace shell fragments below 106.0 ft bgs; trace point deposits.			
5	(105		
\perp	ence Support S			<u>/////////////////////////////////////</u>					

IENT	MDW-1		Califo		OREHOLE LITHOLOGIC LOG (continued) ican Water LOCATION		
	T NUMBER		Came	Jilla Alliei	13017-13 Castroville, CA		
					Lithologic Log		
oth JS	GAMMA	CLID	Zone	Graphic	NOTE: Grain size distribution percentages are approximate. Material code	Depth bgs	Sample
et)	(GAPI)	(mmho/m)	Test	Log	(e.g. SP) reference Unified Soil Člassification visual method. Color code (e.g. 10YR 5/2) reference Munsell Soil Color Charts.	(feet)	Type
7	110	1500 0		///////	Solor sode (v.g. 1911) of E/10101010 Wallboll Solid Solid States.		
4	}			///////	SAND (SP): greenish gray (10Y 5/1), 100% sand, very fine grained, subangular to		
	/				subrounded; trace silt; well sorted; contains quartz, feldspar and mica.		
5						110	
))					
.	\						
5)		4			115	
.	(\					
.	\	1			OAND (OD)		
.	\				SAND (SP): greenish gray (5GY 5/1), 100% fine to coarse grained sand, predominantly medium grained, subrounded to rounded; trace fine to coarse gravel up to 32 mm, rounded;		
5	/				poorly sorted; contains quartz, feldspar, mica, amphibole and other; includes siltstone and	_120	
			_		chert. SILT (ML): dark greenish gray (5GY 4/1), 100% silt; trace fine grained sand; trace clay, 1 in.	/ ==	
	\				clay interbeds; contains mica; thin horizontal black/ashy laminations in clays.		
	\						
					FAT CLAY (CH): dark greenish gray (5GY 4/1), 100% clay, high plasticity, dense; very dense from 124.3 - 127.0 ft bgs; thin rusty and black/ashy horizontal lamination from 126.0 -		
5)		_		127.0 ft bgs.	125	
	\						× •
.	}				SILT (ML): dark greenish gray (10Y 4/1), 100% silt; trace thin clayey interbeds; thin		
					horizontal black/ashy lamination.	<u></u>	
5	(FAT CLAY (CH): dark greenish gray (10Y 4/1), 100% clay, medium to high plasticity, soft clay from 128.3 - 129.6 ft bgs, dense clay from 129.6 - 135.2 ft bgs; trace silt, dark brown	130	
	1	\			silty deposit from 132.2 - 133.4 ft bgs within clay; trace horizontal laminations and point		
		\			black/ashy deposits.		
.	\						
.	/ /						
5	/		_		OHT (MI) 1 1 (40V 4(4) 050(1) 50(1 1 5)	<u>135</u>	
.	\				SILT (ML): dark greenish gray (10Y 4/1), 95% silt; 5% sand, very fine grained, subangular to subrounded; trace clay; contains mica; trace thin horizontal black/ashy laminations.		
1					SAND (SP): greenish gray (5GY 5/1), 95% fine to medium grained sand, subangular to		
	/				subrounded, trace rounded coarse grained; 5% fine to coarse gravel up to 25 mm, rounded; medium sorted; contains guartz, feldspar, mica, amphibole and other; many mineral types.		
)	\				medium sorted, contains qualtz, leidspar, mica, ampribble and other, many mineral types.	140	GF
)						
	(
		1 1					
)					4.45	
5	(4		SAND (SP): greenish gray (10Y 5/1), 100% fine to medium grained sand, subangular to	— <u>145</u>	
	\				rounded; trace fine to coarse gravel up to 35 mm, rounded; medium sorted; contains quartz, feldspar, mica, amphibole and other; trace rounded cobbles up to 75 mm at 145.2 ft bgs;		
			-		\ includes chert and siltstone; many mineral types.	/-···	abla s
) [].		SAND (SP): dark greenish gray (10Y 4/1), 100% fine to medium grained sand, subrounded to rounded; trace fine gravel up to 17 mm, rounded; well sorted; contains quartz, feldspar,		
<u>)</u>	/		4	1777	mica, amphibole and other; trace clay balls; includes siltstone.	_150	GF
.					SAND WITH CLAY (SP-SC): dark greenish gray (5GY 4/1), 85% fine to medium grained sand, subangular to rounded, trace coarse grained; 10% clay; 5% fine to coarse gravel up to		
.)	<i> </i>	Zone	, U [*] /()	\ 65 mm, rounded; contains quartz, feldspar, mica, amphibole and other; many mineral types;	<i></i>	
.			#3	· / ·	\ included siltstone. SAND WITH GRAVEL (SP): light olive gray (5Y 6/2), 60% fine to coarse grained sand,	/ ···· ₌	SIE
5				,	subangular to rounded; 40% fine to coarse gravel up to 70 mm, rounded; poorly sorted;	155	$\stackrel{\circ}{\rightarrow}$
1	\		H	0 0	contains quartz, feldspar, mica, amphibole and other; gravel with sand from 152.6 - 153.5 ft bgs.		
])		SC: 38,100	$\circ \circ$		_:::	
			uS/cm		SAND (SP): olive gray (5Y 5/2), 100% fine grained sand, subangular to subrounded; trace fine to coarse gravel up to 21 mm, subrounded to rounded; well sorted; contains quartz,		
.	\				feldspar, amphibole and other; silt at 156.7 - 157 ft bgs.		
2]		H			160	
	/	1 1					



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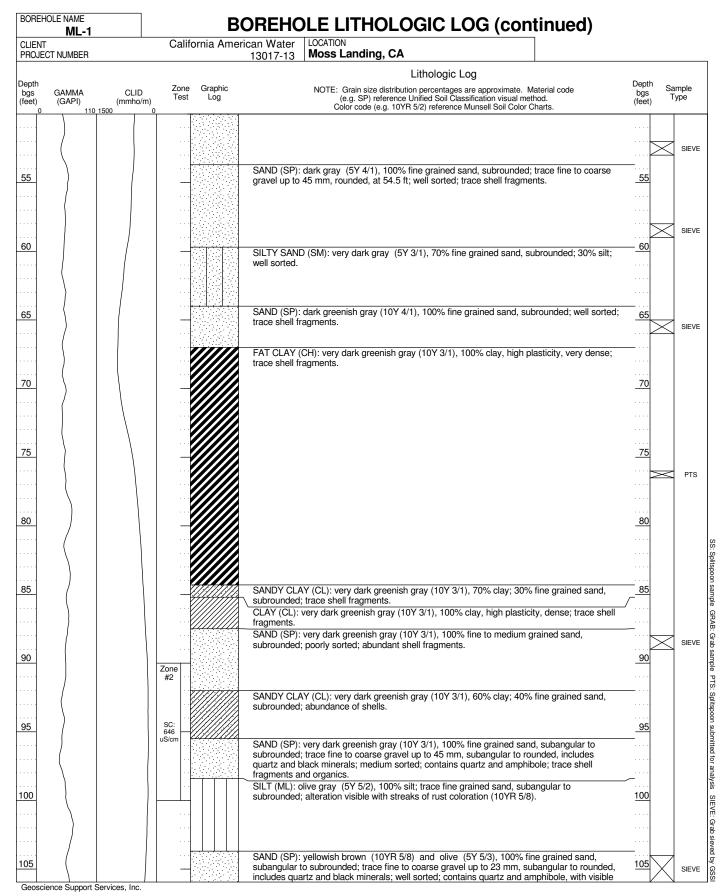




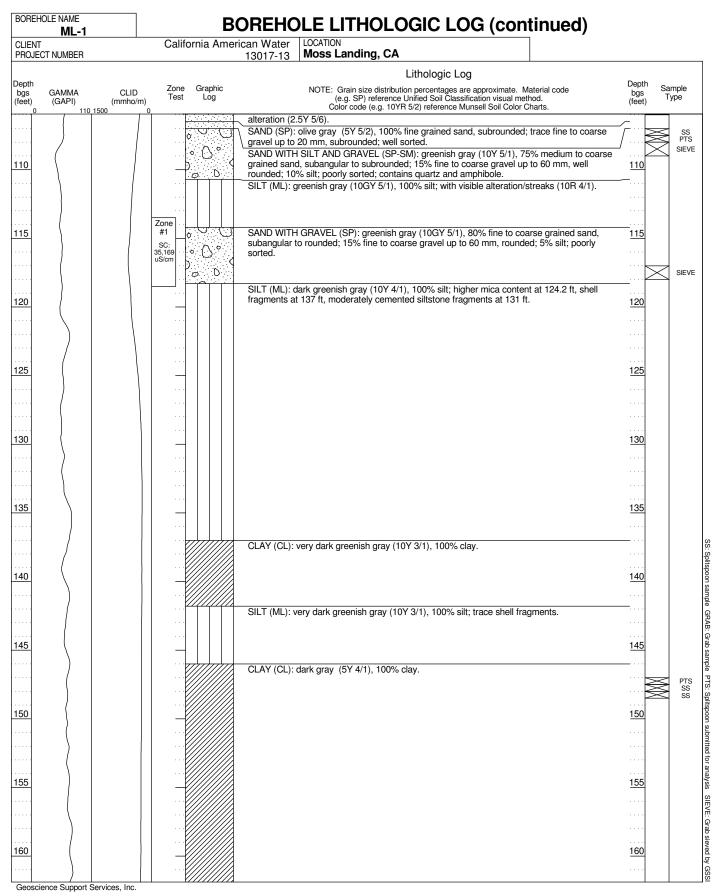


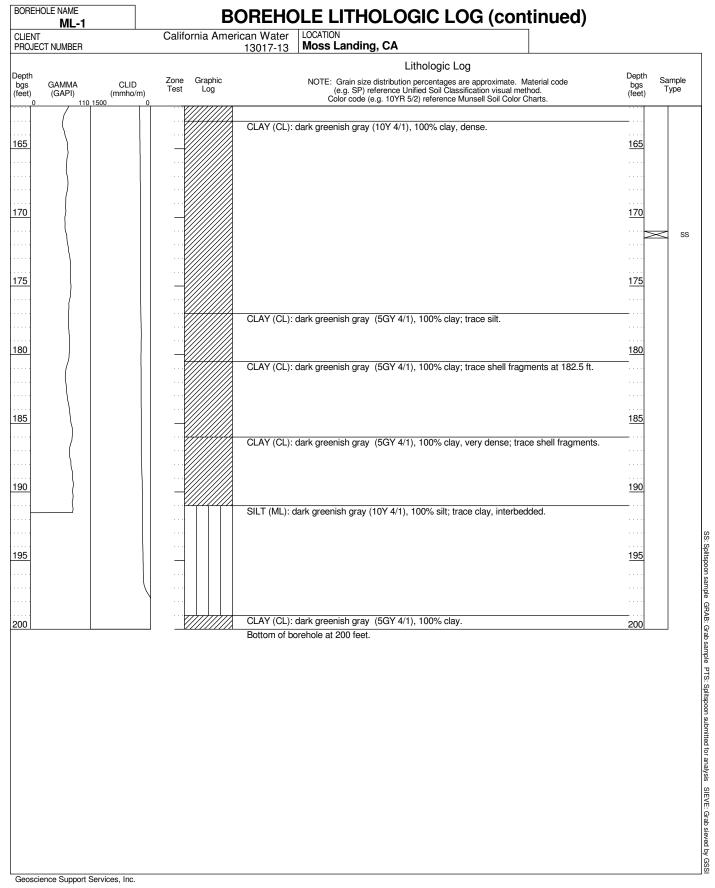
BOREHOLE NAME ML-1				ВС	REHO	LE LITHO	LOGIC LOG	à		
CLIENT PROJECT NUMBER	I	Calif	ornia Ame	rican Water 13017-13	LOCATION Moss Lan	dina. CA				
REPORT DATE				7/8/2014	Sandhold	· ·	Geographic NAD83			
DRILLING CONTRACTO)R			ade Drilling	LOGGED BY	•	Geograpino NADOC			
DRILLING	Prosonic 6	OOT	DRILLING	se Munguia	N. Reyno Sonic	START	10/02/13	BOREHOLE		8 in
RIG TYPE SURFACE			METHOD TOTAL			DATE FINISH		DIAMETER CORE		
ELEVATION	8.	.0 ft	DEPTH		200 ft bgs	DATE	10/07/13	SIZE		6 in
Depth bgs GAMMA (feet) (GAPI)	CLID (mmho/m) 500 0	Zone Test	Graphic Log		(e.g. :	n size distribution percer SP) reference Unified So	ogic Log ntages are approximate. M oil Classification visual metl erence Munsell Soil Color C	nod.	Depth bgs (feet)	Sample Type
				medium to o		trace fine to coarse	fine grained sand, subr gravel up to 35 mm, sub			
				SILT (IVIL).	uaik gray (51 4	+/ 1), 100 % Siit.				
5									5	
/										
)										
10				CLAV (CL)	dork grov (EV	4/1) 1009/ alay bial	a placticity; with visible o	altoration	10	
						(5Y 3/1), 100% clay, high	n plasticity; with visible a with shells.	alteration.		
15		_							15	
				SAND (SP)	· light vellowish	brown (2.5Y 6/4) 1	00% medium to coarse	grained sand		
				subangular	to rounded; tra- up to 120 mm.	ce fine to coarse grav	vel up to 30 mm, rounde	ed; poorly sorted;		
20				CLAY WITH	I SAND (CL): v	ery dark gray (5Y 3/	1), 85% clay; 10% fine t e gravel up to 25 mm, ro	o coarse grained	20	
				\ fragments.			60% silt; 40% fine graine		<i></i>	
						.6 and 34.0 ft, trace		od odira, odbarigalar		
25									25	
····· \										
30									30	
35				CLAY (CL):	very dark gray	(5Y 3/1), 100% clay	, medium plasticity.		35	
			//////////////////////////////////////	SAND (SP):	dark gray (5Y	4/1), 100% fine to m	nedium grained sand, su	bangular; poorly		
	\				very dark gray	(2.5Y 3/1), 100% cla	ay, high plasticity; trace	shell fragments.	⁷	
40	\	-							40	
	\		(///////			rk gray (2.5Y 3/1), 7	70% silt; 30% fine graine	ed sand, subrounded;		
	\			abundant si	nell fragments.					
45				SAND (SP)	: dark gray (5Y	4/1), 100% fine to m	nedium grained sand, su	ıbangular, trace	45	
						o coarse gravel up to s and shell fragments	o 25 mm, subrounded to s.	rounded; poorly		
)										
Geoscience Support Se	ervices, Inc.		<u> 14 (5 4 5 4 4 4 5 5 4 4</u>						50	

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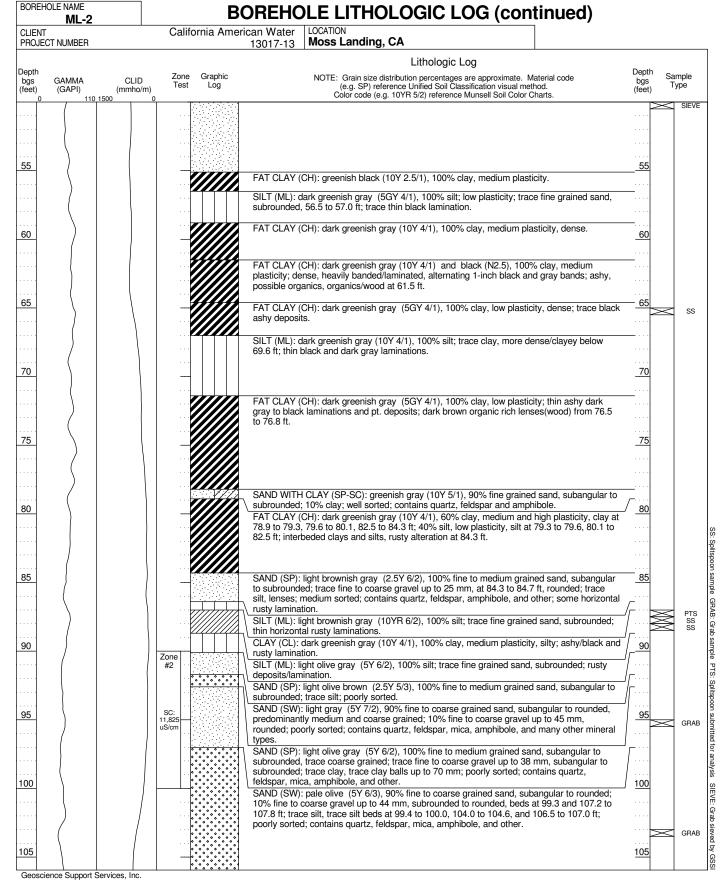
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BOREHOLE NAME ML-2			ВС	REHO	LE LITHOL	OGIC LO	G		
CLIENT PROJECT NUMBER	Cali	fornia Amer	rican Water 13017-13	Moss Lan	•				
REPORT DATE			7/8/2014		Sneries 3", -121°47' 12.4368"	Geographic NAD83			
DRILLING CONTRACTOR DRILLER		Jos	ade Drilling se Munguia	N. Reynol					
DRILLING RIG TYPE Pro	sonic 600T	DRILLING METHOD		Sonic	START DATE	12/09/13	BOREHOLE DIAMETER		8 in
SURFACE ELEVATION	7.0 ft	TOTAL DEPTH		200 ft bgs	FINISH DATE	12/19/13	CORE SIZE		6 in
	CLID Zono mho/m) Tes		CANDY CIL	Color co	ode (e.g. 10YR 5/2) refer	ages are approximate. M il Classification visual met ence Munsell Soil Color C	harts.	Depth bgs (feet)	Sample Type
5			subangular; and other; a SAND (SP): subangular to quartz and fine subangular to subangular subrounded SAND (SP): fine to media coarse graw amphibole, a SAND (SW) subrounded poorly sorter and fine grams and subrounded; trace silt; me fragments. SAND (SP): trace silt; me fragments. SAND (SP): counded; trace silt; me fragments. SAND (SP): counded; trace silt; me fragments. SAND (SP): subrounded quartz, felds SAND (SW) subrounded quartz, felds clay with an SILT (ML): of fragments. SANDY SIL subrounded alternating filaminations FAT CLAY (CL): cay with an subrounded alternating filaminations subrounded alternating filaminations subrounded sand silts apparained sand silts app	T (ML): olive gr 10% fine to co. sphalt present. light yellowish to subrounded, eldspar. T (ML): very da to subrounded; contains quart very dark gray um grained sanel up to 41 mm and other. I light yellowish to rounded; trad; contains quavel layer with si olive gray (5Y edium sorted; contains qua vel layer with si olive gray (5Y edium sorted; contains mica: light yellowish to rounded; trace organics/wery dark green; contains mica: light yellowish to rounded; traspar, amphibole dark greenish gabundance of dark greenish gray d, subangular trace fine gravine sand and si (organics/wood CH): dark gree	ay (5Y 4/2), 65% silt; arse gravel up to 26 n brown (2.5Y 6/4), 100 predominantly fine gravel in trace fine to coarse gravel up to 26 n trace fine to coarse gravel in the coarse	25% fine to medium on subangular; contains, subangular; contains, subangular; contains, subangular; contains, subangular; contains, subangular; contains, subangular, contains, subangular, contains, subangular, and other; well round other; well ro	grained sand, ins quartz, feldspar, wined sand, arm sorted; contains of fine grained sand, bangular to to 90 mm. Wen (2.5Y 4/2), 100% ined; trace fine to ns quartz, feldspar, winded to rounded; nuded coarse sand with a sand, bunded to rounded; nuded coarse sand with a sand, winded to rounded; nuded coarse sand with a sand, with a sand, sorted; contains with a sand, eldspar, and other; thin black/dark brown city; trace shells.		SIEVE

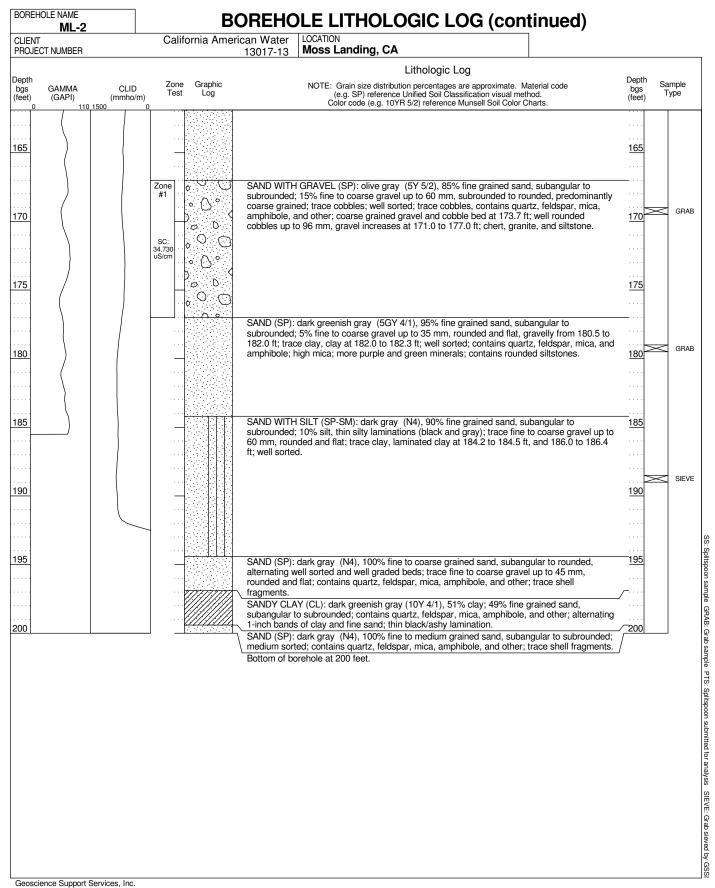


BOREHOLE NAME

RORFHOLF LITHOLOGIC LOG (continued)

JENT	CT NUMBER	California American Water 13017-13 LOCATION Moss Landing, CA							
TUJE	UT NUIVIDEN								
pth		Zone Graphic	Lithologic Log	Depth	Cor	mple			
gs eet)	GAMMA CLIE (GAPI) (mmho	Toct Loa	NOTE: Grain size distribution percentages are approximate. Material code (e.g. SP) reference Unified Soil Classification visual method. Color code (e.g. 10YR 5/2) reference Munsell Soil Color Charts.	bgs (feet)		/pe			
7	110 1500	0	Color code (e.g. 10111 3/2) reference wurisen con color charts.						
)								
			SAND (SP): olive gray (5Y 5/2), 100% fine grained sand, subangular to subrounded; trace	-					
0			fine to coarse gravel up to 26 mm, rounded; trace clay; well sorted; clayey gravel layer at	110					
			108.7 ft. SAND WITH GRAVEL (SW): pale olive (5Y 6/4), 85% fine to coarse grained sand,	<u> </u>	\leq	SIEVE			
			subangular to rounded, altered sand to dark brown at 115.3 to 115.7 ft; 15% fine to coarse						
)		gravel up to 71 mm, rounded; trace cobbles; trace clay; poorly sorted; contains quartz, feldspar, mica, amphibole, and other; cobbles to 80 mm at 111.0 ft.						
5	/			115					
			SAND (SP): olive gray (5Y 5/2), 100% fine grained sand, subangular to subrounded, very	_:::L					
			fine grained; trace fine to coarse gravel up to 31 mm, well rounded; well sorted; contains quartz, feldspar, mica, amphibole, and other.	/	\approx	SS PTS SS			
)		SAND WITH SILT (SP-SM); olive gray (5Y 5/2), 90% fine to medium grained sand.	·	$\widehat{}$	SS			
2	/		subangular to subrounded; 10% silt; trace fine gravel up to 5 mm, subangular to subrounded; poorly sorted; contains quartz, feldspar, amphibole, and other.	<u> 120</u>					
	\		SILT (ML): olive gray (5Y 5/2), 100% silt; trace fine to coarse gravel up to 51 mm, well						
	\		rounded; trace fine to coarse grained sand, subangular to subrounded; trace clay; gravel and silt bed at 121.3 to 122.2 ft; clays at 123.4 to 123.8, 130.2 to 130.5, and 131.4 to 131.6						
)		ft; altered rusty sand at 125.5 to 126.2 ft.						
1				125	\sim	GRA			
				130					
)			100					
)		SAND (SW): olive gray (5Y 5/2), 90% fine to coarse grained sand, subangular to rounded,						
	(predominantly fine grains; 10% fine to coarse gravel up to 42 mm, rounded; poorly sorted; contains quartz, feldspar, mica, amphibole, and other.	[
5			SAND (SP): olive gray (5Y 5/2), 95% fine grained sand, subangular to subrounded; 5% fine	135					
.			to coarse gravel up to 40 mm, rounded; trace clay, trace clay layer at 136.2 to 136.5 ft; well sorted; contains quartz, feldspar, mica, amphibole, and other; thin rusty laminations,						
			transition from olive brown to gray at 138.6 ft.						
			SAND WITH SILT AND GRAVEL (SP-SM): greenish gray (5GY 5/1), 70% fine grained						
)			sand, subangular to subrounded, trace medium and coarse grains; 20% fine to coarse	_140					
			gravel up to 45 mm, rounded; 10% silt; trace clay; well sorted; contains quartz, feldspar, mica, amphibole, and other; clay and gravel at 139.3 to 139.8 ft.	/					
-			SAND (SP): greenish gray (5GY 5/1), 100% fine grained sand, subangular to subrounded;	<u></u>					
-			trace clay; well sorted; contains quartz, feldspar, and other; clay at 140.1 to 140.4 ft.	/					
5)		CLAY (CL): dark gray (N4), 60% clay, low plasticity; 40% silt; trace fine grained sand, subrounded; alternating silt and clay beds with black and dark gray horizontal laminations;	145					
1	/		contains organics/wood; trace thin fine sand beds.						
		2000	SAND (SP): pale olive (5Y 6/3), 100% fine grained sand, subangular to subrounded; trace						
	\		fine gravel up to 18 mm, subangular to rounded; trace clay, trace clay lens at 146.1 ft; well sorted.	/ _		GRA			
			SAND WITH GRAVEL (SW): light olive gray (5Y 6/2), 70% fine to coarse grained sand,			SIIA			
)	/		subangular to rounded; 25% fine to coarse gravel up to 37 mm, rounded; 5% silt; poorly sorted; contains quartz, feldspar, mica, amphibole, and other.	150					
	(SAND (SP): olive gray (5Y 5/2), 95% fine grained sand, subangular to subrounded; 5% silt; trace fine to coarse gravel up to 19 mm, rounded; well sorted; contains guartz, feldspar.						
) /		trace fine to coarse gravel up to 19 mm, rounded; well sorted; contains quartz, feldspar, mica, amphibole, and other.	F	\times	SIEV			
		7777777							
5)		CLAY (CL): olive gray (5Y 5/2), 70% clay; 30% silt; dense silty clay; no plasticity; olive brown with gray lamination, trace rusty deposits.	_155					
-	/		SAND (SP): olive (5Y 5/3), 90% fine grained sand, subangular to subrounded; 10% fine to						
	/ /		coarse gravel up to 68 mm, subrounded to rounded; trace clay; well sorted; contains quartz, feldspar, mica, amphibole, and other; higher mica; contains chert, many mineral types,		\leq	SS			
-			gravel from 157.0-158.5 ft; clay from 162.2 to 163.1 and 164.2 to 164.6 ft.		\approx	SS PTS SS			
0	/ \			160		GRAI			
						GI IAI			
1.1	1 1	 1 10 10 10 2 4 3 2 3 3 			- 1				

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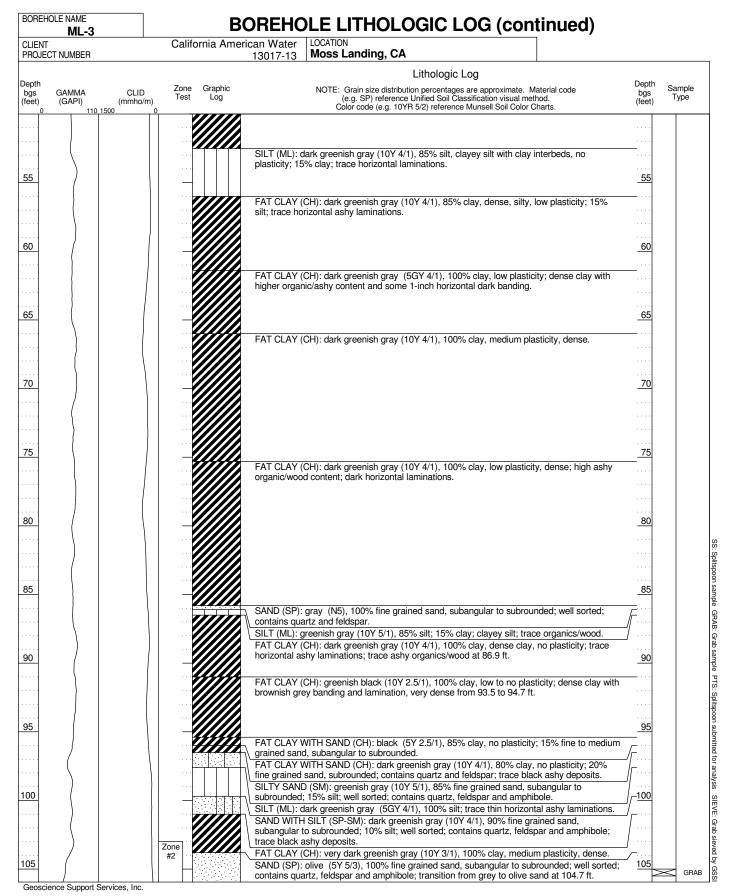


A1-40

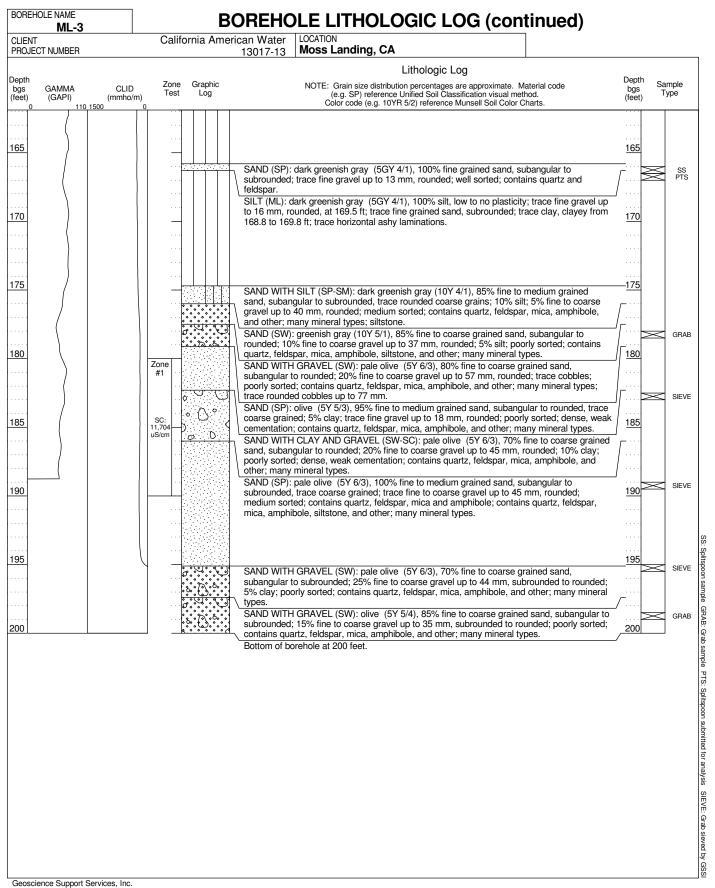


BOREHOLE NAME ML-3			BOI	REHO	LE LITHO	LOGIC LOG	à		
CLIENT PROJECT NUMBER	C	alifornia American	Water	LOCATION Moss Land	ding. CA				
REPORT DATE			2/2014	Nadar Agh	na Property 3", -121° 47' 00.7656"	Coorrentie NADCO			
DRILLING CONTRACTO	R	Cascade D	Orilling	LOGGED BY	-	Geographic NAD83			
DRILLER DRILLING		Jose Mu	unguia	N. Reynol	ds START		BOREHOLE		
RIG TYPE SURFACE	Prosonic 600T	TOTAL		Sonic	DATE	1/07/14	DIAMETER		8 in
ELEVATION	16.0 ft	t DEPTH	2	200 ft bgs	DATE	1/13/13	SIZE		6 in
Depth bgs GAMMA (feet) (GAPI)	(mmho/m)	one Graphic Test Log		(e.g. S	size distribution perce SP) reference Unified S	ogic Log ntages are approximate. M oil Classification visual metl erence Munsell Soil Color C	nod.	Depth bgs (feet)	Sample Type
10 	500 0	to s feld SAI SAI to s poo SAI to s poo SAI to s trac feld SAI sub con san	subrounded spar, mica ND (SP): lig dominantly drounded; for the subrounded orly sorted; ND (SP): lig subrounded orly sorted; ND (SP): lig subrounded orly sorted; ND (SP): lig subrounded at 18.9 ft ND (SP): lig soarse grain nd at 18.9 ft ND (SW): lig soarse grain nded; interlizontal ash ND (SW): lig soarse grain nded; 5% for a, amphibo	ML): light olivit race fine to and amphibo ght yellowish fine, subang trace silt; mer ght yellowish trace fine gontains quality trace fine gontains quality trace fine gontains quality to solive. The substitution of the substitution of the yellowish subrounded; and yel	brown (2.5Y 5/3), o coarse gravel up to le. brown (2.5Y 6/4), 1 ular to subrounded; dium sorted; contain brown (2.5Y 6/3), ravel up to 15 mm, srtz, feldspar, mica a gray (2.5Y 6/2), 95°ch alternating dry promise of the coarse gravel inca and amphibole; orown (2.5Y 6/3), 95°ch diagraphica and amphibole; orown (2.5Y 6/3), 95°ch alternating dry promise and amphibole; orown (2.5Y 6/3), 95°ch alternating dry promise and amphibole; orown (2.5Y 6/3), 95°ch alternating dry promise and amphibole; orown (2.5Y 6/3), 95°ch and amphibole; orown (2.5Y 6/2), 95% fine to 18 mm, rounded, higher mica conterior and	, 70% silt; 30% fine grai 22 mm, subangular; co 22 mm, subangular; co 00% fine to medium grai trace fine to coarse grai subrounded; trace silt, so amphibole. If the fine to medium graine subrounded; trace silt, so amphibole. If the fine to medium graine subrounded; trace silt, so of the fine to medium graine subrounded; medium sorted; co 00% fine to medium graup to 60 mm, rounded; higher mica content; rus fine to coarse grainca and amphibole; high to coarse grained sand poorly sorted; contains it.	ned sand, subangular ntains quartz, ined sand, rel up to 25 mm, flat and amphibole. ned sand, subangular ome silty sand beds; d sand, subangular m 10.3 to 11.1 ft; ontains quartz, ined sand, medium sorted; st colored altered ity, silty clay; 5% fine avel up to 30 mm, n mica content, some subangular to quartz, feldspar,		GRAE
25 	ervices Inc.	coa mic CL/ blac FAT fine with	arse gravel ca, amphibo AY (CL): pa ck and rust T CLAY (Ch grained sa	up to 39 mm, ble, and other ale olive (5Y colored lamin H): dark gree and, subangu	subrounded to rour, high mica content. 6/3), 85% clay, no phations. nish gray (10Y 4/1), lar to subrounded, s	and, subangular to subra ided; well sorted; contain lasticity; 15% silt, thin si 100% clay, medium pla and layer from 32.0 to 3 organics (wood) at 32.7	ns quartz, feldspar, Ity interbeds; thin sticity, dense; trace 2.3 ft; dense clay		

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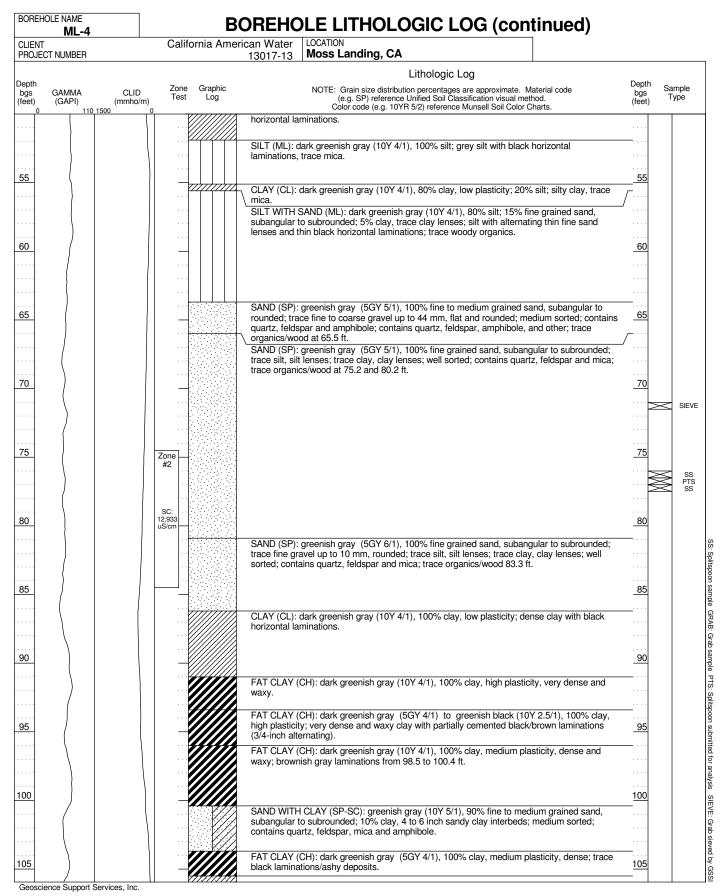
BOREHOLE	E NAME ML-3				В	OREH	OL	E LIT	HOL	ogic i	LOG	(con	tinued)				
CLIENT PROJECT N			Calif	fornia		rican Water 13017-13	r LO	OCATION	ding, CA								
						10017 10	<u> </u>		<u> </u>	Lithologic	c Log						
	AMMA (GAPI)	CLID (mmho/m)	Zone Test				Ν	NOTE: Grai (e.g. Color o	n size distribu SP) reference ode (e.g. 10Y	tion percentage Unified Soil C ('R 5/2) referen	es are appro Classification ce Munsell S	oximate. Ma visual meth Soil Color C	aterial code nod. harts.		Depth bgs (feet)		mple /pe
] /	/		80:										subrounded; tra nses; well sorted			\lessapprox	SS PTS SS
(\		SC: 7,439 uS/cm			contains qu lamination/a			amphibole, a	and other; tra	ace rust an	d purple c	olored				
10			-												110	\times	SIEVE
				*****	****	subrounded	ed, fini	ning upward	; trace fine t		avel up to 2		pangular to brounded; poorly	·	2	~	SIEVE
15						SILT (ML):): dark	k greenish g	ray (5GY 4	hibole, and o	lt; trace cla	ay; trace th	in ashy laminatio	ons;	115		
						and 124.6 t			to 117.0, 1	17.8 to 118.2	2, and 119.	.6 π; сіауе	y from 122.7 to	123.3	113		
20	/		_												120		
25															125		
						SILT (ML): lamination/o				1), 85% silt,	dense; 15%	% clay; tra	ce thin black ash	ny			
							" аоро	المارين والماري									
 80															130		
)																
	}																
35															135		
10						thin horizon	ontal á	áshy lamina	tions. (,,	•		r; 15% silt; silty; ce thin horizonta		140		
						ashy lamina	nations	ns; trace sh	ell fragment	5/1), 100% SI S.	it, contains	inica; trac	e min nonzonta				
15															145		
						SILT (ML):): dark	k greenish ç	ray (5GY 4	/1), 85% silt,	, clayey; 15	5% clay; tr	ace round grave	el to			
50						21mm at 15	157.61	ft; trace thi	n horizontal	ashy lamina	itions/depo	sits.			150		
)																
	/																
55	\														155		
				$ \ \ $													
						EAT OLAY	V (CLI)	1\. dark ====	nich aras /	5GY 4/1), 10	100/ alan !	ow plastic	ty: trace silt:				
60	/		_			\ horizontal a	l ashy l	black lamir	nation.	,,	•	•	•	/	160		
				$ \ \ $		SILT (ML): laminations): dark ns; org	k greenish g ganics/wood	gray (5GY 4 d at 163.5 ft	√1), 100% si	it; trace cla	ay; trace th	in horizontal ash	ny			





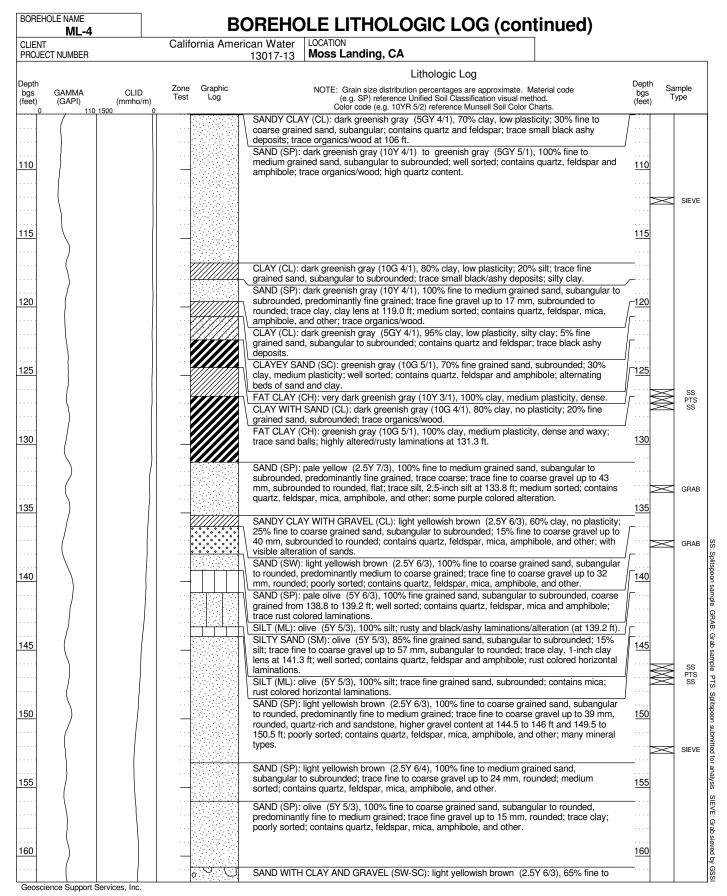
BOREHOLE NAME ML-4				ВС	REHO	LE LITHO	LOGIC LO	a			
CLIENT PROJECT NUMBER		Cali	fornia Amer	rican Water 13017-13	LOCATION Moss Land	ding, CA					
REPORT DATE				7/8/2014	Nadar Agh	na Property	Geographic NAD83				
DRILLING CONTRACTO	R			ade Drilling se Munguia	LOGGED BY N. Reynol	,	3.,				
DRILLING RIG TYPE	Proso	nic 600T	DRILLING METHOD	se mungula	Sonic	START DATE	12/02/13	BOREHOLE DIAMETER			8 in
SURFACE		32.0 ft	TOTAL		201 ft bgs	FINISH	12/06/13	CORE			7 in
ELEVATION		32.0 II	DEPTH		20111.093	DATE	ogic Log	SIZE			7 111
Depth bgs GAMMA (feet) (GAPI)	CLII (mmho					size distribution perce SP) reference Unified S	ntages are approximate. Moloil Classification visual meterence Munsell Soil Color C		Depth bgs (feet)	San Ty	nple pe
5 5 10 15 20				subrounded; well sorted; SANDY SIL subrounded; feldspar; traid subangular traid quartz and find CLAY (CL): subrounded; CLAY (CL): subrounded; SAND (SP): to subrounded; visible rust of CLAY (CL): subrounded; visible rust of CLAY (CL): subangular traidspar; traidspa	; 20% silt; trace contains quartz T (ML): dark brt; trace fine grave ce organics/roo T (ML): very da to subrounded; eldspar; trace colive (5Y 5/3), contains quart light yellowish be ce fine grained inerals (sphericight yellowish be dispersively yellowish ight yellowish; olive (5Y 5/3), to subrounded; light yellowish ed, predominare, rounded; med, redominare, rounded; med trace weakly ce	fine to coarse grave, feldspar, mica and own (10 YR 3/3), 70 el up to 5 mm, subats. rk brown (10 YR 2/2 trace fine gravel up reganics/roots. 90% clay, low plastiz and feldspar; som orown (2.5 Y 6/4), 90 sand, subangular to al). rown (2.5 Y 6/3), 90 o subrounded, 4-inclon and organics. brown (2.5 Y 6/4), 1 orown (2.5 Y 6/4), 1 orown (2.5 Y 6/4), 1 orown (2.5 Y 6/4), 9 orown (2.5 Y	0% clay, low plasticity, to subrounded; friable, or % silt, clayey silt; 10% for rusty sand interbeds; 00% fine grained sand, quartz, feldspar, mica at an silty interbeds; trace fit and black horizontal lating to medium grainer rusty alteration; 5% sinple; contains quartz, felt interbeds.	ular to subrounded; ics/roots. sand, subangular to contains quartz and ained sand, rounded; contains and, subangular to race cemented clay; ganics (black), ine to medium contains quartz and subangular to amphibole; with me grained sand, minations. ne grained sand, minations. net of medium contains quartz and subangular to amphibole; with me grained sand, minations. net of medium contains quartz and subangular to and amphibole; with me grained sand, minations. net of medium contains quartz and subangular to and subangular to ubangular to ubangular to			
25				subrounded,	, trace coarse o		avel up to 18 mm, suba		<u>25</u>	><	SIEVE
				5% fine to co	oarse gravel up	to 65 mm, subangu	parse grained sand, sub ular to rounded, coarse s , feldspar, mica and am	subrounded gravel at			
35							fine grained sand, suba par and amphibole; high		35		
				τounded, tra	ice coarse grair	ed; trace fine grave	e to medium grained sar I up to 18 mm, rounded nica, amphibole, and otl	; trace clay, trace clay	 		
40	,			SAND (SP):	olive gray (5Y	5/2), 100% fine gra	ined sand, subangular t z, feldspar, mica and ar	o subrounded, trace	40	X	GRAB
				CLAY (CL): horizontal la		5/2), 100% clay, low	v to no plasticity; alterati	on visible, rusty			
45					CH): dark gree sible, dark gray		, 100% clay, medium pl	asticity, dense;	45		GRAB
				subrounded:	; alteration visib	le, rusty horizontal I 5/2), 100% clay, me	5% silt; 15% fine grained aminations; contains mi adium plasticity; trace sil	ca.	<u></u>		
50 Geoscience Support Se							6 clay, medium plasticity	; gray to black	50		

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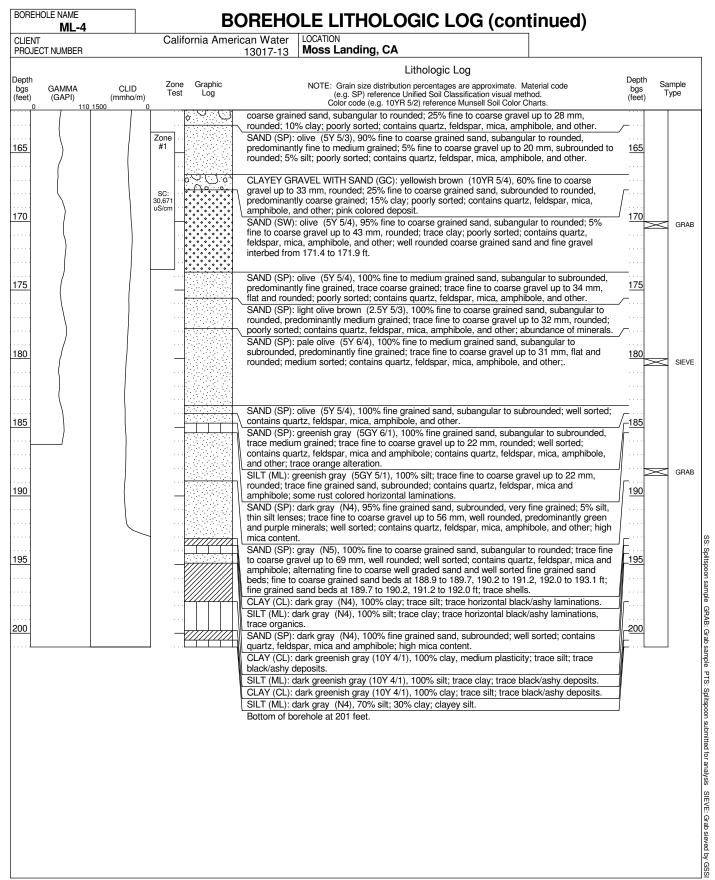
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BOREHOLE NAME ML-6				ВС	REHO	LE LITHOL	OGIC LO	G		
CLIENT PROJECT NUMBER		Cali	fornia Amer	rican Water 13017-13	LOCATION Moss Land	ding, CA				
REPORT DATE				7/8/2014	MBARI 36° 48' 21.4992	?", -121°47' 16.0188"	Geographic NAD83			
DRILLING CONTRACTO	R			ade Drilling se Munguia	LOGGED BY N. Reynol	ds				
DRILLING RIG TYPE	Proso	nic 600T	DRILLING METHOD		Sonic	START DATE	11/18/13	BOREHOLE DIAMETER		8 in
SURFACE ELEVATION		15.0 ft	TOTAL DEPTH		200 ft bgs	FINISH DATE	11/23/13	CORE SIZE		7 in
-	Lithologic Log									
Depth bgs GAMMA (feet) (GAPI) 0 110 15	CLII (mmho						ages are approximate. M I Classification visual met ence Munsell Soil Color C		Depth bgs (feet)	Sample Type
				CLAYEY SA rounded; 15 contains qua						
				rounded; 30	% clay; trace fir	ne to coarse gravel up	medium grained sand to 62 mm, angular to libole; contains shells.	rounded; poorly		
5				Sortou, corne	anio quartz, roic	aspar, mica and ampri	iibole, contains shells.		5	
				SAND (SP):	olive (5V 4/4)	100% fine to medium	grained sand, subang	gular to subrounded:		
10				trace coarse	gravel rounder	d, interbedded; trace s	silt, silt from 8.7 to 9.2 sins quartz, feldspar ar	ft with high mica	10	
		기 ::								
15		_		SAND (SP):	olive gray (5Y	5/2), 100% fine to me	edium grained sand, s	ubangular to	15	
					; medium sorted d sands from 2		dspar, mica and amph	ibole; altered rust and		
20									20	
25		_		5% fine to co	oarse gravel up		se grained sand, suba poorly sorted; contains		25	
				mica, ampin	bole, and other	, trace shells and she	ii ii agiiiciito.			
30		-							_30	
				CLAY (CL): colored alter		5Y 4/4), 100% clay, lo	ow plasticity; with visib	le rust and black		
				organics, alt	ered black and	dark gray and weakly	00% clay, medium pla cemented from 33.7	to 34.2 ft.	<u></u>	
35		-		\ laminations.	, ,		00% clay, low plasticit		<u>35</u>	
				√ very fine gra	ined; contains	mica; thin black lamin	% silt; 5% fine grained ations. (1), 100% clay, mediur			
40					d, subrounded,		2 to 40.4 ft; trace black		40	
				CLAY (CL): at 42.4 to 42		(10Y 2.5/1), 100% cla	ay, medium plasticity; t	trace silt, silt interbed		
45				\ subrounded;	alteration visib	ole with black/grey and			45	
)		\ subrounded;	50% clay; with	visible rust colored a	% fine grained sand, s Iteration; sandy clay to	o clayey sand.		
				subrounded:	trace silt; with	visible rust colored al	y; 5% fine grained sar teration. % fine grained sand, s		[
50 Geoscience Support Se							% fine grained sand, s , feldspar, mica and ai		50	

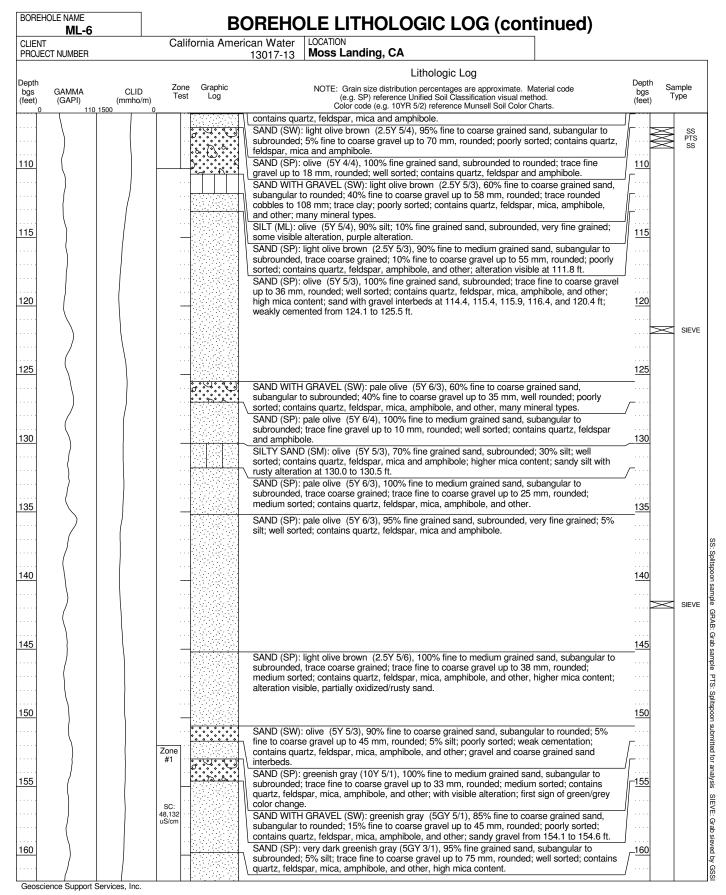
BOREHOLE NAME

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BORFHOLF LITHOLOGIC LOG (continued)

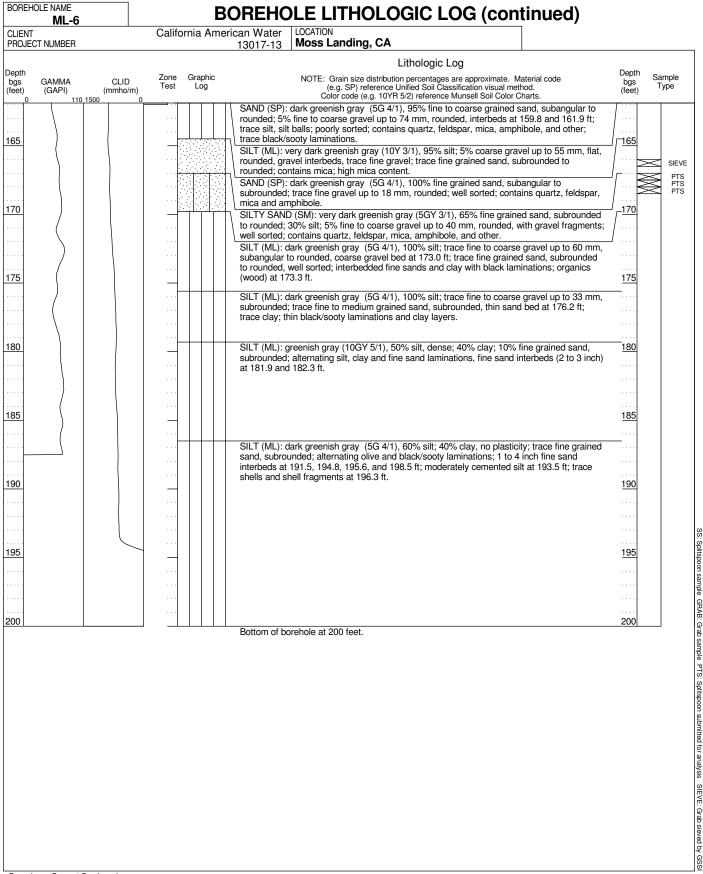
LIENT			California American Water 13017-13 California American Water 13017-13 Moss Landing, CA								
HUJE(CT NUMBER										
epth ogs eet)	GAMMA (GAPI)	CLID (mmho/m)	Zone Test	Graphic Log	Lithologic Log NOTE: Grain size distribution percentages are approximate. Material code (e.g. SP) reference Unified Soil Classification visual method. Color code (e.g. 10YR 5/2) reference Munsell Soil Color Charts.	Depth bgs (feet)	Ja T	mple			
		500 0			visible alteration. SAND (SP): light yellowish brown (2.5Y 6/3), 95% medium to coarse grained sand, subangular to rounded; 5% fine to coarse gravel up to 45 mm, rounded; poorly sorted; contains quartz, feldspar, mica and amphibole; with visible alteration; gravelly sand from 53.7 to 54.9 ft.	<u></u>					
5					CLAY (CL): olive (5Y 5/3), 100% clay; trace silt; silt/fine sand laminations, rusty altered laminations.	<u>55</u>					
					SAND (SP): light yellowish brown (2.5Y 6/3), 95% fine grained sand, subangular to subrounded, very fine grained; 5% silt; trace fine to coarse gravel up to 23 mm, subrounded; trace clay; well sorted; contains quartz, feldspar, mica and amphibole; with visible alteration; thin altered rusty laminations.	[]					
_					SAND (SP): light yellowish brown (2.5Y 6/4), 100% fine to medium grained sand, subangular to subrounded, predominantly fine; medium sorted; contains quartz, feldspar, amphibole, and other.	<u>60</u>					
					SAND (SW): light yellowish brown (2.5Y 6/4), 100% fine to coarse grained sand, subangular to rounded; trace fine to coarse gravel up to 32 mm, subangular to rounded; trace clay, clay balls; poorly sorted; contains quartz, feldspar, amphibole, and other.	GE					
-			<u>-</u>		SAND (SP): light yellowish brown (2.5Y 6/4), 100% fine to medium grained sand, subangular to subrounded, predominantly fine; medium sorted; contains quartz, feldspar, amphibole, and other.	65					
					SILT (ML): olive (5Y 5/4), 95% silt, olive and gray laminated silt; 5% medium grained sand, subangular to subrounded; oxidized silt laminations and sand interbeds. SAND (SP): strong brown (7.5YR 4/6), 100% fine to medium grained sand, subangular to						
					\ subrounded; well sorted; contains quartz, feldspar and amphibole; highly oxidized sand. CLAY (CL): olive (5Y 4/4), 100% clay, no plasticity, silty clay; black/grey and rusty colored laminations.						
					CLAY (CL): very dark greenish gray (10Y 3/1), 95% clay, low plasticity; 5% fine grained sand, subangular to subrounded; dark gray clay with 1-inch gray sand interbeds, black and rusty colored laminations, organics.						
					CLAY (CL): black (N2.5), 100% clay, low plasticity; black clay with dark brown and gray laminations; trace organics (seed). SAND (SP): olive (5Y 4/4), 100% fine to medium grained sand, subangular to subrounded; medium sorted; contains quartz, feldspar, mica and amphibole; higher mica content; with						
· ·	/				visible alteration/oxidation. CLAY (CL): very dark greenish gray (10Y 3/1), 100% clay, low plasticity, dense; rich in organics (wood) especially from 78.0 to 79.0 ft, laminated.	_80	\simeq	PT			
					SAND (SP): light olive brown (2.5Y 5/4), 100% fine grained sand, subangular to subrounded; well sorted; contains quartz, feldspar, mica and amphibole; alteration visible, rusty colored lamination.						
-					CLAY (CL): olive (5Y 5/3), 100% clay, medium plasticity; trace fine grained sand, subrounded, interbedded; contains quartz, feldspar, mica and amphibole; alteration visible, rusty colored laminations in sand and clay.						
					SAND WITH SILT (SP-SM): light olive brown (2.5Y 5/3), 90% fine grained sand, subrounded, very fine grained; 10% silt; well sorted; contains quartz, feldspar, mica and amphibole. SILT WITH SAND (ML): light olive brown (2.5Y 5/4), 85% silt; 15% fine grained sand,	<u></u>					
_					subrounded, fine sand bed from 89.2 to 89.6 ft; contains quartz, feldspar and mica; alteration visible, rusty laminations. SILT (ML): light olive brown (2.5Y 5/4), 100% silt, clayey silt, dense; trace clay; trace	<u>90</u>					
					alteration/oxidizing. SAND WITH SILT (SP-SM): light yellowish brown (2.5Y 6/4), 90% fine grained sand, subrounded; 10% silt; well sorted.		_	SIE\			
-			_		CLAY (CL): light olive brown (2.5Y 5/4), 100% clay, low plasticity; trace alteration including rusty colored and small black ashy deposits. SAND WITH SILT (SP-SM): light olive brown (2.5Y 5/3), 90% fine grained sand,	<u>95</u> 		SILV			
					subrounded, very fine grained, 10% silt; well sorted; contains quartz, feldspar, mica and amphibole; trace purple alteration. CLAY (CL): olive (5Y 4/4), 100% clay, no plasticity; trace fine grained sand, subrounded;	<i></i>	\	SS SS			
<u>)</u>			Zone #2		trace silt; with trace rust colored alteration. SAND WITH SILT (SP-SM): light olive brown (2.5Y 5/3), 90% fine grained sand, subrounded; 10% silt; well sorted; contains quartz, feldspar, mica and amphibole; with some rust colored alteration.						
			QC.		SILT (ML): olive (5Y 5/4), 100% silt; rounded; trace coarse gravel up to 30 mm, rounded, flat; alternating 1/2-inch bands of oxidized/rust color and olive brown. SAND (SP): light olive brown (2.5Y 5/3), 100% fine grained sand, subrounded, trace	<u> </u>	<u>×</u>	SIEV			
5	/		SC: 42,650 uS/cm		medium to coarse grained; trace fine gravel up to 5 mm, subrounded; trace silt; well sorted;	105		J V			

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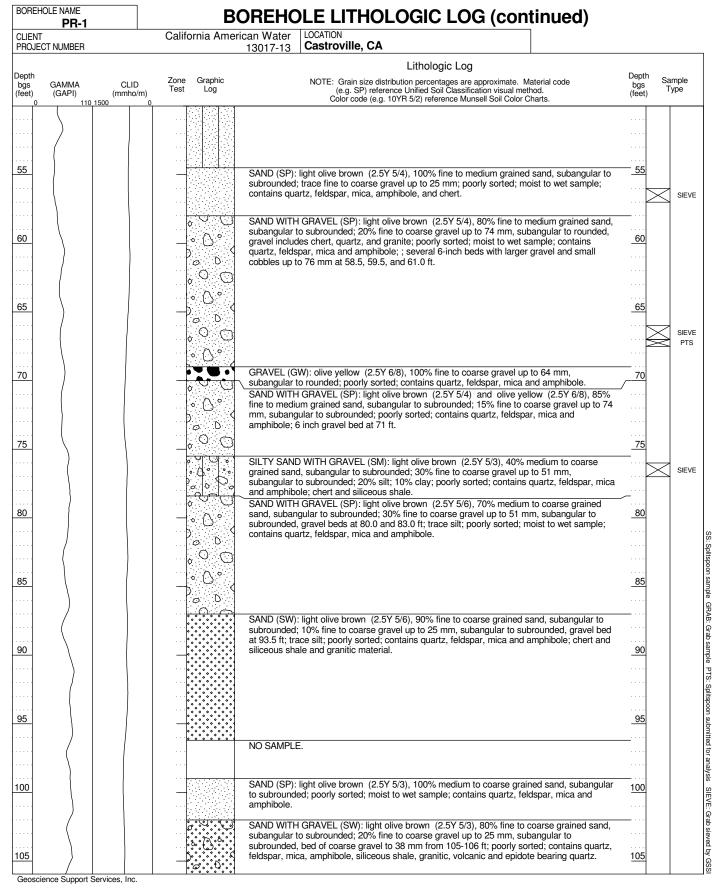
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30REHC	DLE NAME PR-1				ВС	REHO	LE LITH	HOLOGIC LO	G		
CLIENT PROJEC	T NUMBER		Cali	fornia Ame	rican Water 13017-13	LOCATION Castroville	e, CA				
EPORT	DATE				7/8/2014		d 3", -121°47'30.7	248" Geographic NAD83			
RILLING RILLER	G CONTRACTO	OR			cade Drilling se Munguia	B. Villalol	os				
RILLING IG TYPI		Prosor	nic 600T	DRILLING METHOD		Sonic	START DATE	9/21/13	BOREHOLE DIAMETER		8 in
URFAC LEVATI			9.0 ft	TOTAL DEPTH	2	01.5 ft bgs	FINISH DATE	9/25/13	CORE SIZE		6 in
epth gs eet) 0	GAMMA (GAPI)	CLID (mmho/ 1500				Color co	size distribution SP) reference Un	thologic Log percentages are approximate. M filed Soil Classification visual met 2) reference Munsell Soil Color C	laterial code hod. rharts.	Depth bgs (feet)	Sample Type
eeet) 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0			/m) 1636	- Log	subrounded; SILTY SANE to subrounded; SANDY CLA sand, subrou amphibole. SAND (SP): subrounded; quartz, felds SILTY SANE subrounded, NO SAMPLE	brown (7.5YR) poorly sorted; D (SM): dark bred; 20% silt; pour (7.5YR) brown (7.5YR) 5% fine grave par, mica and D (SM): dark gravery fine grain E.	5/3), 100% fin moist sample. own (10YR 3/3) orly sorted; moist black (5GY) e grained; moist 1 up to 5 mm, samphibole.	e to medium grained sand, so 3), 80% fine to medium graine bist sample. 2.5/1), 70% clay, organic clay at sample; contains quartz, feldium to coarse grained sand, ubangular to subrounded; po GB 4/1), 80% fine grained sa ell sorted; moist sample.	ubangular to ed sand, subangular r; 30% fine grained ldspar, mica and subangular to orly sorted; contains		Type
60					subangular t SILTY SANE subangular t silt beds. SAND (SP): to subrounde SAND (SP): well sorted; I SANDY SILT subangular t SILT (MH): c subangular t SAND (SP):	o subrounded; O (SM): dark gro subrounded; light olive browed; trace fine g dark olive graymoist sample. F (ML): dark gro subrounded, dark greenish go subrounded, dark greenish	poorly sorted; eenish gray (5 15% silt; trace on (2.5Y 5/4), ravel up to 5 m or (5Y 3/2), 100 eenish gray (5 very fine grain lary (5GB 4/1) very fine grain gray (5GB 4/1)	GB 4/1), 85% fine to medium fine gravel up to 5 mm; poor 100% medium to coarse grain m; poorly sorted; moist samp% fine grained sand, subangu GB 4/1), 70% silt; 30% fine ged; moist to wet sample; conto 90% silt, organic silt; 10% fined; moist to wet sample; conto 100% medium grained sand, 100% medium grained sand	n grained sand, ly sorted; few clayey med sand, subangular ole. ular to subrounded; rained sand, tains mica. ne grained sand, tains mica. d, subangular to	30	
10					CLAY (CL): sample; mod	dark greenish derately firm; n O (SM): dark groosubrounded;	gray (5GB 4/1) lassive; few 3 r eenish gray (5 20% silt; trace	iple; contains quartz and feld, , 80% clay, medium plasticity nm black organic stringers. GB 4/1), 80% medium to coafine gravel up to 5 mm; poor id amphibole; abundant shell	r; 20% silt; moist arse grained sand, ly sorted; moist to wet	40	
50	nce Support S	Services, Inc.			inch bi-valve		isopai, mica di	a amprissor, assuradire stiell		50	

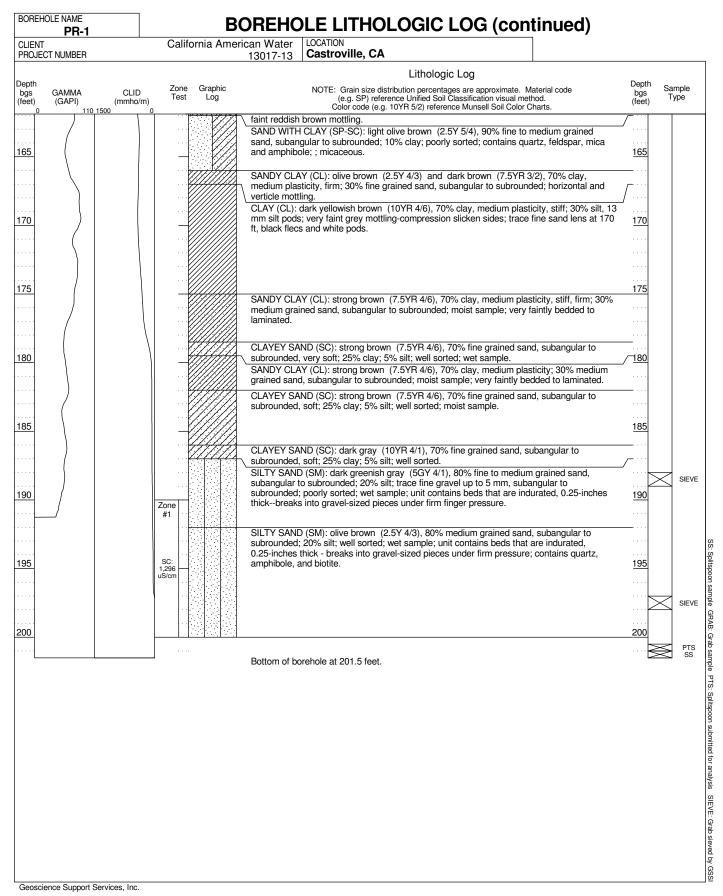
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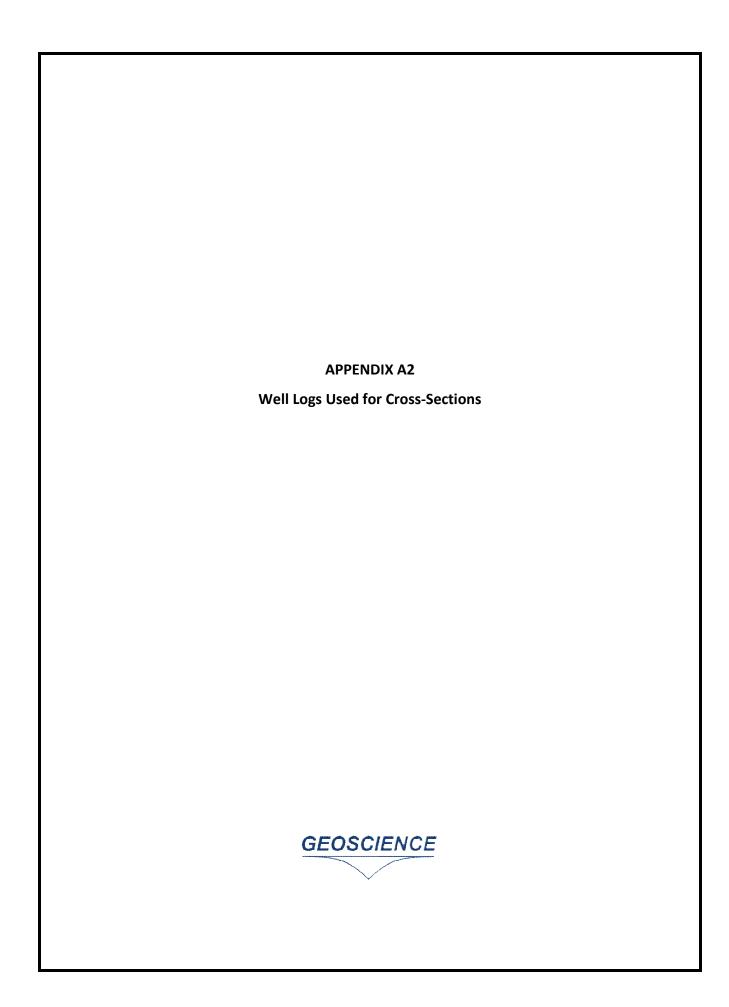


BOREHOL	E NAME PR-1			В	OREHOLE LITHOLOGIC LOG (continued)			
CLIENT PROJECT	NUMBER		Calif		ican Water LOCATION 13017-13 Castroville, CA			
					Lithologic Log			
	GAMMA (GAPI) 110 1	CLID (mmho/m)	Zone Test	Graphic Log	NOTE: Grain size distribution percentages are approximate. Material code (e.g. SP) reference Unified Soil Classification visual method. Color code (e.g. 10YR 5/2) reference Munsell Soil Color Charts.	Dept bgs (feet	Sa	mple ype
		300 0						
110	}				GRAVEL (GP): light olive brown (2.5Y 5/3), 100% fine to coarse gravel up to 38 mm, subangular to subrounded; poorly sorted; contains quartz, feldspar, mica, amphibole and siliceous shale; granitic, volcanic and epidote bearing quartz.	110		SIEVE
					SAND WITH GRAVEL (SW): light olive brown (2.5Y 5/3), 80% fine to coarse grained sand, subangular to subrounded; 20% fine to coarse gravel up to 25 mm, subangular to subrounded; contains quartz, feldspar, mica and amphibole.			SILVL
15					GRAVEL (GP): light olive brown (2.5Y 5/3), 100% fine to coarse gravel up to 38 mm, subangular to subrounded; subangular to rounded; poorly sorted; contains quartz, feldspar, mica and amphibole.	115		
					SAND WITH GRAVEL (SW): light olive brown (2.5Y 5/3), 80% fine to coarse grained sand, subangular to subrounded; 20% fine to coarse gravel up to 25 mm, subangular to subrounded; poorly sorted; contains quartz, feldspar, mica and amphibole.			
20					SAND (SP): light olive brown (2.5Y 5/4), 100% medium to coarse grained sand, subangular to subrounded; trace fine to coarse gravel up to 25 mm, subangular to subrounded; poorly sorted; moist to wet sample; contains quartz, feldspar, mica and amphibole.	120		
25			Zone		GRAVEL (GP): light olive brown (2.5Y 5/4), 100% coarse gravel up to 75 mm, subangular to rounded; trace silt; trace clay; poorly sorted; contains quartz, feldspar, mica and amphibole.	<u></u>		SIEVE
			#2 ···		SAND (SW): light olive brown (2.5Y 5/4), 100% medium to coarse grained sand, subangular to subrounded; trace fine to coarse gravel up to 25 mm, subangular to subrounded; poorly sorted; moist to wet sample; contains quartz, feldspar, mica and amphibole.			
30	/		SC: 53,610 uS/cm			130		
					GRAVEL (GW): light olive brown (2.5Y 5/4), 100% fine to coarse gravel up to 38 mm, subangular to rounded; trace silt; trace clay; poorly sorted; contains quartz, feldspar, mica and amphibole.			
35				$\circ \circ \circ$	SAND WITH GRAVEL (SP): light olive brown (2.5Y 5/4), 85% medium to coarse grained sand, subangular to subrounded; 15% fine to coarse gravel up to 25 mm, subangular to subrounded, predominantly fine; coarse gravel bed from 138.5-139.0 ft; poorly sorted;	135		
				000	contains quartz, feldspar, mica and amphibole.			
40					CLAY (CL): olive brown (2.5Y 4/3) and light olive brown (2.5Y 5/3), 70% clay, medium plasticity, stiff; 30% silt; massive, black organic streaks, very faint grey mottling, 4.6 - 6.4 mm elongated carbonate pods, 4.6 mm reddish brown sandy pods.	140		
					J			
45						145		PTS
					SILT (ML): olive brown (2.5Y 4/3), 60% silt, soft to firm; 30% clay; 10% fine grained sand,			
50			_		SIL1 (ML): Olive brown (2.5Y 4/3), 60% stilt, soft to firm; 30% clay; 10% fine grained sand, subangular to subrounded; moist sample; contains mica.	<u>150</u>		
					CLAY (CL): dark greenish gray (5GB 4/1), 70% clay, medium plasticity; 30% silt; trace fine grained sand, subrounded, very fine grained elongate sand pods to 6.4 mm; massive,		>	PTS
55					compression slicken sides, small carbonate flecks, very faint yellow-blue mottling.	155		
60	/				SANDY CLAY (CL): grayish brown (2.5Y 5/2), 70% clay; 30% fine grained sand,	160		
	ce Support Se				subrounded; contains quartz, feldspar, mica and amphibole; ; sand increases at 161.5 ft with	····		

Telephone: (909) 451-6650 Fax: (909) 451-6638

www.gssiwater.com





APPENDIX A2:

WELL LOGS USED FOR CROSS-SECTIONS

CONTENTS

Description	Page
13S/1E-36H (Monterey Dunes Colony Well)	
14S/1E-24L2-5 (DMW1)	
14S/2E-6L1	
14S/2E-17K1	
14S/2E-17L1	
14S/2E-18E1	
14S/2E-20B3 (?)	A2-9
14S/2E-21E1	A2-11
14S/2E-21F2	A2-11
Borehole TH-1	
Borehole TH-2	
Borehole TH-3	



ORIGINAL File with DWR

STATE OF CALIFORNIA

WELL COMPLETION REPORT

Refer to Instruction Pamphlet

Age 1 of 2 Owner's Well No. #4

No. e011049

Date Work Began 01/24/04 Ended 03/10/04

Local Permit Agency Monterey Dunes Health Dept

Permit No. 03-01231 Permit Date 11/18/03

STATE WELL NOJSTATION NO.

LATITUDE

APN/TRS/OTHER

Permit No. 03-01231 Permit Date 11/1	8/03 WELL OWNER
GEOLOGIC LOG	Washing Burns Calany
ORIENTATION () X VERTICAL HORIZONTAL ANGLE (SPECIF	
DRILLING Direct Rotary FLUID Bentonite	Mailing Address 195 Monterey Dunes Way
SURFACE DESCRIPTION	Castroville, CA 95012 STATE ZP
Ft. to Ft. Describe material, grain size, color, etc.	
0: 80 Fine to course sand	Address 195 Monterey Dunes Way
80: 90 Fine to course sand w/blue clay	City Castroville
90 100 Fine to med. sand	County Monterey
100 123 Fine to med, sand w/clay lenses	APN Book 229 Page 041 Parcel 004
123 143 Blue clay w/fine to med. sand	Township Range Section
143: 154 Blue clay w/fine to course sand	Latitude I NORTH Longitude I WI
and gravel	
154 165 Fine to course sand w/gravel	LOCATION SKETCH DEG. MM. SEC. ACTIVITY (**) New Well
and rock	14cusing
165 187 Fine to med, sand & cobbles	PARKING LOT Deepen
with clay lenses	Other (Specify
187: 197: Fine to med. sand	
197 219 Fine to course sand	Procedures and Mate
219 250 Fine to course sand & gravel	Under "GEOLOGIC L
	PLANNED USES (
	— Domestic — Publ
304 314 Fine to course sand w/clay and	United the second secon
cobbles	MONITORING
314 355 Fine to course sand w/90% clay	MONITORING TEST WELL CATHODIC PROTECTION HEAT EXCHANGE DIRECT PUSH INJECTION
355 366 Fine to course sand w/clay	CATHODIC PROTECTION
366 387 Fine to med. sand w/clay lenses	DIRECT PUSH .
387 408 Fine to med. sand w/50% clay	
408 418 Fine to course sand	VAPOR EXTRACTION SPARGENG
418 440 Fine to course sand & gravel	North SPARGING
440 455 Fine to course sand w/40% clay	
455! 461! Fine to course sand & gravel	Illustrate or Describe Distance of Well from Roads, Buildings, Fences, Ricers, etc. and attach a map. Use additional paper if necessary, PLEASE BE ACCURATE & COMPLETE.
with 50% clay	WATER LEVEL & YIELD OF COMPLETED WELL
461 485 Fine to course sand & gravel	
485 505 Fine to course sand	DEPTH TO FIRST WATER N/A (Ft.) BELOW SURFACE
505 556 Fine to course sand & gravel	DEPTH OF STATIC 13 (Ft.) & DATE MEASURED 03/04/04
556. 577 Fine to course sand w/red clay	ESTIMATED VIELD - 200 (GPM) & TEST TYPE PUMP
TOTAL DEPTH OF BORING: 1422 (Feet)	TEST LENGTH 24 (Hrs.) TOTAL DRAWDOWN 42 (R.)
TOTAL DEPTH OF COMPLETED WELL 1364 (Feet)	* May not be representative of a well's long-term yield. 24 hour Tes
orne per in or community in the Community	ruly not be representance of a wears long-term yield. 24 11001 168
DEPTH CASING (S)	DEPTH ANNULAR MATERIAL

DE	EPT	н	BORE-					CASING (S)			DEPTH ANNULAR MATERIAL							RIAL	
FROM	SU	RFACE	HOLE	1		(=)					FROM					TY	TYPE		
FL	to	ค.	DIA. (inches)	BLANK	SCREEN	DUCTOR FILL PIPE	MATERIAL / GRADE	INTERNAL DIAMETER (Inches)	GAUGE OR WALL THICKNESS	SLOT SIZE IF ANY (Inches)	Fl.	to	PL.	CE- MENT (×)	BEN- TONITE ()	FILL (×)		TER PACK YPE/SIZE)	
0	1	60	36			x	A53B	29.260	.375		0	,	60	X	-	,	10	sack	
0	i	321	28	T		x	A53B	19.260	.375		0	1	321	х			10	sack	
+2	11	221	18	1 2	1		A53B	8"	.322		0	11	220	x			Nea	t cem	
221	11	301	18	1 >			304ss	8"	.322		1220	11	370			x	8x		
301	11	361	18		x		304ss	8"	XXHD	.040		-		1					
361	11	364	18	×			30455	811	.322			1							

___ Geologic Log

___ Well Construction Diagram

__X Geophysical Log(s)

___ Soil/Water Chemical Analyses

ATTACH ADDITIONAL INFORMATION, IF IT EXISTS.

I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and bellef.

NAME Rottman Drilling Co.

46471 N Division, Lancaster, CA 93535

Larry W. Rottman, President

03/19/04 C

316599 C-57 LICENSE MUMBER

ORIGINAL DWR USE ONLY STATE OF CALIFORNIA - DO NOT FILL File with DWR WELL COMPLETION REPORT Page 2 of 2 Refer to Instruction Pamphlet No. e011049 Owner's Well No. 01/24/04 __, Ended 03/10/04 LONGITUDE Date Work Began_ Local Permit Agency Monterey Dunes Health Dept APN/TRS/OTHER Permit No. 03-01231 Permit Date 11/18/03 GEOLOGIC LOC WELL OWNER X_ VERTICAL ____ HORIZONTAL __ __ ANGLE ____ (SPECIFY) Name Monterey Dunes Colony DRILLING Direct Rotary FLUID Bentonite Mailing Address 195 Monterey Dunes Way DEPTH FROM DESCRIPTION SURFACE Castroville, CA 95012 Describe material, grain size, color, etc. Address 195 Monterey Dunes lenses 610 Fine to course sand, rock & clay City <u>Castroville</u> 610 620 Fine to course sand County Monterey 630 Fine to course sand & gravel 620 i APN Book 229 Page 041 Parcel __ 004 650 Fine to course sand & gravel Township _____ Range _ Section _ with clay lenses Latitude NORTH
DEG. MIN. SEC.
LOCATION SKETCH 661 Fine to med. sand with clay Longitude. 650 DEG. MINL ACTIVITY (=) 661 681 Fine sand with clay 681 693 Fine sand & gravel w/clay lenses MODIFICATION/REPAIR 725 80% Silty clay w/20% hard sand _ Deepen 737 90% Hard silty clay & sand lense 725 ___ Other (Specify) 737 767: 90% Hard silty clay w/sand rock DESTROY (Describe lenses Procedures and Materials Under "GEOLOGIC LOG" 791 95% Hard packed clay - cemented 820 Brown silty clay (hard packed) PLANNED USES (=) WATER SUPPLY 882 Grayish brown clay w/blue stricks _ Domestic Irrigation 882 945 Clay with rock MONITORING 945 : 1011 : Clay w/fine sand & silt TEST WELL 1011 : 1105 : 20% Clay w/fine to med sand CATHODIC PROTECTION 1105 1170 Fine sand and silt HEAT EXCHANGE 1170 1190 Clay w/fine sand, silt & rock DIRECT PUSH 1190 | 1230 | Fine sand, silt & rock 1230 | 1270 | Clay with fine sand INJECTION VAPOR EXTRACTION 1270 : 1290 : Silt & clay SPARGING Blustrate or Describe Distance of Well from Roads, Buildings, Fences, Rivers, etc. and attach a map. Use additional paper if necessary, PLEASE BE ACCURATE & COMPLETE. REMEDIATION 1290 : 1365 Fine sand OTHER (SPECIFY) 1365 1391 Clay w/fine sand lenses WATER LEVEL & YIELD OF COMPLETED WELL DEPTH TO FIRST WATER _______12 (PL) BELOW SURFACE DEPTH OF STATIC 13 (FL) & DATE MEASURED _03/02/04 WATER LEVEL_ _ (GPM) & TEST TYPE TO 102 500 Pumo ESTEMATED YIELD . TOTAL DEPTH OF BORING: 1422 (Feet) TEST LENGTH 4 (Hrs.) TOTAL DRAWDOWN TOTAL DEPTH OF COMPLETED WELL 1364 (Feet) * May not be representative of a well's long-term yield. (Step Test) DEPTH FROM SURFACE CASING (S) BORE-HOLE ANNULAR MATERIAL DEPTH FROM SURFACE TYPE (土) TYPE SCREEN CON-DUCTOR FILL PIPE MATERIAL / GAUGE SLOT SIZE CE. BEN-DIAMETER OR WALL GRADE IF ANY MENT TONITE FEITER PACK FILL to PL (TYPE/SIZE) (=) (=) 60 36 A53B 29.260 375 0: 60 X 10 sack 0:321 28 A53B 19,260 .375 0: 321 X 10 sack +2 11221 18 811 A53B .322 0:1220 Neat cem. 811 1221 11301 18 304ss .322 1220 1370 8x16 X 1301 1361 18 811 304ss XXHD 040 1361 1364 18 k | ATTACHMENTS (±) 30455 322 CERTIFICATION STATEMENT

... Geologic Log _ Well Construction Diagram X Geophysical Log(s) ___ Soit/Water Chemical Analyses Other

ATTACH ADDITIONAL INFORMATION, IF IT EXISTS.

DATE 155 REV. 11-97

I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and bellef.

STATE

316599

C-57 LICENSE MUMBER

Rottman Drilling Co. CPERSON, FIRM, OR CORPORATION (TYPED OR PRINTED)

46471 N Division, Lancaster, CA 93535

03/19/04

IF ADDITIONAL SPACE IS NEEDED, USE NEXT CONSECUTIVELY NUMBERED FORM A2-2

REPRESENTATIVE

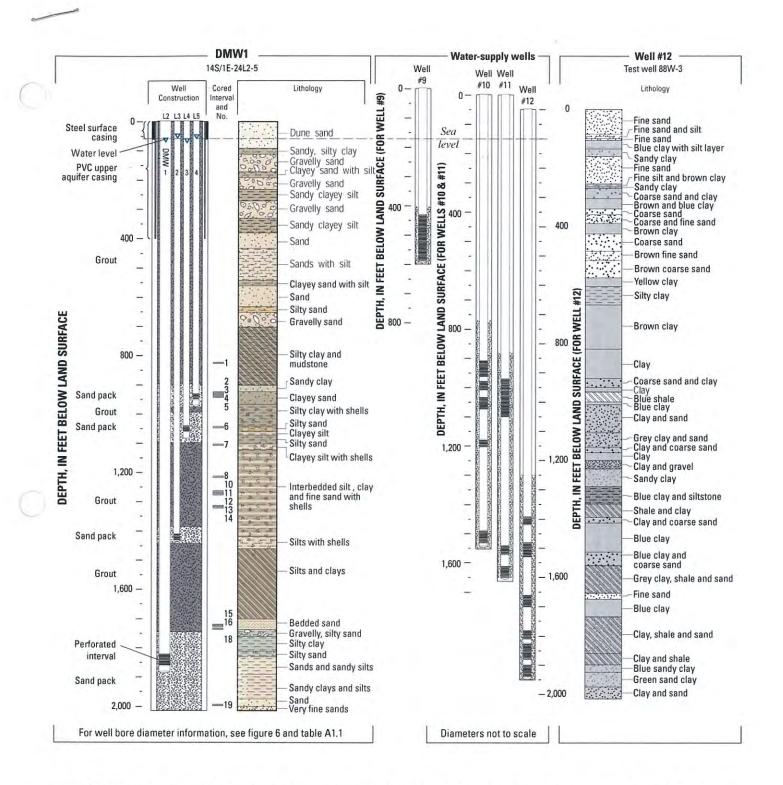


Figure 3. Well construction and lithology for the deep-aquifer monitoring well and selected nearby water-supply wells, Marina, California.

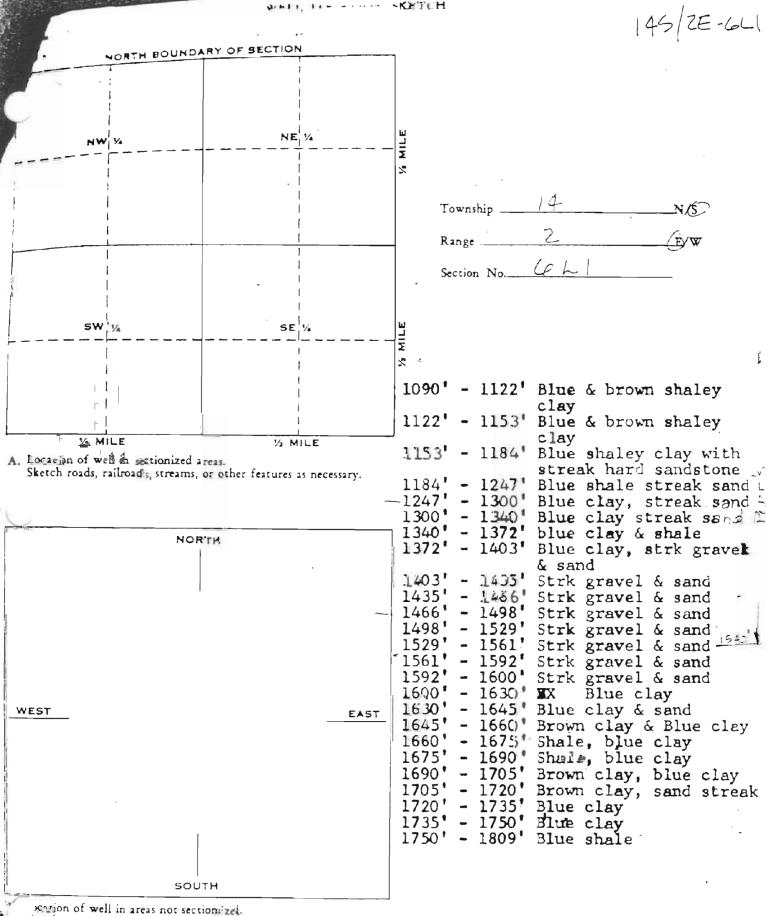
PLICATE Gleve Teylor

THE RESOURCES AGENCY DEPARTMENT OF WATER RESOURCES WATER WELL DRILLERS REPORT

Do Not Fill In

Nº 141763
State Well No. 195 ZE -6L \
Other Well No.

OWNER:					(11) WEL	L LOG:	
me Nontere	y Count	v E100	d Cont	rol Di	Motal depth	1809	fs. Depth of completed well 1560 f
dress County					1	icribe by color.	character, size of material, and structure
Salinas						0_	to 6 Top Coil 6
LOCATION OF					AR.		
Montere	V	Owner's number.	of any		61	- 15'	Blue sandy clay
nship, Range, and Section	,	m Hill			15'		Fine blue sand
ance from sitter, roads, railro			hed ma	ח	32		Blue clay w/sea shell
					60.	- 75'	Blue soft sand
TYPE OF WOR	RK (check):			75'	- 1001	Blue clay
Well & Deepening	Recon	ditioning [Destroyin	ng 🗀	100	- 184	Blue clay & sand streak
estruction, Jescribe mate		ure in Item 11.			184	- 278	Coarse sand & gravel
PROPOSED US	E (check)	:	(5) EQU	IPMENT:		- 300	Yellow Clay
mestic Industria		l l	Rotary	$\Box_{\mathbf{x}}$	300	3.30	Blue clay
igation Test We			Cable	$\vec{\Box}$		- 360'	
			Other	ō		- 500	of clay
CASING INST	ALLED:				360	- 4341	Yellow clay, streaks blu
	THER	1f	gravel pac	ked			& brown shale
GLE TX DOUBLE T]	- •		4.34.1	- 640	Yellow clay, streaks blu
	,						& brown shale
rom fo	Gage	Diameter of	From	Τυ	4401	4.00	White coarse sand
fr 11. Dia	1	Bore	ft.	1 t.	490'	5201	Blue clay
600' 1	6 3/8	28-1/	2 0	600			
The second second	-	cer 26	1000			610	Sand & gravel, streak cl
20.75 - 20.1 10.5 25 - 25	2" 342	26		603 1563	610'	C 01 1	Yellow Clay
of shore a well range		Swe of gravel				7151	Sand & gravel
ibe with Weld		38501 111411	- Spec	sand	621'	715	
PERFORATION	IS OR SCI	RFFN.			715	7/.71	Vallay alay //strack mag
of the Characters of many of the		CDDIT.			747'	7701	Yellow clay w/streak gra
nick	1					- 795'	Yellow clay w/streak gra
troni or To	Perf. per	Rows	١.	Size		1.9.)	J
11 880 in	row	ft.	1	x in.	7951	9/.01	blue clay
850 × 1540			2/22	Horz.	7.93	- 040	Yellow clay w/streak gra
1340					840'	0701	blue clay
		 		re Full	6701	- 8/2	Blue clay 30
		 	Flo		872	- 503.	Blue clay
	-	1	-+		9031	- 934	Brown clay
CONICTION	<u> </u>	J			934	- 965'	Hard brown clay & shale
CONSTRUCTIO				4.6.0	965	997'	Hard brown clay & shale
s surface sanitary seal provide				800 ft	997'	- 1028	Hard brown clay & shale
any orrata scaled against poll	ution? Yes G	No 🗆	If yes, note	depth of strain	1028	1059	Blue clay
ft. to	ft.				1059'	1090	Blue & brown clay
/t. to	ft.				Work started	9/20	19 76. Completed 11/12 19 78
od of sealing Concr		30" s	teel c	onducto	WELL DRI		
WATER LEVEL				100	This well of my knowl		inder my jurisdiction and this report is true to the be
h at which water was first f	ound, if known		ſs		JI MJ KNOW	e Ki wan beili	у.
ine level before perforating	, if known		ſŧ.		NAME S	alinac	Pump Co
" ne level after perforating :	and developing		ſt.				erson, himfor corporation) (Typed or printed)
WELL TESTS:					Address	128 Ma	digan Iana
pump test made? Yes -	No []	f yes, by whom?			ç	alinas	Ca. 93901
gal. 'min		fr. drawdow	n after	hrs	[SIGNED]	The state of	a French
resture of water	1000	cal analysis made		_		and the same	(Vell Dollar)
	W B1 2 CREMI						
electric log made of well? Y		li ver ar		ŧυ □	.,	27 20 5	2 5 1



hopen roads, railroads, streams, or other features as necessary.

Indicate distances.

145/62E-17K1

TRIPLICATE Owner's Copy

STATE OF CALIFORNIA
THE RESOURCES AGENCY
TO ADTMENT OF WATER RES

DEPARTMENT OF WATER RESOURCES
WATER WELL DRILLERS REPORT

NEW WATER SUPPLY WELL LOCATED)

Do not fill in

No. 286024

State Well No. 145/62E-17K6/ Other Well No PRESSURE - 180 Ft.

ddress P.O. E		Waste Mymot Di	strom ft to ft Formation (Describe by color, character, size	or material)
ity	brina, CA 9393	3ZIP	0 - 4 Top soil	
2) LOCATION	OF WELL (See ins	tructions):	4 - 35 Beach sand	
	srey Ov		35 - 56 Brown silt	
		na Disposal sita	56 - 91 Loose red sand	
ownship =		Section	91 == 126 Green clay & sand	
stance from cities	roads, railroads, fences, e		126 - 152 Rod sand water hearing	
**			152 - 159 Green clay	
17 17	11 5 m		159 - 194 Charges sand	
	114	J. Drain France	194 - 805 Sticky breen clay	
	A	(3) TYPE OF WORK:	205 - 255 Goarse\grave!	
(4)	× 34 americ	New Well Deepening		
PA -	2 7115	5 to 1 to 2 to 2 to 2 to 3 to 3 to 3 to 3 to 3		
	2	Reconditioning		
FI - EM	7 7 4	Horizontal Well		
10	7 . 4	Destruction [(Describe	11-	
一个工事(3	destruction materials and pro	0 1/1/2	
12.23	-			9/.
	2]	(4) PROPOSED USE		
101	5 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	Domestic realized + A	-100	
		Irrigation	4 1 1050	
V MA	TH.	Industrial 5 *	m O7-/>	
	tu maker much :			
	misapp cation	1 11	2/1/20	
元が海をは				100
	OCATION SKETCH	(Describe)	V	
EQUIPMENT	SOCIE SE DESERTIN	GRAVEL RACK	A TOTAL ON THE PROPERTY OF THE PARTY OF THE	
Rotary La	Reverse 🗆 🏋		the service committee warmers in	
Cable ET	Air 🗆 🗆	netes of bore half		
Other II.4	Bucket Pac	ced from 18059 to 250	(Cit) A c + it userated with study sources	~, : "
可以外的基础	ED- 17 (8)	Convert Acritical Services	Sand ensored, extra-quick this overload relays	
7) CASING INSTAL	(9)	retroin Tions pea grave	Can to the Company of	- 12.5
teel 🗆 Plasti		s or bettoepou or erse or screen.	Σ	
From To	Dia Gage or	To Stot	NAME OF TAXABLE PARTY O	1 344
tt . Kith	m Wall	Size		
0 210	6 CVCSDP21F48	210 250 030	pyc sand Screen	
1000000		- 01112		-
No. of the second	OF WERCHANTS	און דע אין בודים בינים יותב		
9) WELL SE	AL: SEYOND THE DU	-	BLE 3 (PPESS VEARPARTES AND NOSE MENTAL	5. We
Was surface sanitary s	eal provided? Nat & d.N	If yes to depth 180	-th tation of incidental or isosophical areades or	A FAR TO
Were strate scaled aga	inst pollution? inst pollution?	No. E. Anthemala solid		89 19
Method of staling	to vou noat for	ent 's you specific least re		
(10) WATER	LEVELS: 10 state	31	WELL DRILLER'S STATEMENT:	9 mg/m
Depth of first Valler, if	known	31	This well was drilled under my jurisdiction and this report is	true to the
Depth of first Scales, if Standing lever after w	ell completion	73 131	-ft. best of my knowledge and belief.	
(11) WELL T	ESTS:		Signed James J. John	\$-J. 10
		l yes, by whom? Solf Air lift	Well Driller)	A
Type of test	toftest 121 ft.	At end of test 736 Water Emperature 67 Yes, by whom? A 130 Fyes, attach copy to this report	NAME FRED ASI & SONS TAY (Person, time or corporation) (Typed or printed) 7 Address 16339 Castrovi 11e Blvd	
Discharge block	gal/min after 223 hour	Water femperature 57	Address 16339 Castroville Blvd.	
Chemical analysis ma	del Ye Te No L	yes by whom? Al Tab	City Salfnas, Cl 93907 71P	C 100
773 176	THE TREE TO THE THE	Carrier to be a finisher	License No. 391047 Date of this report	B_0_80

STAIRITE INDUSTRIES, INC.

To the Fabruage Impostment Inc. 1980, 1381

ROY V. ALSOP & SON Well Drilling

FAIRBANKS-MORSE PUMPS AND PRESSURE SYSTEMS POMONA

SALINAS, CALIFORNIA 93901

Dia. 14" #10 ga.

LOG OF WELL

June 3, 1972

for

Monterey Peninsula Garbage & Refuse Disposal District

			1
0 ft.	to	108 ft.	Sand Blue clay
132	11	144	Yellow sandy-sediment
144	11	148	Blue clay
148	18	162	Sandy yellow sediment
162	17	176	Fine packed sand
176	12	188	Yollow clay
188	19	200	Sand & fine gravel
200	18	206	Fine silty sand
206	15	214	Fine sand & float rock
214	77	226	Blue clay
226	11	236	Yellow clay
-146 > 236		240	Fine gravel
240 T	111	747	Sand & gravel
303	11	305	Yellow clay
305	!1	320	Mucky sand
320 I	11	351	Sand & gravel
351	11	354	Soft sand stone

Perforations: 244 ft. to 303 ft.

Concrete Plug - 6 ft.

Static Water Level - 1392 ft.

Bumps 1090 gal per minute

Ground elev. approx 90 feet

LATE CALIFORNIA 18E1

THE RE OURCES AGENCY

THE RESOURCES AGENCY

File with DWE THE TOTAL LO DEPARTMENT OF WATER RESOURCES

Do Not Fill In

Nº 121665

	water C	ode Sec	. 10w.a	TER W	ELL D	RILLERS RE	EPORT	Other Well No.				
(1) OWN	ER: Arm	strong R	ench			(11) WELL LC	G:					
	M. L. Du					,		870				
Name 6/0	Dox P,	Cacing in	. 	516		Total depth		ft. Depth of completed well 870 ft.				
Address	, 20) ,					Formation: Describe by	color, character	to to 75 fine sand				
Technology (_					75 to	1001	coarse gravel				
(2) LOCA	TION OF					100	100,	125 gravel-ctreaks clay				
County Mont	GLel	0	wner's number.	if any	_	125		150 SLLY TUCK				
Township, Range	and Section TN	gen Mari	ma œ Ça	20104111		150		175 coarse gravel				
Distance from cit	in, rost, filled			ili fing ±	1	175		200 ##RPERRARSENALK==PFFF				
100		<u>pis Bars</u>				 						
	OF WOR				_	200		225 Pina conj strank also				
_	Deepening				s 🗆	225		250 fine sand streak clay				
	describe materi					250		275 gravel				
` '	OSED USE	•		(s) EQUI		22.5		300 sine sony " strank wys				
] Industrial			Rotary	괄	300		325 shite eard				
Irrigation [Test Well		her 🗌	Cable .		725		357 sindualin strooks				
				Other		350		575 send				
(6) CASII	NG INSTA	LLED:				37.5		400 sina erni				
STEEL	.: ОТ	HER:	If	gravel pack	s e d	<u> </u>		<u> 425 = cnd = = vol</u>				
SINGLE 🔯	DOUBLE [425		450 sand gravel				
1	1	Gage	Diameter	1	ł	450		475 sand streaks clay				
From	To	or	of	From	То	47.5		500 coarse gravel-clay				
ft.	ft. Diam	. Wali	Bore	fc.	ft.	500		525 sand olay				
	303 14"	1/4	26	300	370	525		550 sand clay				
303	305 1412	la" red	coer	=.2'.		550		575 sandy clay				
06 8	370 12	1/13				57 <		600 fine part olay				
Size of shoe or -	ell cing:		Size of erave	11/4 per	â	600		625 sand				
Describe juint	alded					625		650 Red clay smayel				
(7) PERF	ORATION	OR SCF	REEN:			5.50		575 yellow clay				
` '	un or name of scre					67.5		AGO Aerich ofsh				
		Perf.	Rows			700		725 Time gravel				
From	To	per	per	s	ize	725		750 coarse gravel				
fr.	ft.	row	ft.	in.	x in.	7.50		770 coards gravel				
656	834	3	42	1/8" :	std lour	re ?75		800 fine gravel				
4.8.						800		825 coarse gravel				
						625		850 coarse gravel				
						لتر 6		6/5 yellow olsy				
						87.5		890 wellow clay				
(8) CONS	TRUCTIO	N ·				890		913 vellow play				
-	vitary seal provided		. Π τ	o what deptiff ?!	n fo							
	ealed against pollu		No 🗀		depth of strata							
From 0	11. to 300		110	11 901, 11010	Jept// 0/ 11/11/1							
From	ft. to	ſŧ.				Work started 7-2-	-74	Completed 7-7-7-19				
Method of sealing						WELL DRILLER"						
						_		my jurisdiction and this report is true to the bes				
	ER LEVEL			fr.		of my knowledge an						
	elure perforating.					Salinas Pump Co.,						
	fter perforating as	-		ft.			(Person, fi	rm, or corporation, (Typed or printed)				
	L TESTS:		S C + C - 1	- It		- 1128 Mad	dison La	ane, Salimas, Ca.93901				
at pump test m		- Y		1		Audress	<u> </u>					
Yield.			f yes, by whomi			(Sieven)	-	10 week ve				
Temperature of	gal./min. w		fr. drawdov		bri.	[SIGNED]		(till Dulan)				
		w as a coemic	TOTAL TOTAL	: 153 U N	<u> </u>	2725	3.53					

Vas zlectric log made of well? Yes . No .

TRIPLICATE DWR USE ONLY - DO NOT FILL IN STATE OF CALIFORNIA Owner's Copy WELL COMPLETION REPORT Page ___ of ___ Refer to Instruction Pampblet STATE WELL NO./STATION NO. 701471 06/26/97 419777 Owner's Well No. _ 06/18/97 Date Work Began _ LATITUDE __ , Ended _ LONGITUDE Local Permit Agency MONTEPEY COURTY DEPARTMENT OF HEALTH 'WSAL 97 067 _ Permit Date _____04:07/97 - GEOLOGIC LOG -- WELL OWNER ORIENTATION (∠) _ ___ VERTICAL ____ HORIZONTAL ____ ANGLE ____ (SPECIFY) Name _ HENT CA 5 HARRIS COURT DEPTH TO FIRST WATER _____ ___(Ft.) BELOW SURFACE Mailing Address. DEPTH FROM HONTEREY, CA. 93940 SURFACE DESCRIPTION STATE Ft. to Describe material, grain size, color, etc. 71P WELL LOCATION 14811 DEL MONTE AVE. TOP SOIL Address _ ŝ 60 CLEAN HOLE HONTEREY City_ Qiji 60 SAND HONTEPEY County ... SAUDY CLAY AND CLAY ъğ 100 175 Page ___ ⁰¹¹Parcel 041 APN Book _ 100 (120 BLUE CLAY AND SANDY CLAY Township_ _ Range _ _ Section . 155 120 Latitude _ NORTH Longitude MIN. 155 160 SANDY CLAY AND SAND DEG. SEC - LOCATION SKETCH -ACTIVITY (土)・ 150 180 SAND AND GRAVEL NEW WELL 180 200 SAND SEE ATTACHED MODIFICATION/REPAIR 200 220 CLAY. ____ Deepen 220 230 CLAY AND SAND __ Other (Specity) 230 SAND AND GRAVEL Jeternia. 240 340 245 SAND DESTROY (Describe 255 245 CLAY Procedures and Materia Under "GEOLOGIC LOG 255 250 SAND PLANNED USE(S) 260 280 SAND AND LITTLE CLAY $1 \leq 1$ _ MONITÓRING 286 345 SAND AND GRAVEL WATER SUPPLY 345 360 CLAY Domestic 360 380 CLAY AND SAND A Public 380 400 BROWN AND BLUE CLAY ____ Irrigation 400 486 CLAT ___ indestriai 480 520 CLAY AND SANDY CLAY "TEST WELL" 520 540 CLAY AND GRAVEL CATHODIC PROTECTION
OTHER (Specify) SOUTH -540 560 CLAY AND SAND Illustrate or Describe Distance of Well from Landmarks 560 562 SAND such as Roads, Buildings, Fences, Rivers, etc. PLEASE BE ACCURATE & COMPLETE. 562 600 SANDY CLAY DRILLING 500 640 CLAY AND FINE SANDY CLAY PEVERSE ROTARY WATER METHOD. . FLUID . 640 655 - WATER LEVEL & YIELD OF COMPLETED WELL -CLAY DEPTH OF STATIC 162.25 (FL) & DATE MEASURED _____ 660 655 ! SAND 08/18/97 250 (GPM) & TEST TYPE_ ESTIMATED YIELD*___ 840_ (Feet) TOTAL DEPTH OF BORING TEST LENGTH _____ (Hrs.) TOTAL DRAWDOWN _____ 19.33(Ft.) TOTAL DEPTH OF COMPLETED WELL . * May not be representative of a well's long-term yield. (Feet) CASING(S) ANNULAR MATERIAL DEPTH DEPTH BORE-FROM SURFACE FROM SURFACE TYPE (上) HOLE TYPE INTERNAL GAUGE SLOT SIZE DIA. SCREEN CON-DUCTOR FILL PIPE MATERIAL / BLANK CE- BEN- MENT TONITE FILL DIAMETER OR WALL IF ANY (Inches) GRADE FILTER PACK Ft. to Ft. (inches) THICKNESS (Inches) to Ft. (TYPE/SIZE) (스)[(스)](스) Û 50 32 STEEL .250 STAINLESS .040 91 650 $\chi_{\mathcal{O}}$ o i 670 22 STEEL .250 STAINLESS 650 i 940 ХХ 8X16 570 ! 730 22 X .250 Stainļess .040 STEEL 730 : 785 22 .250 stainless STEEL 785 808 22 STEEL ,250 STAINLESS . 040 805 825 2.2 Х STEEL STAINLESS .250 ATTACHMENTS (∠) - CERTIFICATION STATEMENT I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief. Geologic Log MAGGIORA BROS. DRILLING, INC. NAME (PERSON, FIRM, OR CORPORATION) (TYPED OR PRINTED) Well Construction Diagram Geophysical Log(s) 595 AIRPORT BLVD. WATSONVILLE, CA 95076 Soil/Water Chemical Analyses ADDRESS 11/14/97 STATE 243957 Other Signed WELL DRILLER/AUTHORIZED REPRESENTATIVE ATTACH ADDITIONAL INFORMATION, IF IT EXISTS. DATE SIGNED C-57 LICENSE NUMBER

TRIPLICATE STATE OF CALIFORNIA DWR USE ONLY - DO NOT FILE Owner's Copy WELL COMPLETION REPORT Page 🔬 of 🗟 Refer to Instruction Pamphlet STATE WELL NO./STATION NO 419779 LATITUDE Date Work Began _______, Ended ______, Ended _____ LONGITUDE Local Permit Agency MONTEPRY COUNTY DEPARTMENT OF HEALTH Permit No. 'WSAL 97-067 _ Permit Date _ - GEOLOGIC LOG -WELL OWNER ORIENTATION () VERTICAL HORIZONTAL ANGLE (SPECIFY) MRWPCL DEPTH TO FIRST WATER _____(Ft) BELOW SURFACE Mailing Address S HARRIS COURT DEPTH FROM DESCRIPTION MONTEREY, CA. 93940 Ft. Describe material, grain size, color, etc. to Ft. - WELL LOCATION -660 ' 680 COARSE SAND AND GRAVEL 14811 DEL MONTE AVE. Address _ 680 700 COARSE SAND City ____ HONTEREY 700 715 HARD SAND County ___ HOHTEREY 715 SAND AND GRAVEL 720 APN Book 175 Page 011 Parcel __ 726 730 SAND AND GRAVEL Township . __ Range __ . Section . 730 Latitude _ 740 CLAY DEG. MIN. SEC. NORTH Longitude DEG. MIN. 740 780 HARD CLAY · LOCATION SKETCH · ACTIVITY (<) -785 780 CLAY - NORTH -NEW WELL 785 790 SAND AND GRAVE! SEE ATTACHED MODIFICATION/REPAIR 790 600 HARD SAND ____ Deepen 800.1 840 ' CLAY ____ Other (Specify) DESTROY (Describe Procedures and Materials Under "GEOLOGIC LOG". PLANNED USE(S) (ビ) MONITORING WATER SUPPLY Domestic X Public irrigation Industrial "TEST WELL" _ CATHODIC PROTEC-SOUTH -Illustrate or Describe Distance of Well from Landmarks such as Roads, Buildings, Fences, Rivers, etc. PLEASE BE ACCURATE & COMPLETE. OTHER (Specify) REVERSE ROTARY _ FLUID _ WATEL - WATER LEVEL & YIELD OF COMPLETED WELL -DEPTH OF STATIC WATER LEVEL _ ESTIMATED YIELD * 250 (GPM) & TEST TYPE ____ DIDAP TOTAL DEPTH OF BORING ___ TEST LENGTH ___5.5 (Hrs.) TOTAL DRAWDOWN __19.33 (Ft.) <u>...840</u> (Feet) TOTAL DEPTH OF COMPLETED WELL 825 (Feet) * May not be representative of a well's long-term yield.

	≃тн	BORE-			С	ASING(S)				EPTH	1	1	ANNU	LAR	MATERIAL	
FROM S	URFACE	HOLE DIA.	-	'PE (∠)		INTERNAL	GAUGE	SLOT SIZE	FROM	SUR	FACE	TYPE				
Ft. t	o Ft.	(Inches)	BEANK	SCREEN CON- DUCTOR FILL PIPE	MATERIAL/ GRADE	DIAMETER (inches)	OR WALL THICKNESS	IF ANY (Inches)	Ft.	to	Ft.	CE- MENT (エ)	BEN- TONITE (上)	3 I	FILTER PACK (TYPE/SIZE)	
0	50	32		Ж	STEEL	.250	STAINLE	SS ,040	9	 	650	XX				
0	<i>6</i> 70	22	X.		STEEL	.250	STAINLE	ss	650	i	840		•	XX	8X16	
670	730	22		X	STEEL	-250	STATULE	SS ,040	L.	t !					_	
736	785	22	X		STEEL	.250	STAINLE	53		:						
785	905	22		14	STEEL	250	STAINLE	SS .040		- '						
805	825	32	У		STEEL	.250	STAINLE	ss	L	į					_	

805 825 22 X	STEEL .250 STAINLESS
ATTACHMENTS (∠)	CERTIFICATION STATEMENT
Geologic Log	I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief
Well Construction Diagram	NAME MAGGIORA BROS. DRILLING, INC.
Geophysical Log(s)	(PERSON, FIRM, OR CORPORATION) (TYPED OR PRINTED)
Soil/Water Chamical Analyses	595 AIRPORT BLVD. WATSONVILLE, CA 95076

ADDRESS _ Other . Signed ATTACH ADDITIONAL INFORMATION, IF IT EXISTS, WELL DRILLER/AUTHORIZED REPRESENTATIVE

249957 11/14/97

C-57 LICENSE NUMBER

DATE SIGNED

Appendix A. Summary of Lithology Recorded on Cross-Section Well Logs Hydrogeologic Investigation of the Salinas Valley Basin in the Vicinity of Fort Ord and Marina Monterey County Water Resources Agency

Cross-Section B-B' Well Names	Top (feet bgs)	Bottom (feet bgs)	Boring log record	GEOBASE Code
14S/2E-21N01	438	498	sand and gravel (pea to 1") clay at top-streaks	snd/grvl/cly
14S/2E-21N01	498	510	yellow brown clay	yellow clay
14S/2E-21N01	510	534	sand and gravel (1-3" rocks)	gravel/sand
14S/2E-21N01	534	564	sand	sand
14S/2E-21N01	564	580	sand and gravel (1-4" rocks)	gravel/sand
14S/2E-21N01	580	596	red sand	red sand
14S/2E-21N01	596	600	red sandstone	red sand
14S/2E-21E01	0	128	yellow dry sand	yellow sand
14S/2E-21E01	128	130	yellow clay w/streaks of red	yellow clay
14S/2E-21E01	130	144	blue clay - hard	blue clay
14S/2E-21E01	144	156	hard yellow clay	yellow clay
14S/2E-21E01	156	180	fine yellow clay	yellow sand
14S/2E-21E01	180	188	blue clay	blue clay
14S/2E-21E01	188	196	blue sand	blue sand
14S/2E-21E01	196	218	coarse sand w/some gravel	gravel/sand
14S/2E-21E01	218	242	brown sand - fine/some gravel	gravel/sand
14S/2E-21E01	242	272	hard yellow clay w/some sand	sandy clay
14S/2E-21E01	272	280	sand w/some rock	gravel/sand
14S/2E-21E01	280	396	sand/gravel rock (3-6")	gravel/sand
14S/2E-21E01	396	408	yellow clay	yellow clay
14S/2E-21E01	408	428	sand and some gravel	gravel/sand
14S/2E-21E01	428	442	sand and heavy gravel/rock (1-3")	gravel/sand
14S/2E-21E01	442	450	sand and heavy gravel/clay streaks	snd/grvl/cly
14S/2E-21E01	450	456	sand and gravel (1-3")	gravel/sand
14S/2E-21E01	456	460	yellow clay	yellow clay
14S/2E-21E01	460	466	sand	sand
14S/2E-21E01	466	470	yellow clay	yellow clay
14S/2E-21E01	470	484	fine sand and some gravel	gravel/sand
14S/2E-21E01	484	492	coarse sand and heavy gravel	gravel/sand
14S/2E-21E01	492	508	coarse sand and some gravel	gravel/sand
14S/2E-21E01	508	514	hard yellow clay	yellow clay
14S/2E-21E01	514	518	white sandstone w/yellow clay	sandy clay
14S/2E-21E01	514	532	fine sand	fine sand
14S/2E-21E01	532	542	coarse sand and gravel/rocks (1-4")	gravel/sand
14S/2E-21E01	542	550	sandy clay	sandy clay
14S/2E-21E01	550	562	sand and gravel w/clay streaks	gravel/sand
14S/2E-21E01	562	576	sand and heavy gravel	gravel/sand
14S/2E-21E01	576	592	fine sand	fine sand
14S/2E-21E01 14S/2E-21E01	592	612		gravel/sand
14S/2E-21E01 14S/2E-21E01			sand and gravel (1-5" rock)	_
	612	614	red sandstone	red sand
14S/2E-21F02	0	8	top soil sediment	topsoil
14S/2E-21F02	8	65		sediment
14S/2E-21F02	65	90	blue sandy clay	blue clay
14S/2E-21F02	90	116	yellow clay	yellow clay
14S/2E-21F02	116	130	mucky sand	sand
14S/2E-21F02	130	134	sandy yellow clay	yellow clay
14S/2E-21F02	134	140	river gravel	gravel
14S/2E-21F02	140	166	yellow clay	yellow clay
14S/2E-21F02	166	186	sand and gravel	gravel/sand
14S/2E-21F02	186	194	sand and fine gravel	gravel/sand
14S/2E-21F02	194	263	heavy gravel	gravel

Appendix A. Summary of Lithology Recorded on Cross-Section Well Logs Hydrogeologic Investigation of the Salinas Valley Basin in the Vicinity of Fort Ord and Marina Monterey County Water Resources Agency

Cross-Section B-B' Well Names	Top (feet bgs)	Bottom (feet bgs)	Boring log record	GEOBASE Code
14S/2E-21F02	263	277	red sand	red sand
14S/2E-21F02	277	280	yellow clay	yellow clay
14S/2E-21F02	280	297	gravel and yellow clay	gravelly clay
14S/2E-21F02	297	300	yellow clay	yellow clay
14S/2E-16G01	0	100	clay	clay
14S/2E-16G01	100	170	coarse sand	coarse sand
14S/2E-16G01	170	220	gravel	gravel
14S/2E-16G01	220	230	gravel/brown clay	gravelly clay
14S/2E-16G01	230	240	gravel/clay	gravelly clay
14S/2E-16G01	240	260	coarse sand/clay	sandy clay
14S/2E-16G01	260	360	clay/sand	sandy clay
14S/2E-16G01	360	370	sand/clay	sandy clay
14S/2E-16G01	370	420	coarse sand	coarse sand
14S/2E-16G01	420	440	clay/sand	sandy clay
14S/2E-16G01	440	470	coarse sand	coarse sand
14S/2E-16G01	470	490	sand/clay	sandy clay
14S/2E-16G01	490	520	sand/clay	sandy clay
14S/2E-16G01	520	540	clay	clay
14S/2E-16G01	540	570	sand	sand
14S/2E-16G01	570	610	coarse sand	coarse sand
14S/2E-16G01	610	630	sand/clay	sandy clay
14S/2E-09D04	0	150	brown clay	brown clay
14S/2E-09D04	150	180	coarse sand	coarse sand
14S/2E-09D04	180	220	coarse sand/gravel	gravel/sand
14S/2E-09D04	220	230	clay/gravel	gravelly clay
14S/2E-09D04	230	260	silt stone/clay	clay
14S/2E-09D04	260	270	clay	clay
14S/2E-09D04	270	280	coarse sand/clay	sandy clay
14S/2E-09D04	280	330	clay	clay
14S/2E-09D04	330	420	sand/clay	sandy clay
14S/2E-09D04	420	430	coarse sand/clay	sandy clay
14S/2E-09D04	430	440	coarse sand	coarse sand
14S/2E-09D04	440	460	coarse sand/clay	sandy clay
14S/2E-09D04	460	490	coars sand	coarse sand
14S/2E-09D04	490	500	coarse sand/clay	sandy clay
14S/2E-09D04	500	540	sand/clay	sandy clay
14S/2E-09D04	540	550	hard clay	clay
14S/2E-09D04	550	570	hard clay/sand	sandy clay
14S/2E-09D04	570	580	coarse sand	coarse sand
14S/2E-09D04	580	610	coarse sand/clay	sandy clay
14S/2E-09D04	610	630	clay/sand	sandy clay

Notes:

^{*} a partial boring log description is provided for this well

CONTROL BOARD No. 3

WATER WELL DRILLERS REPORT

751

Do Not Fill In

(Sections 7076, 7077, 7071, Water Code)

STATE OF CALIFORNIA

	1	2	2	
	2	2	7	101
人	×	()	6	

1	State Well No
	Other Well No. 14/2 - 21F
	1 = 7-1

OWNER:	10-14 =
	(11) WELL LOG:
Mrs. A. Warcken Address Pomber Street	Total depth 300 ft. Depth of completed well 300
	Formation: Describe by color, observeder, size of material, and structure. Oft. to 2 ft. Ton 3017
Castroville, California	Office 2 fc Top soil 2 " 65 " Sediment
(2) LOCATION OF WELL:	65 90 Blue sandy clay
County Monterey Owner's number, if any-	90 " 116 " Yellow clay
R. F. D. or Street No.	116 " 130 " Mucky sand
On Bres B	130 " 134 " Sandy yellow clay
On Breschini Ranch 22 Mi. E. SE of	134 " 140 " River grayel
Twin Bridges & State Highway 1.	140 166 Yellow clay
50 ft. NE of old well # 46 cm Map	166186 Sand & gravel
(3) TYPE OF WORK (check):	186 194 Sand & fine gravel
New well Deepening Reconditioning Abandon	194 263 Heavy gravel 264 277 Red sand
If abandonment, describe material and procedure in Item 11.	277 " 280 " Yellow clay
(4) PROPOSED USE (check): (5) EQUIPMENT:	280 " 297 " Gravel & yellow clay
Domestic Industrial Municipal Rotary	297 " 300 " Yallow clay
Imparion Test Well Other Cable	" " " " " " " " " " " " " " " " " " " "
Dug Well	" "
O(6) CASING INSTALLED: If gravel packed	
-SINGLE T DOUBLE T	
reFrom ft. to ft. Diam. Wall of Bore ft. ft.	
≥ ·· 0 ·· 300 ·· 12 ·· 12 ·· · · · ·	
	" "
<u>C</u>	n
O vpc and size of shoe or well ring Size of gravel:	
Describe joint	
(7) PERFORATIONS:	
Type of perforator used Mills	, ,
Size of perforations 31 in., length, by in.	
From ft. to ft. Perf. per row Rows per ft.	
<u> 200 261 6 """ 1 """</u>	
# # # # # # # # # # # # # # # # # # #	" "
	0 0
(8) CONSTRUCTION:	
Was a surface sanitary seal provided? Yes No To what depth ft.	, e1
Vere any strate sealed against pollution? Yes No If yes, note depth of strate	in in
From	
ft. to ft.	*
Method of Sealing	
(9) WATER LEVELS:	WELL DRILLER'S STATEMENT: This well was drilled under my jurisdiction and this report is true to the best
Depth at which water was first found ft.	my knowledge and belief.
Standing level before perforating ft.	NAME BOY V. Alson & Son
erel after perforating ft.	NAME ROY V. Alson & Son (Typed or primited)
WELL TESTS:	Address 1508 Abbott Street
	Salines, California
Was a pump test made? ☐ Yes ☐ No. If yes, by whom? Yield: gal./min. with ft. draw down after hrs.	[SIGNED] ACCOUNTY
Temperature of water Was a chemical analysis model Yes No	License No. 132870 Dated: Octobe 28 19 56
	12
Was electric log made of well? Yes No AZ	TI SEET 1-34 TH OUIX TO BPC DWR FORM NO. 246 (REY. 3-1

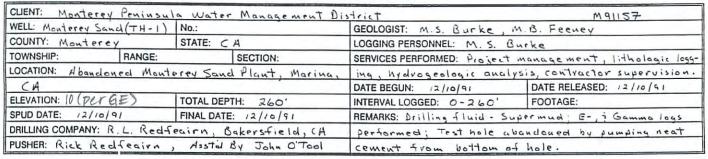
STAAL, GARDNER & DUNNE, INC.

Consulting Engineers and Geologists 5855 Olivas Park Drive • Ventura, California 93003-7672

TH- (

SGD

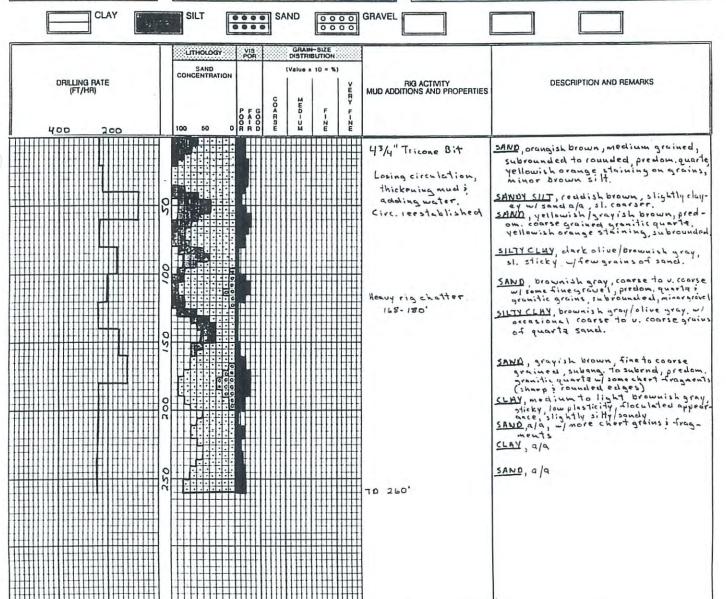
DRILLING LOG



0 - 260	4.3/4"

SPACE NA	CASING RE	CORD to the section

SHOW AND AND AND AND ADDRESS OF THE PARTY AND	BREVIATIO	JN5
CIRCULATE OUT	PR	POOR RETURNS
LOGGED AFTER TRIP	SC	SAND CONTENT (%)
NEW BIT	VIS	VISCOSITY (SECONDS)
NEW CORE BIT	WL	WATER LOSS (CC/30 MIN)
NO RETURN	WT	FLUID WEIGHT (LBS/CU.FT.)
	CIRCULATE OUT LOGGED AFTER TRIP NEW BIT NEW CORE BIT	CIRCULATE OUT PR LOGGED AFTER TRIP SC NEW BIT VS NEW CORE BIT WL



STAAL, GARDNER & DUNNE, INC.

Consulting Engineers and Geologists
5855 Olivas Park Drive • Ventura, California 93003-7672

TH-2

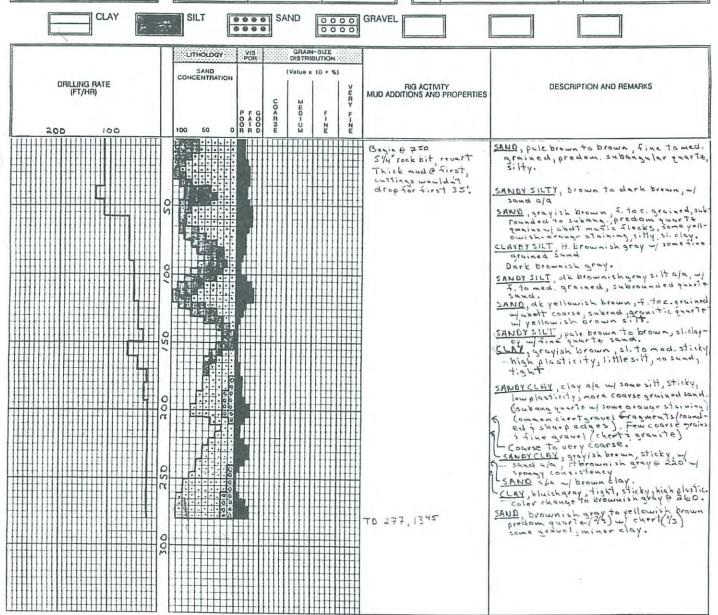
DRILLING LOG

CLIENT: Monterey Peninsul	a Water Management Dist	rict	M91157
WELL: Regional Park (TH-2)		GEOLOGIST: M. S. Burke,	
COUNTY: Wonterey	STATE: CA	LOGGING PERSONNEL: M. S. Buck	
TOWNSHIP: RANGE:	SECTION:	SERVICES PERFORMED: Project Me	anagement, lithologic logging.
LOCATION: Regional Park Di	strict, Marina, CH. Edge	hydrogeologic consultation	n, contractor observation.
of bluff at and of road	starting at and of Dune Ur.	DATE BEGUN: 12/18/91	DATE RELEASED: /2//8/91
ELEVATION: 19 ft (DEFGE)		INTERVAL LOGGED: 0 - 277'	FOOTAGE: 277'
SPUD DATE: 12/18/91		REMARKS: Drilling fluid - Rever	T E- i Gamma logs perform-
DRILLING COMPANY: Pitcher D		ed, test hole abandoned	
PUSHER: Wayne Baker, Ga	rry Foppiono (usst)		

0 - 277'	5.1/4"
2 477	- /-

HISTORISTS	CASING R	ECORD
	_	
	_	

ABBREVIATIONS				
PR	POOR RETURNS			
SC	SAND CONTENT (%)			
VIS	VISCOSITY (SECONDS)			
WL	WATER LOSS (CC/30 MIN)			
WT	FLUID WEIGHT (LBS/CU.FT.)			
	PR SC VIS WL			



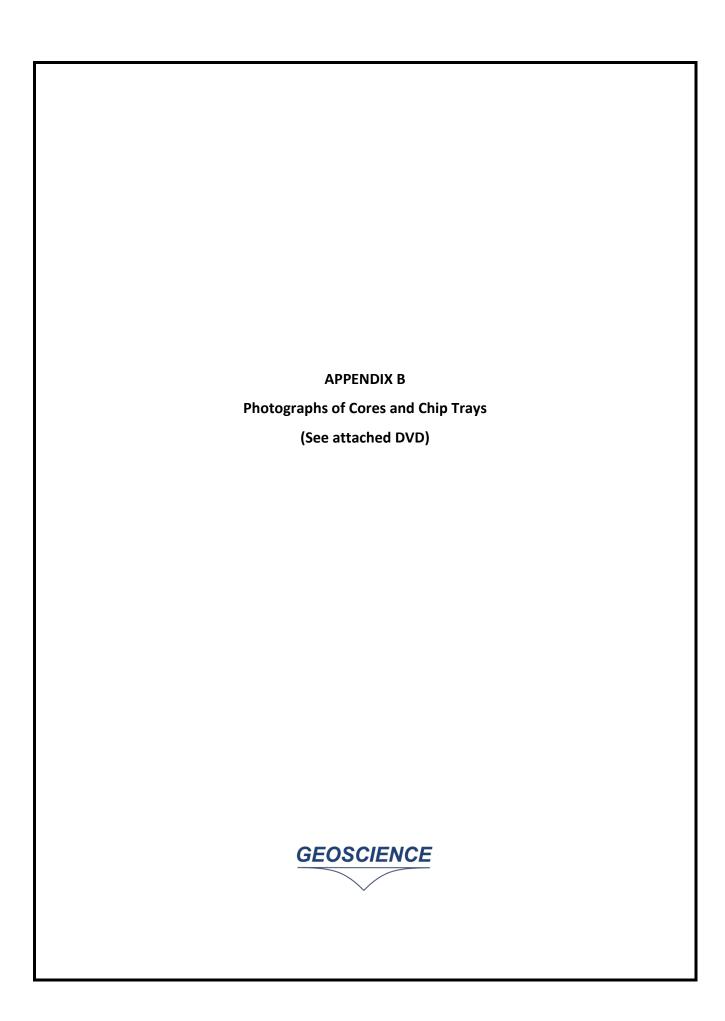
STAAL, GARDNER & DUNNE, INC.
Consulting Engineers and Geologists
5855 Olivas Park Drive • Ventura, California 93003-7672

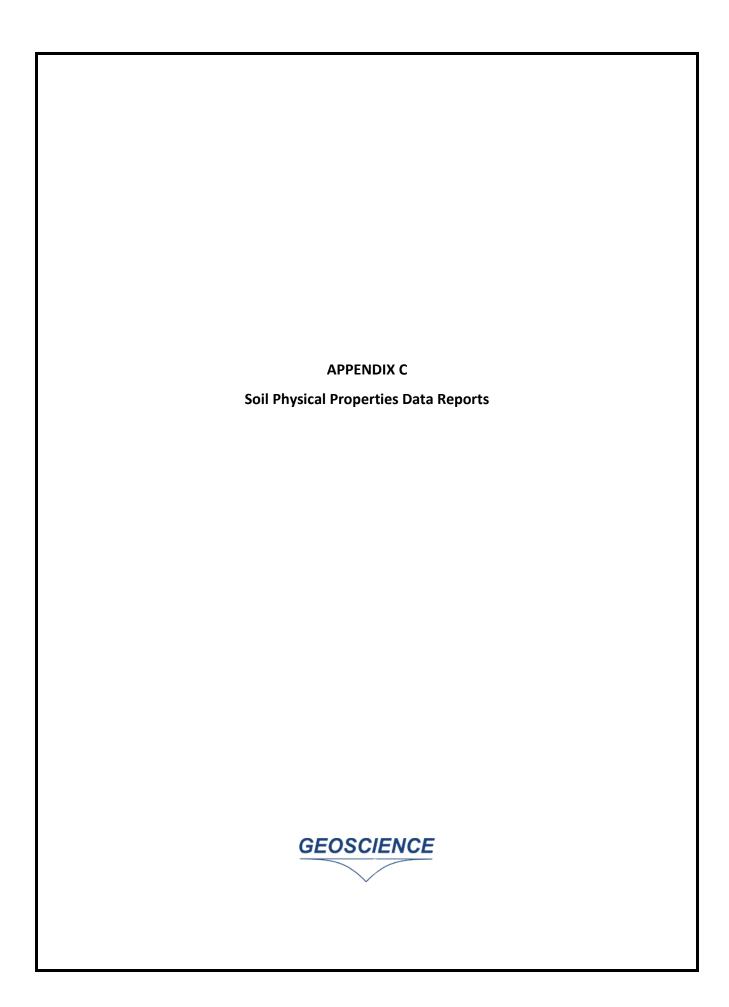
SGD

DRILLING LOG

WFII: 6 +- B + / /-	nsula Water Management Dist.	7161	W41127	
WELL: Granite Rock (o. (TH-3) No.:		GEOLOGIST: M.S. Burke, M.	B. Feeney	
COUNTY: Monterey STATE: CA		LOGGING PERSONNEL: M. S. Burke		
TOWNSHIP: RANG		SERVICES PERSONATE. ()		
LOCATION: On the beach at the Granite Rock Co. property		hydrogeologic consultation, contractor supervision.		
in Marina, CH		DATE BEGUN: /2//9/		
ELEVATION: 7 CA (Der G		INTERVAL LOGGED: 0- 250'		
SPUD DATE: 12/19/91 FINAL DATE: 12/19/91		REMARKS: Drilling fluid - Revert E & Gamma logs		
DRILLING COMPANY: Pitcher Drilling, Pala Alto, CH.		performed test hole abandoned w/ neat cement.		
PUSHER: Wayne Baker.	usstid by Garry Foppiono			

SPUD DATE: 12/19/91	FINAL DATE: /2/19/91		ling fluid - Rever		: 6
DRILLING COMPANY: 17 Heher	Drilling Polo Alto CH				3 Gamma logs
PUSHER: Wayne Rabas	בילו איני ל	per-ormed.	test hole abando	ined u	, neat cement.
COLUMN COLUMN BARRY	usstid by Garry Foppiono				
HOLE SIZE	CASING RECORD	19 19 19 19 19 19 19 19 19 19 19 19 19 1	ABE	REVIATI	ONS
0-250' 514"		СО	CIRCULATE OUT	PR	
		LAT	LOGGED AFTER TRIP	SC	POOR RETURNS SAND CONTENT (%)
		NB	NEW BIT	VIS	VISCOSITY (SECONDS)
		NCB	NEW CORE BIT	WL	WATER LOSS (CC/30 MIN)
		NR.	NO RETURN	WT	FLUID WEIGHT (LBS/CU.FT.)
		1111	HO NETONA		PEOID WEIGHT (EB3/CO.11.)
CLAY	SILT SAND 0000	GRAVEL T		1	
	0000	5		- 1	
The state of the s	CONTROL CONTRO				
	LITHOLOGY VIS GRAIN-SIZE POR DISTRIBUTION	8			
	SAND (Value x 10 = %)				
DRILLING RATE	SOMETIMENT V	RIG ACTI	VITY	DESCRIF	TION AND REMARKS
(FT/HR)	G M R	MUD ADDITIONS AND	D PROPERTIES		
	PEG A D E E				
400 200	PFG A D F F F F F F F F F F F F F F F F F F	2			
441141111111111111111111111111111111111	CONTROL ME		4000		
**** ******* * ** *	111111111111111111111111111111111111111	HI Begin drilling	6 822 NAD De	ma, + 14	e to course gr., predom, m
		al grad p.	many b	rown / al	unded, predom, quarts wi ive gray grains, silty.
#######################################	0000000	H			Siay Siaine, Elity.
<u> </u>		+++	SAND brow	unis Las	av ala thank conseque
		##	granit	ic sour	ay, ala, though courser greet for quarte, less silt, so
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		##	CLAYEY SI	LT .	4 1-1-1
 		wiper run , 11	30- 1200 8045.	51. 39	gray to dark alive gray, mi
		"mud rings"	forming		-1
	O IN LUDGE	in bore hole			
		H	SAND, fin	e to coar	se grained though predom .
	* ; conductor	#			
		Щ			of winas (borsiers c rest de
		Ш	CLAY NI	ish ara	to elive gray, moderatel
		 	+ight.	stick	silty.
<u> </u>		Ш			ss sitt.
		H .	SAUD :	Dall'	Live to cooke grained
	11000	Change to roc	k bit suban	aniar t	, Line to coarse grained, o subrounded, predom que
 		Ħ	w/ about	Taruin	SOT CHPFT, COMMON CHPF
		<u>##</u>			ul sharp i rounded edges
		Н	CLAY, oli	vetool	ive gray, sticky, low plasti
		HH .	siltys	st. Sane	dy.
<u> </u>		H	Tielder	. 1000	ult ; sand.
<u>+++++++++++++++++++++++++++++++++++++</u>		111	1134161	1	
		##	CHAIN	,	
#######################################		#1	SAND, a	10	
	<u> </u>	TO 250', 1	450		4
	n	H 10 230) 1	CLAY) ali	ve brown	nto grayish brown, stick
		Ħ	+15/-	' nest !	ttle sand or silt
+++++++++++++++++++++++++++++++++++++++		#1			
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<u>#####################################</u>		Ħ		0.0	
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APPENDIX C:

SOIL PHYSICAL PROPERTIES DATA REPORTS

CONTENTS

Description	Page
Cover Letter (October 14, 2013)	C-1
Cover Letter (March 5, 2014)	C-2
Soil Physical Properties Data Reports	C-3
Chain of Custody Records	C-10





8100 Secura Way • Santa Fe Springs, CA 90670 Telephone (562) 347-2500 • Fax (562) 907-3610

October 14, 2013

Brian Villalobos Geoscience Support Services P.O. Box 220 Claremont, CA 91711

Re: PTS File No: 43626

Physical Properties Data MPWSP; 13017-13

Dear Mr. Villalobos:

Please find enclosed report for Physical Properties analyses conducted upon samples received from your MPWSP; 13017-13 project. All analyses were performed by applicable ASTM, EPA, or API methodologies. An electronic version of the report has previously been sent to your attention via the internet. The samples are currently in storage and will be retained for thirty days past completion of testing at no charge. Please note that the samples will be disposed of at that time. You may contact me regarding storage, disposal, or return of the samples.

PTS Laboratories appreciates the opportunity to be of service. If you have any questions or require additional information, please contact Rachel Spitz at (562) 347-2504.

Sincerely,

PTS Laboratories, Inc.

Michael Mark Brady, P.G.

District Manager

Encl.



8100 Secura Way • Santa Fe Springs, CA 90670 Telephone (562) 347-2500 • Fax (562) 907-3610

March 5, 2014

Brian Villalobos Geoscience Support Services P.O. Box 220 Claremont, CA 91711

Re:

PTS File No: 44073 Physical Properties Data

MPWSP; 13017-13

Dear Mr. Villalobos:

Please find enclosed report for Physical Properties analyses conducted upon samples received from your MPWSP; 13017-13 project. All analyses were performed by applicable ASTM, EPA, or API methodologies. An electronic version of the report has previously been sent to your attention via the internet. The samples are currently in storage and will be retained for thirty days past completion of testing at no charge. Please note that the samples will be disposed of at that time. You may contact me regarding storage, disposal, or return of the samples.

PTS Laboratories Inc. appreciates the opportunity to be of service. If you have any questions or require additional information, please contact Morgan Richards at (562) 347-2509.

Sincerely,

PTS Laboratories, Inc.

Michael Mark Brady, P.G.

District Manager

Encl.



8100 Secura Way • Santa Fe Springs, CA 90670 Telephone (562) 347-2500 • Fax (562) 907-3610

March 13, 2014

Brian Villalobos Geoscience Support Services P.O. Box 220 Claremont, CA 91711

Re:

PTS File No: 44073

Revised Physical Properties Data Rev.01

MPWSP; 13017-13

Dear Mr. Villalobos:

Please find enclosed revised report for Physical Properties analyses conducted upon samples received from your MPWSP; 13017-13 project. The report has been revised to correct a unit calculation error for horizontal Hydraulic Conductivity for sample ML-4 146.5-147 at 146.95. All analyses were performed by applicable ASTM, EPA, or API methodologies. An electronic version of the report has previously been sent to your attention via the internet. The samples are currently in storage and will be retained for thirty days past completion of testing at no charge. Please note that the samples will be disposed of at that time. You may contact me regarding storage, disposal, or return of the samples.

PTS Laboratories Inc. appreciates the opportunity to be of service. If you have any questions or require additional information, please contact Morgan Richards at (562) 347-2509.

Sincerely,

PTS Laboratories, Inc.

Michael Mark Brady, P.G.

District Manager

Encl.

Project Name: MPWSP PTS File No: 44073

Project Number: 13017-13 Client: Geoscience Support Services

TEST PROGRAM - 20140206

CORE ID	Depth ft.	Core Recovery ft.	Hydraulic Conductivity Pkg.	Hydraulic Conductivity API RP40/EPA 9100	Notes
Date Received: 20140204		Plugs:	Vert. 1"	Horz. 1"	
CX-B1 66.5-67	66.5-67	0.50	Х	Х	
CX-B1 166.5-167.0	166.5- 167.0	0.50	Х	Х	
CX-B1 257.5-258	257.5-258	0.50	Х		
CX-B2 207.5-208	207.5-208	0.50	Х	Х	
CX-B2 259-259.5	259-259.5	0.50	X		
CX-B3 107.5-108	107.5-108	0.50	X	Х	
CX-B3 129-129.5	129-129.5	0.50	X		
CX-B3 177.5-178	177.5-178	0.50			
CX-B3 197.5-198	197.5-198	0.50	X	Х	
ML-1 76-76.5	76-76.5	0.50	X		
ML-1 107.5-108	107.5-108	0.50	X	Х	
ML-1 147-147.5	147-147.5	0.50	X		
ML-2 87-87.5	87-87.5	0.50	Х		
ML-2 117.5-118	117.5-118	0.50	Х	Х	
ML-2 157.5-158	157.5-158	0.50	Х	Х	
ML-3 106.5-107	106.5-107	0.50	Х	Х	
ML-3 166.5-167	166.5-167	0.50	Х	Х	
ML-4 76.5-77	76.5-77	0.50	Х	Х	
ML-4 126.5-127	126.5-127	0.50	X		
ML-4 146.5-147	146.5-147	0.50	Х	х	
ML-6 79.5-80	79.5-80	0.50	X		
ML-6 107.5-108	107.5-108	0.50	X	X	
ML-6 167-168.5	167-168.5	0.50	Х	Х	
TOTALS:	23 cores	11.50	22	14	23

Project Number: 13017-13 Client: Geoscience Support Services

TEST PROGRAM - 20140206

		Core	Hydraulic	Hydraulic	
CORE ID	Depth	Recovery	Conductivity	Conductivity	
	ft.	ft.	Pkg.	API RP40/EPA 9100	Notes
		Plugs:	Vert. 1"	Horz. 1"	

Laboratory Test Program Notes

Contaminant identification: NONE

Standard TAT for basic analysis is 10 business days.

Hydraulic Conductivity Package – Saturated Zone: Native-state permeability to water, total and air-filled porosity, grain and bulk density, moisture content, total pore fluid (water only) saturation.

PTS File No: 44073

Client: Geoscience Support Services

Report Date: 03/05/14

PHYSICAL PROPERTIES DATA - HYDRAULIC CONDUCTIVITY PACKAGE

Project Name: MPWSP Project No: 13017-13

API RP 40	API	RP 40	API RP 40	API RP 40; EPA 9100			
7			74114 40	25 PSI CONFINING			
DENSITY	POROSI	TY, %Vb (2)	TOTAL PORE FLUID	EFFECTIVE (4,5)	HYDRAULIC		
	TOTAL	AIR-FILLED	SATURATIONS (3),	PERMEABILITY TO WATER,	CONDUCTIVITY (4,5),		
cc g/cc			% Pv	millidarcy	cm/s		
46 2.66	45.0	11.6	74.2	273	2.76E-04		
	43.8				4.87E-04		
11 2.61	57.7			1.75	1.75E-06		
	44.6		71.1		3.76E-03		
	49.3		83.9		1.85E-06		
43 2.64	45.8		64.2	5210	5.26E-03		
25 2.62	52.1	7.6	85.5	2.83	2.86E-06		
66 2.69	38.2	8.1	78.8	101	1.00E-04		
17 2.67	56.1	6.3	88.7	4.89	4.83E-06		
53 2.65	42.1	19.0	54.8	8540	8.52E-03		
31 2.66	50.8	8.4	83.4	1.97	1.98E-06		
50 2.66	43.4	12.7	70.8	101	1.00E-04		
43 2.64	45.8	11.0	76.0	47.3	4.70E-05		
52 2.61	41.6	12.3	70.5	110	1.10E-04		
53 2.64	42.0	22.3	47.0	1900	1.87E-03		
31 2.65	50.7	13.2	73.9	9.6	9.51E-06		
41 2.62	46.3	16.2	65.1	954	9.49E-04		
44 2.64	45.5	9.5	79.1	1.18	1.18E-06		
45 2.61	44.3	23.8	46.3	6180	6.10E-03		
33 2.64	49.7	6.9	86.0	2.43	2.43E-06		
41 2.64	46.3	25.2	45.6	4710	4.65E-03		
38 2.62	47.4	12.1	74.3	72.6	7.23E-05		
	BULK, GRAIN, g/cc 46 2.66 58 2.82 11 2.61 48 2.67 33 2.63 43 2.64 25 2.62 66 2.69 17 2.67 53 2.65 31 2.66 50 2.66 43 2.64 52 2.61 53 2.64 41 2.62 44 2.64 45 2.61 33 2.64 41 2.64	DENSITY POROSI BULK, GRAIN, g/cc TOTAL 46 2.66 45.0 58 2.82 43.8 11 2.61 57.7 48 2.67 44.6 33 2.63 49.3 43 2.64 45.8 25 2.62 52.1 66 2.69 38.2 17 2.67 56.1 53 2.65 42.1 31 2.66 50.8 50 2.66 43.4 43 2.64 45.8 50 2.66 43.4 43 2.64 45.8 50 2.66 43.4 44 2.64 45.5 41 2.62 46.3 44 2.64 45.5 44 2.64 45.5 45 2.61 44.3 33 2.64 49.7 41 2.64 46.3	DENSITY POROSITY, %Vb (2) BULK, cc GRAIN, g/cc TOTAL AIR-FILLED 46 2.66 45.0 11.6 58 2.82 43.8 4.7 11 2.61 57.7 12.2 48 2.67 44.6 12.9 33 2.63 49.3 7.9 43 2.64 45.8 16.4 25 2.62 52.1 7.6 66 2.69 38.2 8.1 17 2.67 56.1 6.3 53 2.65 42.1 19.0 31 2.66 50.8 8.4 50 2.66 43.4 12.7 43 2.64 45.8 11.0 52 2.61 41.6 12.3 53 2.64 45.8 11.0 52 2.61 41.6 12.3 53 2.64 45.8 11.0 52 2.61 <t< td=""><td>DENSITY POROSITY, %Vb (2) TOTAL PORE FLUID SATURATIONS (3), % Pv 46 2.66 45.0 11.6 74.2 58 2.82 43.8 4.7 89.3 11 2.61 57.7 12.2 78.8 48 2.67 44.6 12.9 71.1 33 2.63 49.3 7.9 83.9 43 2.64 45.8 16.4 64.2 25 2.62 52.1 7.6 85.5 66 2.69 38.2 8.1 78.8 17 2.67 56.1 6.3 88.7 53 2.65 42.1 19.0 54.8 31 2.66 50.8 8.4 83.4 50 2.66 43.4 12.7 70.8 43 2.64 45.8 11.0 76.0 52 2.61 41.6 12.3 70.5 53 2.64 45.8 11.0 76.0</td><td> DENSITY POROSITY, %Vb (2) TOTAL PORE FLUID SATURATIONS (3), % Pv PRMEABILITY TO WATER, millidarcy </td></t<>	DENSITY POROSITY, %Vb (2) TOTAL PORE FLUID SATURATIONS (3), % Pv 46 2.66 45.0 11.6 74.2 58 2.82 43.8 4.7 89.3 11 2.61 57.7 12.2 78.8 48 2.67 44.6 12.9 71.1 33 2.63 49.3 7.9 83.9 43 2.64 45.8 16.4 64.2 25 2.62 52.1 7.6 85.5 66 2.69 38.2 8.1 78.8 17 2.67 56.1 6.3 88.7 53 2.65 42.1 19.0 54.8 31 2.66 50.8 8.4 83.4 50 2.66 43.4 12.7 70.8 43 2.64 45.8 11.0 76.0 52 2.61 41.6 12.3 70.5 53 2.64 45.8 11.0 76.0	DENSITY POROSITY, %Vb (2) TOTAL PORE FLUID SATURATIONS (3), % Pv PRMEABILITY TO WATER, millidarcy		

⁽¹⁾ Sample Orientation: H = horizontal; V = vertical; R = remold

Water = filtered Laboratory Fresh (tap) or Site water.

⁽²⁾ Total Porosity = all interconnected pore channels; Air Filled = pore channels not occupied by pore fluids.

⁽³⁾ Fluid density used to calculate pore fluid saturations: Water = 0.9996 g/cc.

⁽⁴⁾ Effective (Native) = With as-received pore fluids in place.

⁽⁵⁾ Permeability to water and hydraulic conductivity measured at saturated conditions.

Vb = Bulk Volume, cc; Pv = Pore Volume, cc; ND = Not Detected

PTS Laboratories

PTS File No: 44073

Client: Geoscience Support Services

Report Date: 03/13/14

PHYSICAL PROPERTIES DATA - HYDRAULIC CONDUCTIVITY Rev.01

(Methodology: API RP 40; EPA 9100)

Project Name: MPWSP Project No: 13017-13

				25 PSI CONFINING STRESS									
	_	<u> </u>		EFFECTIVE		INTRINSIC							
		SAMPLE		PERMEABILITY	HYDRAULIC	PERMEABILITY							
SAMPLE	DEPTH,	ORIENTATION	ANALYSIS	TO WATER (2,3),	CONDUCTIVITY (3),	TO WATER (3),							
ID.	ft.	(1)	DATE	millidarcy	cm/s	cm ²							
CX-B1 66.5-67	66.95	Н	20140305	1560	1.53E-03	1.54E-08							
CX-B1 166.5-167.0	466.95	Н	20140305	622	6.10E-04	6.14E-09							
CX-B2 207.5-208	207.95	Н	20140305	1440	1.41E-03	1.42E-08							
CX-B3 107.5-108	107.95	Н	20140305	5200	5.12E-03	5.13E-08							
CX-B3 197.5-198	197.95	Н	20140305	644	6.34E-04	6.35E-09							
ML-1 107.5-108	107.95	Н	20140305	6330	6.26E-03	6.25E-08							
ML-2 117.5-118	117.95	Н	20140305	111	1.10E-04	1.10E-09							
ML-2 157.5-158	157.95	Н	20140305	3270	3.21E-03	3.23E-08							
ML-3 106.5-107	106.95	Н	20140305	851	8.42E-04	8.40E-09							
ML-3 166.5-167	166.95	Н	20140305	7.59	7.53E-06	7.49E-11							
ML-4 76.5-77	76.95	Н	20140305	873	8.68E-04	8.62E-09							
ML-4 146.5-147	146.95	Н	20140305	12900	1.29E-02	1.28E-07							
ML-6 107.5-108	107.95	Н	20140305	3990	4.00E-03	3.94E-08							
ML-6 167-168.5	167.95	Н	20140305	130	1.30E-04	1.28E-09							

⁽¹⁾ Sample Orientation: H = horizontal; V = vertical; R = remold

⁽²⁾ Effective (Native) = With as-received pore fluids in place.

⁽³⁾ Permeability to water and hydraulic conductivity measured at saturated conditions. Water = filtered Laboratory Fresh (tap) or Site water.

Project Number: 13017-13 Client: Geoscience Support Services

TEST PROGRAM - 20131002

CORE ID	Depth ft.	Core Recovery ft.	Hydraulic Conductivity Pkg.	Hydraulic Conductivity API RP40/EPA 9100	Notes
		Plugs:	Vert. 1"	Horz. 1"	
Date Received: 20130926					
PR-1 67 ft - 67.5 ft	67-67.5	0.50	X	X	
PR-1 145.5 ft - 146 ft	145.5-146	0.50	X		
PR-1 152 ft - 152.5 ft	152-152.5	0.50	Х		
PR-1 200.5 ft - 201 ft	200.5-201	0.50	X	Х	
TOTALS:	4 cores	2.00	4	2	4

Laboratory Test Program Notes

Contaminant identification:

Standard TAT for basic analysis is 10 business days.

Hydraulic Conductivity Package – Saturated Zone: Native-state permeability to water, total and air-filled porosity, grain and bulk density, moisture content, total pore fluid (water only) saturation.

PTS File No: 43626

Client: Geoscience Support Services

Report Date: 10/14/13

PHYSICAL PROPERTIES DATA - HYDRAULIC CONDUCTIVITY PACKAGE

Project Name: MPWSP Project No: 13017-13

API RP 40 /

		METHODS:	ASTM D2216	API RI	P 40	AP	I RP 40	API RP 40	API RP 40; EPA 9100						
									25 PSI CONFINING	STRESS					
		SAMPLE	MOISTURE	DENS	ITY	POROS	ITY, %Vb (2)	TOTAL PORE FLUID	EFFECTIVE (4,5)	HYDRAULIC					
SAMPLE	DEPTH,	ORIENTATION	CONTENT,	DRY BULK,	GRAIN,	TOTAL	AIR-FILLED	SATURATIONS (3),	PERMEABILITY TO WATER,	CONDUCTIVITY (4,5),					
ID.	ft.	(1)	% weight	g/cc	g/cc	TOTAL	AII - ILLLD	% Pv	millidarcy	cm/s					
PR-1 67 ft - 67.5 ft	67.2	V	15.1	1.69	2.59	34.8	9.4	73.0	91.1	9.13E-05					
PR-1 145.5 ft - 146 ft	145.6	V	28.6	1.38	2.68	48.5	9.0	81.4	2.08	2.08E-06					
PR-1 152 ft - 152.5 ft	152.1	V	27.1	1.45	2.72	46.5	7.1	84.8	2.03	2.04E-06					
PR-1 200.5 ft - 201 ft	200.65	V	16.5	1.61	2.67	39.8	13.3	66.6	5120	5.10E-03					

Water = filtered Laboratory Fresh (tap) or Site water.

⁽¹⁾ Sample Orientation: H = horizontal; V = vertical; R = remold

⁽²⁾ Total Porosity = all interconnected pore channels; Air Filled = pore channels not occupied by pore fluids.

⁽³⁾ Fluid density used to calculate pore fluid saturations: Water = 0.9996 g/cc.

⁽⁴⁾ Effective (Native) = With as-received pore fluids in place.

⁽⁵⁾ Permeability to water and hydraulic conductivity measured at saturated conditions.

Vb = Bulk Volume, cc; Pv = Pore Volume, cc; ND = Not Detected

PTS Laboratories

PTS File No: 43626

Client: Geoscience Support Services

Report Date: 10/14/13

PHYSICAL PROPERTIES DATA - HYDRAULIC CONDUCTIVITY

(Methodology: API RP 40; EPA 9100)

Project Name: MPWSP Project No: 13017-13

				25 PSI CONFINING STRESS									
				EFFECTIVE		INTRINSIC							
		SAMPLE		PERMEABILITY	HYDRAULIC	PERMEABILITY							
SAMPLE	DEPTH,	ORIENTATION	ANALYSIS	TO WATER (2,3),	CONDUCTIVITY (3),	TO WATER (3),							
ID.	ft.	(1)	DATE	millidarcy	cm/s	cm ²							
PR-1 67 ft - 67.5 ft	67.05	Н	20131010	61.1	6.03E-05	6.03E-10							
PR-1 200.5 ft - 201 ft	200.55	Н	20131010	269	2.73E-04	2.65E-09							

⁽¹⁾ Sample Orientation: H = horizontal; V = vertical; R = remold

⁽²⁾ Effective (Native) = With as-received pore fluids in place.

⁽³⁾ Permeability to water and hydraulic conductivity measured at saturated conditions. Water = filtered Laboratory Fresh (tap) or Site water.

P	THE SERVICE OF THE SE	S	L	abo	ora	ator	ies.	Inc.
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COMPANY					***						A۱	۱A۱	_YS	SIS	RE	ΞQI	JE:	ST								PO# 13017-13
Geoscience Support Service			- Apple	┰														084								TURNAROUND TIME
ADDRESS PO 220	CITY Claremon	it, CA	ZIP CODE 91711													12937		² 40, D5	164M							24 HOURS 5 DAYS 648 HOURS 648 NORMAL 648
PROJECT MANAGER Brian Villalobos	bvillalob	os@geos	cience-water.com			GE	ЭE	岩						Σ		STM [API RF)422/4			ガジ				72 HOURS OTHER:
PROJECT NAME MPWSP			PHONE NUMBER 009-451-6650			PACKA	ACKA(ACKA		Ε	чарну	D2216		M D425	54	40 or 4		⊃A9100	ASTM [4318	45		.		SAMPLE INTEGRITY (CHECK):
PROJECT NUMBER 13017-13		9	FAX NUMBER 09-451-6638	ES	S PACKAGE	CONDUCTIVITY PACKAGE	PORE FLUID SATURATIONS PACKAGE	TCEQ/TNRCC PROPERTIES PACKAGE	\GE	FLUID PROPERTIES PACKAGE	РНОТОГОС: СОВЕ РНОТОСВАРНУ	MOISTURE CONTENT, ASTM D2216	POROSITY: TOTAL, API RP40	POROSITY: EFFECTIVE, ASTM D425M	SPECIFIC GRAVITY, ASTM D854	BULK DENSITY (DRY), API RP40 or ASTM D2937	AIR PERMEABILITY, API RP40	HYDRAULIC CONDUCTIVITY, EPA9100, API RP40, D5084	GRAIN SIZE DISTRIBUTION, ASTM D422/4464M	X	ATTERBERG LIMITS, ASTM D4318	Conductionty				NTACT \(ON ICE \(\) PTS QUOTE NO.
SITE LOCATION CEMEX				SAMPLES	TIES P	ONDU	SATUR,	PROP	PACK/	RTIES	ORE	ONTEN	JTAL, 4	-FECT	4VITY,	Y (DR)	3ILITY,	ONDOC	ISTRIE	Y-BLA	IMITS	प्र				PTS FILE:
SAMPLER SIGNATURE				R	ROPER	ULIC C	ירטום פ	NRCC	ARITY	PROPE	LOG: C	JRE CC	ITY: TC	ITY: EF	IC GR	ENSIT	RMEAE	ULIC CC	SIZED	ALKLE	BERG I	Harizonta				44073
SAMPLE ID NUMBER	DATE	TIME	DEPTH, FT	NUMBER	SOIL PROPERTIE	HYDRAULIC	PORE F	тсеа/т	CAPILLARITY PACKAGE	FLUID F	РНОТО	MOIST	POROS	POROS	SPECIF	BULK D	AIR PE	нүрва	GRAIN	TOC: WALKLEY-BLACK	ATTERI	Hari				COMMENTS
CX-B1 66.5-67	10/22/13	1500	66.5-67	Ţ		X																X				
CX-B1 166.5-167.0	10/23/13	1500	166.5-167	A		Х																X				
CX-B1 257.5-258	10/25/13	1500	257.5-258	-		X																X				2 inches of sample missing
CX-B2 207.5-208	11/5/13	1345	207.5-208	-control		χ																X				
CX-B2 259-259.5	11/6/13	1000	259-259.5			χ																Χ				
CX-B3 107.5-108	11/10/13	1500	107.5-108	7/00-04		X																X				
CX-B3 129-129.5	11/10/13	1500	129-129.5	"Street		χ																χ				
CX-B3 177.5-178	11/10/13	1500	177.5-178	1		X																Χ				
CX-B3 197.5-198	11/10/13	1500	197.5-198	45,000		X																X			_	
					<u></u>																					76°F
1. RELINQUISHED BY Northern Royaldy Math	hysish	2. REGEI	Idrew Lieta//	1/-	/ m/		for		3. R			IISH	ED/1	ΒΥ ~~/	<u>L</u>								<	IVE	D B	<u> </u>
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DATE TIME 17:0	00	DATE 1.3-	TIN	华::	00						<u></u> H -					TIN	IE L	(,					_	/1		TIME

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COMPANY					ANALYSIS REQUEST														PO# 13017-13						
Geoscience Support Service	S							Γ										84				T			TURNAROUND TIME
ADDRESS PO 220	CITY Claremon	t, CA	ZIP CODE 91711													D2937		HYDRAULIC CONDUCTIVITY, EPABTOO, API RP40, D5084	464M		F.	3			24 HOURS ☐ 5 DAYS ☐ 48 HOURS ☐ NORMAL ☑ 72 HOURS ☐
PROJECT MANAGER Brian Villalobos	bvillalob	os@geoso	cience-water.com			B GE	ЗE	GE				-		Σ		ASTM	1	, API H	7422/4		1	2			OTHER:
PROJECT NAME MPWSP			PHONE NUMBER 109-451-6650		Ш	PACKA	PACKA	PACKA		GE	ЗВАРНУ	4 D2216	0	TM D42	854	P40 or /	Q. .	EFA9100	ASTM.	200	31 W D4318	3			SAMPLE INTEGRITY (CHECK): INTACT X ON ICE
PROJECT NUMBER 13017-13		9	FAX NUMBER 09-451-6638	ES	SOIL PROPERTIES PACKAGE	HYDRAULIC CONDUCTIVITY PACKAGE	PORE FLUID SATURATIONS PACKAGE	TCEQ/TNRCC PROPERTIES PACKAGE	4GE	FLUID PROPERTIES PACKAGE	РНОТОГОВ: СОВЕ РНОТОВВАРНУ	MOISTURE CONTENT, ASTM D2216	POROSITY: TOTAL, API RP40	POROSITY: EFFECTIVE, ASTM D425M	SPECIFIC GRAVITY, ASTM D854	BULK DENSITY (DRY), API RP40 or ASTM D2937	AIR PERMEABILITY, API RP40	١١٨١١٪	GHAIN SIZE DISTRIBUTION, ASTM D4ZZ/4464M	ATTENDED OF IMITS AND MOSE	, AS IVI	à			PTS QUOTE NO.
SITE LOCATION Sandholdt dr area, Moss Lan	ding			SAMPLES	TIES F	COND	SATUR	PROF	PACK	RTIES	SORE	ONTER	OTAL,	FFECT	AVITY,	Y (DR	BILITY,	ONDO	JISTR			2			PTS FILE:
SAMPLER SIGNATURE				P	ROPEF	AULIC C	FLUID (TNRCC	CAPILLARITY PACKAGE	PROPE	OLOG: (URE C	SITY: T	SITY: E	FIC GR	DENSIT	ERMEA	AULIC C	GRAIN SIZE DISTRIBUT		Haria Andrews	700			44073
SAMPLE ID NUMBER	DATE	TIME	DEPTH, FT	NUMBER	SOIL P	нүрв/	PORE	TCEQ/	CAPILI	FLUID	PHOT(MOIST	PORO	PORO	SPECI	BULK	AIR PE	HYDH	GHAIN						COMMENTS
ML-1 76-76.5	10/3/13	10:30	76-76.5	-		χ															Х				
ML-1 107.5-108	10/3/13	13:10	107.5-108			X															X				
ML-1 147-147.5	10/3/13	14:00	147-147.5	1		X															X				
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100																	l			1	T				76°E
1. RELINQUISHED BY		2. RECEL	1/5 1 1/1		D		f	L	3. F	HECIN	NQU) I IISH	ED	BX	1						4.	REC	T CEIVI	ED B	- Anna Carlotte
Nathan Reynolds/ Mith / Andrew Geta/ // COMPANY					<u>-{}/</u>	-7	-		de	MPA		<u>~~</u>	<u> </u>		-1-						C	OMF	PANY		LABS
GEOSCIENCE GEOSCIENCE									DĄŢ	(~ E .	<u>Co</u>	<u>5C</u> !!!	اکار	n4	9	TIMI	2/				D,	ATE		'	TIME
2-3-14 17:0	17:00 17-5-14						1									-	44	1/14	10:26						

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COMPANY					ANALYSIS REQUEST													PO# 13017-13							
Geoscience Support Service	S			H													Т	4	T		T				TURNAROUND TIME
ADDRESS PO 220	CITY Claremon	t, CA	ZIP CODE 91711													D2937	AIR PERMEABILITY, API RP40	P40, D50	464M	-					24 HOURS
PROJECT MANAGER Brian Villalobos	bvillalob	os@geoso	cience-water.com			GE	ЗЕ	ЗЕ		•				Σ		ASTM		, API R	7422/4						OTHER:
PROJECT NAME MPWSP			PHONE NUMBER 109-451-6650			PACKA	PACKA(PACKA(ЗЕ	зВАРНУ	1 D2216		FM D425	854	P40 or /	면	=PA9100	ASTM [D4318	DAMACTIVITY			SAMPLE INTEGRITY (CHECK): INTACT X ON ICE
PROJECT NUMBER 13017-13		9	FAX NUMBER 09-451-6638	ES	SOIL PROPERTIES PACKAGE	HYDRAULIC CONDUCTIVITY PACKAGE	PORE FLUID SATURATIONS PACKAGE	TCEQ/TNRCC PROPERTIES PACKAGE	\GE	FLUID PROPERTIES PACKAGE	РНОТОLOG: СОВЕ РНОТОGRAРНУ	MOISTURE CONTENT, ASTM D2216	POROSITY: TOTAL, API RP40	POROSITY: EFFECTIVE, ASTM D425M	SPECIFIC GRAVITY, ASTM D854	BULK DENSITY (DRY), API RP40 or ASTM D2937	API RP	TIVITY,	GRAIN SIZE DISTRIBUTION, ASTM D422/4464M	<u> </u>	ATTERBERG LIMITS, ASTM D4318	700			PTS QUOTE NO.
SITE LOCATION Del Mar Fisheries, Moss Lan	ding			SAMPLES	ATIES F	CONDU	SATUR	PROP	CAPILLARITY PACKAGE	ERTIES	CORE	ONTEN	OTAL,	FFECT	AAVITY,	TY (DR)	BILITY,	SONDOC	DISTRI	IOC: WALKLEY-BLACK	LIMITS	112			PTS FILE:
SAMPLER SIGNATURE				ER OF	ROPE	AULIC	FLUID	TNRC	LARIT	PROP	JLOG:	URE C	SITY: 1	SITY: E	FIC GF	DENSI	ERME	AULIC (SIZE	WALK	BERG	TUK 1720" FIRE			44073
SAMPLE ID NUMBER	DATE	TIME	DEPTH, FT	NUMBER	SOIL P	HYDR/	PORE	тсеа/	CAPILI	FLUID	РНОТ(MOIST	PORO	PORO	SPECI	BULK	AIR P	HYDR	GRAIN	3	ATTE				COMMENTS
ML-2 87-87.5	12/9/13	1610	87-87.5	State of the last		X																			
ML-2 117.5-118	12/10/13	0935	117.5-118	eponism(T)		X)				
ML-2 157.5-158	12/10/13	1430	157.5-158	l l		X															2				
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COMPANY											ΑN	IAL	YS	IS I	REC	JUE	:S1								FO# 13017-13
Geoscience Support Service	es									T		T					34								TURNAROUND TIME
ADDRESS PO 220	CITY Claremon	t, CA	ZIP CODE 91711				***************************************				٠				75037		HYDRAULIC CONDUCTIVITY, EPA9100, API RP40, D5084	464M			6		į		24 HOURS
PROJECT MANAGER Brian Villalobos	bvillalob	os@geosc	cience-water.com			GE	ЗЕ	ЗE						Σ	MTS		, API R	0422/4			11				OTHER:
PROJECT NAME MPWSP			PHONE NUMBER 109-451-6650			PACKA	ACKA(ACKA		щ	АРНУ	D2216		M D425	154 240 or /		PA9100	ASTM I		4318	(MC:			-	SAMPLE INTEGRITY (CHECK):
PROJECT NUMBER 13017-13		9	FAX NUMBER 09-451-6638	Si	SOIL PROPERTIES PACKAGE	HYDRAULIC CONDUCTIVITY PACKAGE	PORE FLUID SATURATIONS PACKAGE	TCEQ/TNRCC PROPERTIES PACKAGE	CAPILLARITY PACKAGE	PACKAG	PHOTOLOG: CORE PHOTOGRAPHY	MOISTURE CONTENT, ASTM D2216	POROSITY: TOTAL, API RP40	POROSITY: EFFECTIVE, ASTM D425M	SPECIFIC GRAVITY, ASTM D854 RITE DENSITY (DRV) API RP40 or ASTM D9937	AIR PERMEABILITY, API RP40	TIVITY, E	GRAIN SIZE DISTRIBUTION, ASTM D422/4464M	X	ATTERBERG LIMITS, ASTM D4318	Conductivit				PTS QUOTE NO.
SITE LOCATION Moss Landing, Nadar Agha	property			SAMPLES	TIES P	CONDUC	SATUR	PROPE	PACKA	ERTIES	COREP	ONTEN	OTAL, A	FFECTI	(AVITY,)	BILITY.	CONDIC	DISTRIE	TOC: WALKLEY-BLACK	LIMITS	12				PTS FILE:
SAMPLER SIGNATURE				ER OF	ROPEF	AULIC (FLUID	TNRCC	LARITY	PROPE	OLOG:	TURE C	SITY: T	SITY: E	IFIC GF	ERMEA	AULIC C	N SIZE	WALKL	RBERG	Horizonta				44073
SAMPLE ID NUMBER	DATE	TIME	DEPTH, FT	NUMBER	SOILF	HYDR	PORE	тсеа	CAPIL	FLUID	PHOT	MOIS	PORC	PORC	SPEC	AIR P	HYDR	GRAII	TOC:	ATTE	Hor	_			COMMENTS
ML-3 106.5-107	1/7/14	1600	106.5-107	i		X															X				
ML-3 166.5-167	1/8/14	1350	166.5-167	Detroine		X											<u> </u>	L.			X		_		
ML-4 76.5-77	11/26/13	1320	76.5-77	es.indexed*		X												_			X	_			
ML-4 126.5-127	12/2/13	1350	126.5-127			X															X				
ML-4 146.5-147	12/2/13	1745	146.5-147	entirities		X							_								X				
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Geoscience Support Service	es .			H	Ι		Π		Π	Π								84							TURNAROUND TIME
ADDRESS PO 220	CITY Claremon	t, CA	ZIP CODE 91711													D2937		HYDRAULIC CONDUCTIVITY, EPA9100, API RP40, D5084	464M			12	·		24 HOURS
PROJECT MANAGER Brian Villalobos	bvillalob	os@geoso	ience-water.com			GE	ЭE	腸		-				Σ		ASTM		, AP! F	7422/4			<u> </u>			OTHER:
PROJECT NAME MPWSP			PHONE NUMBER 09-451-6650		ш	HYDRAULIC CONDUCTIVITY PACKAGE	PORE FLUID SATURATIONS PACKAGE	TCEQ/TNRCC PROPERTIES PACKAGE		GE	PHOTOLOG: CORE PHOTOGRAPHY	MOISTURE CONTENT, ASTM D2216	0	POROSITY: EFFECTIVE, ASTM D425M)854	BULK DENSITY (DRY), API RP40 or ASTM D2937	40	EPA9100	GRAIN SIZE DISTRIBUTION, ASTM D422/4464M		D4318	brductivity			SAMPLE INTEGRITY (CHECK): INTACT Y ON ICE
PROJECT NUMBER 13017-13		9	FAX NUMBER 09-451-6638	ES	ACKAG	CTIVITY	ATIONS	ERTIES	AGE	PACKA	РНОТО	IT, ASTI	API RP4	IVE, AS	ASTM [Y), API F	API RP	STIVITY,	BUTION	Š	, ASTM	\exists			PTS QUOTE NO.
SITE LOCATION MBARI, Moss Landing				SAMPLES	TIES	OND	SATUR	PROP	PACK	RTIES	ORE	ONTEN	JTAL,	FECT	AVITY,	Y (DR	SILITY,	ONDINC	ISTRI	Y-BLA	LIMITS	1ta			PTS FILE:
SAMPLER SIGNATURE				1 5	SOIL PROPERTIES PACKAGE	AULIC C	FLUID S	TNRCC	CAPILLARITY PACKAGE	FLUID PROPERTIES PACKAGE	JLOG: C	URE CC	POROSITY: TOTAL, API RP40	SITY: EF	SPECIFIC GRAVITY, ASTM D854	DENSIT	AIR PERMEABILITY, API RP40	AULIC CO	N SIZE D	TOC: WALKLEY-BLACK	ATTERBERG LIMITS, ASTM D4318	Hovizontal			44073
SAMPLE ID NUMBER	DATE	TIME	DEPTH, FT	NUMBER (SOIL P	нүрв.	PORE	TCEQ/	CAPILI	FLUID	РНОТС	MOIST	PORO	PORO	SPECI	BULK	AIR PE	HYDR/	GRAIN	TOC:	ATTE	101			COMMENTS
ML-6 79.5-80	11/19/13	1310	79.5-80	Ĭ		X																X			1 28
ML-6 107.5-108	11/19/13	1320	107.5-108	· Internation		X																X			
ML-6 167-168.5	11/20/13	0935	167-168.5	**demont		X																X			
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ADDRESS PO 220 PROJECT MANAGER Brian Villalobos		nont, CA	ZIP CODE 91711	MANAGED PROPERTY OF THE PROPER		Ш					i			f		TM D2937		HYDRAULIC CONDUCTIVITY, EPA9100, API RP40, D5084	22/4464M			17.17	<u> </u>			24 HO 48 H O 72 HO	URS URS URS	ND TIM		'S □ MAL □
PROJECT NAME MPWSP PROJECT NUMBER			PHONE NUMBER 1-6650	- Armonios de la Company de la	Ę	/ PACKAG	PACKAGI	PACKAGI		GE	зварну	/ D2216	0	TM D425M	854	P40 or AS	Ot	EPA9100, A	ASTM D4		D4318	Conductivi			F		LE INT		Y (CH	
13017-13 SITE LOCATION		909-4	FAX NUMBER 51-6638	LES	PACKAG	JCTIVITY	RATIONS	PERTIES	AGE	PACKA	РНОТО(JT, ASTA	API RP4	IVE, AS	ASTM D	Y), API F	API RP	TIVITY, E	3UTION,	Š	, ASTM	Cal				PTS Q)N ICE	
Potrero Rd Parking A	rea, Mos	ss Landir	าg	R OF SAMPLES	SOIL PROPERTIES PACKAGE	HYDRAULIC CONDUCTIVITY PACKAGE	PORE FLUID SATURATIONS PACKAGE	TCEQ/TNRCC PROPERTIES PACKAGE	CAPILLARITY PACKAGE	FLUID PROPERTIES PACKAGE	РНОТОLOG: СОЯЕ РНОТОGRAPHY	MOISTURE CONTENT, ASTM D2216	POROSITY: TOTAL, API RP40	POROSITY: EFFECTIVE, ASTM D425M	SPECIFIC GRAVITY, ASTM D854	BULK DENSITY (DRY), API RP40 or ASTM D2937	AIR PERMEABILITY, API RP40	JLIC CONDUC	GRAIN SIZE DISTRIBUTION, ASTM D422/4464M	TOC: WALKLEY-BLACK	ATTERBERG LIMITS, ASTM D4318	Horizontal	en e	-		PTS F	ILE: 4	136:	26	
SAMPLE ID NUMBER	DATE	TIME	DEPTH, FT	NUMBER	SOIL PI	HYDRA	PORE F	TCEQ/I	CAPILL	FLUID F	РНОТО	MOIST	POROS	POROS	SPECIF	BULK D	AIR PEI	HYDRAI	GRAIN	TOC: W	ATTERE	Hari					CO	ММЕ	NTS	
PR-1 67 ft - 67.5 ft	9/21/13	1500	67 - 67.5	1	1 4	X																A)				
PR-1 145.5 ft -146 ft	9/22/13	1400	145.5 - 146)		X																X				5) (a)	74	of F
PR-1 152 ft - 152.5 ft	9/2/13	1420	152 -152.5	1		χ																X							<u></u>	
PR-1 200.5 ft - 201 ft	9/22/13	1730	200.5 -201	1		Χ															ŀ	X	T		T	ナ		******		
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Project Number: 13017-13 Client: Geoscience Support Services

TEST PROGRAM - 20140206

		Core	Hydraulic	Hydraulic	
CORE ID	Depth	Recovery	Conductivity	Conductivity	
	ft.	ft.	Pkg.	API RP40/EPA 9100	Notes
		Plugs:	Vert. 1"	Horz. 1"	
Date Received: 20140204		0.50			
CX-B1 66.5-67	66.5-67 166.5-	0.50	X	X	
CX-B1 166.5-167.0	167.0	0.50	X	X	
CX-B1 257.5-258	257.5-258	0.50	X		
CX-B2 207.5-208	207.5-208	0.50	X	X	
CX-B2 259-259.5	259-259.5	0.50	X		
CX-B3 107.5-108	107.5-108	0.50	X	X	
CX-B3 129-129.5	129-129.5	0.50	X		
CX-B3 177.5-178	177.5-178	0.50			
CX-B3 197.5-198	197.5-198	0.50	X	X	
ML-1 76-76.5	76-76.5	0.50	X		
ML-1 107.5-108	107.5-108	0.50	X	X	
ML-1 147-147.5	147-147.5	0.50	X		
ML-2 87-87.5	87-87.5	0.50	X		
ML-2 117.5-118	117.5-118	0.50	X	X	
ML-2 157.5-158	157.5-158	0.50	X	X	
ML-3 106.5-107	106.5-107	0.50	X	X	
ML-3 166.5-167	166.5-167	0.50	X	X	
ML-4 76.5-77	76.5-77	0.50	X	X	
ML-4 126.5-127	126.5-127	0.50	X		
ML-4 146.5-147	146.5-147	0.50	X	X	
ML-6 79.5-80	79.5-80	0.50	X		
ML-6 107.5-108	107.5-108	0.50	X	X	
ML-6 167-168.5	167-168.5	0.50	X	Х	
TOTALS:	23 cores	11.50	22	14	23

Project Number: 13017-13 Client: Geoscience Support Services

TEST PROGRAM - 20140206

		Core	Hydraulic	Hydraulic	
CORE ID	Depth	Recovery	Conductivity	Conductivity	
	ft.	ft.	Pkg.	API RP40/EPA 9100	Notes
		Plugs:	Vert. 1"	Horz. 1"	

Laboratory Test Program Notes

Contaminant identification: NONE

Standard TAT for basic analysis is 10 business days.

Hydraulic Conductivity Package – Saturated Zone: Native-state permeability to water, total and air-filled porosity, grain and bulk density, moisture content, total pore fluid (water only) saturation.

PTS File No: 44073

Client: Geoscience Support Services

Report Date: 03/13/14

PHYSICAL PROPERTIES DATA - HYDRAULIC CONDUCTIVITY PACKAGE Rev.01

Project Name: MPWSP Project No: 13017-13

> API RP 40 / METHODS: ASTM D2216

		METHODS:	ASTM D2216	API R	P 40	AP	I RP 40	API RP 40	API RP 40; EF	A 9100
									25 PSI CONFINING	G STRESS
		SAMPLE	MOISTURE	DENS		POROS	ITY, %Vb (2)	TOTAL PORE FLUID	EFFECTIVE (4,5)	HYDRAULIC
SAMPLE ID.	DEPTH, ft.	ORIENTATION (1)	CONTENT, % weight	DRY BULK, g/cc	GRAIN, g/cc	TOTAL	AIR-FILLED	SATURATIONS (3), % Pv	PERMEABILITY TO WATER, millidarcy	CONDUCTIVITY (4,5), cm/s
ID.	II.	(1)	% weight	g/cc	g/cc			70 FV	milidaicy	CITI/S
CX-B1 66.5-67	66.6	V	22.9	1.46	2.66	45.0	11.6	74.2	273	2.76E-04
CX-B1 166.5-167.0	166.6	V	24.7	1.58	2.82	43.8	4.7	89.3	484	4.87E-04
CX-B1 257.5-258	257.5-258	V	41.1	1.11	2.61	57.7	12.2	78.8	1.75	1.75E-06
CX-B2 207.5-208	207.6	V	21.5	1.48	2.67	44.6	12.9	71.1	3820	3.76E-03
CX-B2 259-259.5	259.1	V	31.0	1.33	2.63	49.3	7.9	83.9	1.83	1.85E-06
CX-B3 107.5-108	107.6	V	20.6	1.43	2.64	45.8	16.4	64.2	5210	5.26E-03
CX-B3 129-129.5	129.1	V	35.5	1.25	2.62	52.1	7.6	85.5	2.83	2.86E-06
CX-B3 197.5-198	197.6	V	18.1	1.66	2.69	38.2	8.1	78.8	101	1.00E-04
ML-1 76-76.5	76.1	V	42.4	1.17	2.67	56.1	6.3	88.7	4.89	4.83E-06
ML-1 107.5-108	107.6	V	15.0	1.53	2.65	42.1	19.0	54.8	8540	8.52E-03
ML-1 147-147.5	147.1	V	32.4	1.31	2.66	50.8	8.4	83.4	1.97	1.98E-06
ML-2 87-87.5	87.1	V	20.5	1.50	2.66	43.4	12.7	70.8	101	1.00E-04
ML-2 117.5-118	117.6	V	24.3	1.43	2.64	45.8	11.0	76.0	47.3	4.70E-05
ML-2 157.5-158	157.6	V	19.2	1.52	2.61	41.6	12.3	70.5	110	1.10E-04
ML-3 106.5-107	106.6	V	12.9	1.53	2.64	42.0	22.3	47.0	1900	1.87E-03
ML-3 166.5-167	166.6	V	28.6	1.31	2.65	50.7	13.2	73.9	9.6	9.51E-06
ML-4 76.5-77	76.6	V	21.4	1.41	2.62	46.3	16.2	65.1	954	9.49E-04
ML-4 126.5-127	126.6	V	25.0	1.44	2.64	45.5	9.5	79.1	1.18	1.18E-06
ML-4 146.5-147	146.6	V	14.1	1.45	2.61	44.3	23.8	46.3	6180	6.10E-03
ML-6 79.5-80	79.6	V	32.2	1.33	2.64	49.7	6.9	86.0	2.43	2.43E-06
ML-6 107.5-108	107.6	V	15.0	1.41	2.64	46.3	25.2	45.6	4710	4.65E-03
ML-6 167-168.5	167.6	V	25.6	1.38	2.62	47.4	12.1	74.3	72.6	7.23E-05

⁽¹⁾ Sample Orientation: H = horizontal; V = vertical; R = remold

Water = filtered Laboratory Fresh (tap) or Site water.

⁽²⁾ Total Porosity = all interconnected pore channels; Air Filled = pore channels not occupied by pore fluids.

⁽³⁾ Fluid density used to calculate pore fluid saturations: Water = 0.9996 g/cc.

⁽⁴⁾ Effective (Native) = With as-received pore fluids in place.

⁽⁵⁾ Permeability to water and hydraulic conductivity measured at saturated conditions.

Vb = Bulk Volume, cc; Pv = Pore Volume, cc; ND = Not Detected

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COMPANY	•	· · · · · · · · · · · · · · · · · · ·		Ī							Α!	۱A۱	LYS	SIS	RE	Ql	JE:	ST								PO# 13017-13
Geoscience Support Service				┢														084						T		TURNAROUND TIME
ADDRESS PO 220	CITY Claremon	it, CA	ZIP CODE 91711												1	72937		P40, D50	464M							24 HOURS 5 DAYS 48 HOURS NORMAL
PROJECT MANAGER Brian Villalobos	bvillalob	os@geos	cience-water.com			GE	ЗЕ	3E						Σ		ASTM (, API R	3422/4			1177				72 HOURS □ OTHER:
PROJECT NAME MPWSP			PHONE NUMBER 909-451-6650			PACKA	PACKA(PACKA		먎	RAPHY	D2216		M D425	854	P40 or A	0	:PA9100	ASTM [04318	Sondarchurth			ŀ	SAMPLE INTEGRITY (CHECK):
PROJECT NUMBER 13017-13		g	FAX NUMBER 109-451-6638	ES	PACKAGE	HYDRAULIC CONDUCTIVITY PACKAGE	PORE FLUID SATURATIONS PACKAGE	TCEQ/TNRCC PROPERTIES PACKAGE	GE	FLUID PROPERTIES PACKAGE	PHOTOLOG: CORE PHOTOGRAPHY	T, ASTM	POROSITY: TOTAL, API RP40	POROSITY: EFFECTIVE, ASTM D425M	SPECIFIC GRAVITY, ASTM D854	BULK DENSITY (DRY), API RP40 or ASTM D2937	AIR PERMEABILITY, API RP40	HYDRAULIC CONDUCTIVITY, EPA9100, API RP40, D5084	GRAIN SIZE DISTRIBUTION, ASTM D422/4464M	X	ATTERBERG LIMITS, ASTM D4318	(Joyd			ŀ	NTACT ON ICE PTS QUOTE NO.
SITE LOCATION CEMEX				SAMPLES		NONO	ATUR/	PROPI	PACKA	ATIES	OREF	NTEN	TAL, A	FECTI	VITΥ,	r (DR)	ILITY,	NDOC	ISTRIE	Y-BLA(IMITS.	Y				PTS FILE:
SAMPLER SIGNATURE		- A-8 HV-1		R	世	ULIC C	FLUID S	INRCC	CAPILLARITY PACKAGE	PROPEI	LOG: C	URE CC	SITY: TC	SITY: EF	FIC GRA	DENSIT	RMEAB	יחרוכ ככ	SIZE D	TOC: WALKLEY-BLACK	BERG L	Harizonta				44073
SAMPLE ID NUMBER	DATE	TIME	DEPTH, FT	NUMBER (SOIL P	HYDRA	PORE	TCEQ/	CAPILL	FLUID	PHOTC	MOIST	POROS	POROS	SPECII	BULK	AIR PE	нурва	GRAIN	TOC: V	ATTER	Har				COMMENTS
CX-B1 66.5-67	10/22/13	1500	66.5-67	į		X																χ				
CX-B1 166.5-167.0	10/23/13	1500	166.5-167	13.00 K		X																X				
CX-B1 257.5-258	10/25/13	1500	257.5-258	(Allega)		X																X				2 inches of sample missing
CX-B2 207.5-208	11/5/13	1345	207.5-208	-contractor		χ																X				
CX-B2 259-259.5	11/6/13	1000	259-259.5	ı		X																X				
CX-B3 107.5-108	11/10/13	1500	107.5-108	¹ S (Statements		X																X				
CX-B3 129-129.5	11/10/13	1500	129-129.5	"Unce.		χ																χ				
CX-B3 177.5-178	11/10/13	1500	177.5-178			X																Χ				
CX-B3 197.5-198	11/10/13	1500	197.5-198	No.		X																X				the relative
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					<u>L</u>							/														76°F
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COMPANY) COMPANY / COMPANY					/				CON	> C	051	27	n C	l								COI F	ΜΡΑΙ) Τ S	NY L	A	35
DATE 71ME 77:6	ESCIENCE (SEOSCIPALE) TIME 17:00 23-14				00			- 20	DAT	E	<u></u> 니 -	-] [1			TIN	IE - Z	()				DAT 2	E, /4	11	4	75 TIME 10:26

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COMPANY		ANALYSIS REQUEST															PO# 13017-13								
Geoscience Support Service	S			┢														84			\prod	Ť			TURNAROUND TIME
ADDRESS PO 220	CITY Claremon	t, CA	ZIP CODE 91711													D2937	AIR PERMEABILITY, API RP40	P40, D50	464M		+	2			24 HOURS ☐ 5 DAYS ☐ 48 HOURS ☐ NORMAL ☑ 72 HOURS ☐
PROJECT MANAGER Brian Villalobos	bvillalob	os@geoso	cience-water.com			B GE	ЗE	GE				-		Σ		ASTM	1	, API H	0422/4		13	3			OTHER:
PROJECT NAME MPWSP			PHONE NUMBER 909-451-6650		Ш	PACKA	PACKA	PACKA		GE	зварну	A D2216	0	TM D42	854	3P40 or /	40	EFA9100	, ASTM		04318	01/200/101/14			SAMPLE INTEGRITY (CHECK): INTACT X ON ICE
PROJECT NUMBER 13017-13		9	FAX NUMBER 09-451-6638	SAMPLES	SOIL PROPERTIES PACKAGE	HYDRAULIC CONDUCTIVITY PACKAGE	PORE FLUID SATURATIONS PACKAGE	TCEQ/TNRCC PROPERTIES PACKAGE	AGE	FLUID PROPERTIES PACKAGE	РНОТОLOG: СОВЕ РНОТОGRAPHY	MOISTURE CONTENT, ASTM D2216	POROSITY: TOTAL, API RP40	POROSITY: EFFECTIVE, ASTM D425M	SPECIFIC GRAVITY, ASTM D854	BULK DENSITY (DRY), API RP40 or ASTM D2937	AIR PERMEABILITY, API RP40	١١٨١١٪,	GRAIN SIZE DISTRIBUTION, ASTM D422/4464M	2	HEIGHT AND ASTRANDESTR	à			PTS QUOTE NO.
SITE LOCATION Sandholdt dr area, Moss Landing						COND	SATUR	PROF	PACK	RTIES	SORE	ONTE	OTAL,	FFECT	AVITY,	7 (DR		OND	SISTRI	10-11		17			PTS FILE:
SAMPLER SIGNATURE				A	ROPEF	AULIC (FLUID	TNRCC	CAPILLARITY PACKAGE	PROPE	JLOG: (URE C	SITY: T	SITY: E	FIC GR	DENSI	FRMEA	O CO	GRAIN SIZE DISTRIBUT	NALAL NALAL	ALLEHBERG LIMIT	100			44073
SAMPLE ID NUMBER	DATE	TIME	DEPTH, FT	NUMBER	SOIL P	нүрн,	PORE	TCEQ/	CAPILI	FLUID	PHOT	MOIST	PORO	PORO	SPECI	BULK	AIR PE	HYDH	GRAIN		Al ler				COMMENTS
ML-1 76-76.5	10/3/13	10:30	76-76.5	•		χ															λ				
ML-1 107.5-108	10/3/13	13:10	107.5-108	George		X															X				
ML-1 147-147.5	10/3/13	14:00	147-147.5	1		X)				
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N. Hran Reynlds/ Meth / Hndrew Kieta/ //					4/	-7			o@i	MPA	NY		<u> </u>	<u>_</u>	7-	-					C	ОМЕ	PANY		
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COMPANY		ANALYSIS REQUEST															PO# 13017-13								
Geoscience Support Service	s			H													Т	84	T		T		T		TURNAROUND TIME
ADDRESS PO 220	CITY Claremon	t, CA	ZIP CODE 91711													D2937	AIR PERMEABILITY, API RP40	P40, D50	464M						24 HOURS
PROJECT MANAGER Brian Villalobos	bvillalob	os@geoso	cience-water.com			GE	ЗЕ	ЗЕ		•				Σ		ASTM		, API R)422/4		-				OTHER:
PROJECT NAME MPWSP	*****		PHONE NUMBER 909-451-6650		Ш	PACKA	PACKA(PACKA(ЗЕ	зВАРНУ	1 D2216		FM D425	854	P40 or /	요	EPA9100	ASTM [D4318	LANGER LITTE			SAMPLE INTEGRITY (CHECK): INTACT X ON ICE
PROJECT NUMBER 13017-13		9	FAX NUMBER 09-451-6638	ES	SOIL PROPERTIES PACKAGE	HYDRAULIC CONDUCTIVITY PACKAGE	PORE FLUID SATURATIONS PACKAGE	TCEQ/TNRCC PROPERTIES PACKAGE	\GE	FLUID PROPERTIES PACKAGE	РНОТОLOG: СОВЕ РНОТОGRAРНУ	MOISTURE CONTENT, ASTM D2216	POROSITY: TOTAL, API RP40	POROSITY: EFFECTIVE, ASTM D425M	SPECIFIC GRAVITY, ASTM D854	BULK DENSITY (DRY), API RP40 or ASTM D2937	API RP	TIVITY, I	GRAIN SIZE DISTRIBUTION, ASTM D422/4464M	<u></u>	ATTERBERG LIMITS, ASTM D4318	700			PTS QUOTE NO.
SITE LOCATION Del Mar Fisheries, Moss Lan	ding		40 Maria	SAMPLES	ATIES F	CONDU	SATUR	PROP	CAPILLARITY PACKAGE	ERTIES	CORE	ONTEN	OTAL,	FFECT	AAVITY,	TY (DR)	BILITY,		DISTRI	IOC: WALKLEY-BLACK	LIMITS	प्रका			PTS FILE:
SAMPLER SIGNATURE				ER OF	ROPE	AULIC (FLUID	TNRC	LARITY	PROP	olog:	URE C	SITY: 1	SITY: E	FIC GF	DENSI	ERMEA	AULIC (SIZE	WALK	ABERG	10/1/20/11A			44073
SAMPLE ID NUMBER	DATE	TIME	DEPTH, FT	NUMBER	SOILF	HYDR,	PORE	тсеа/	CAPIL	FLUID	PHOT(MOIST	PORO	PORO	SPEC	BULK	AIR PI	HYDR	GRAIN	500	ATTE) a. L			COMMENTS
ML-2 87-87.5	12/9/13	1610	87-87.5	4 Sanay		X															Ì				33
ML-2 117.5-118	12/10/13	0935	117.5-118	et-minute.		Χ̈́															2	Ý.			214 - 1825 13 - 1811 - 1
ML-2 157.5-158	12/10/13	1430	157.5-158	Table 1		X															į	4			
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DATE TIME DATE TI 2-3-14 17:00 7-3-14									DÀT	<u>-</u>	4.	- l'	4		l	Ď-	E	>					2/14	1/1	4 10:26

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PAGE	Appendix QF
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Food Park N/		Т		_							`												PO# 13017-13		
COMPANY				ANALYSIS REQUEST															FO# 13017-13						
Geoscience Support Service	S				П													42							TURNAROUND TIME
ADDRESS PO 220	CITY Claremon	t, CA	ZIP CODE 91711				***************************************									D2937		HYDHAULIC CONDUCTIVITY, EPABLOO, API RP40, D5084	464M			2			24 HOURS
PROJECT MANAGER Brian Villalobos	bvillalob	os@geosc	ience-water.com			GE	GE	GE						M		ASTM	1	API K	D422/4		1.36.0				OTHER:
PROJECT NAME MPWSP	•		PHONE NUMBER 09-451-6650			PACKA	ACKA	ACKA		ΪΕ	ВАРНУ	D2216	•	M D42	354	P40 or,	0	PABLOC	ASIM	9157	1, 6,	3			SAMPLE INTEGRITY (CHECK):
PROJECT NUMBER 13017-13		9	FAX NUMBER 09-451-6638	ES	SOIL PROPERTIES PACKAGE	HYDRAULIC CONDUCTIVITY PACKAGE	PORE FLUID SATURATIONS PACKAGE	TCEQ/TNRCC PROPERTIES PACKAGE	CAPILLARITY PACKAGE	PACKAG	РНОТОСОВ: СОВЕ РНОТОВВАРНУ	MOISTURE CONTENT, ASTM D2216	POROSITY: TOTAL, API RP40	POROSITY: EFFECTIVE, ASTM D425M	SPECIFIC GRAVITY, ASTM D854	BULK DENSITY (DRY), API RP40 or ASTM D2937	AIR PERMEABILITY, API RP40		GHAIN SIZE DISTRIBUTION, ASTM D4224464M	ATTEBBEBG LIMITS ASTM DA318		CONGINETIVIT			INTACT Y ON ICE PTS QUOTE NO.
SITE LOCATION Moss Landing, Nadar Agha p	oroperty			SAMPLES	TIES P	CONDUC	SATUR	PROPE	PACKA	ERTIES	CORE P	ONTEN.	OTAL, A	FFECTI	(AVITY,	TY (DRY	BILITY,	CNDOC	GRAIN SIZE DISTRIBUT	K MI		3			PTS FILE:
SAMPLER SIGNATURE				ER OF	ROPEF	AULIC (FLUID	TNRCC	LARITY	PROPE	OLOG:	TURE C	SITY: T	SITY: E	IFIC GF	DENSI	ERMEA	AULIC C	N SIZE	איזייי	2 2	101100114			44073
SAMPLE ID NUMBER	DATE	TIME	DEPTH, FT	NUMBER	SOILF	HYDR	PORE	TCEQ,	CAPIL	FLUID	PHOT	MOIS	PORC	PORC	SPEC	BULK	AIRP	HYDH	GHA GHA		7 7	0			COMMENTS
ML-3 106.5-107	1/7/14	1600	106.5-107	è		X												_			γ	1		1	
ML-3 166.5-167	1/8/14	1350	166.5-167	custrage		X														_	Х	1	_		
ML-4 76.5-77	11/26/13	1320	76.5-77	ł		X														_	X				
ML-4 126.5-127	12/2/13	1350	126.5-127			X												_			X				
ML-4 146.5-147	12/2/13	1745	146.5-147	cutetto		X															17	4			
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GEOSCIENTE GOOSCIENCE DATE TIME DATE 7 2 - 3 - 14 17:00 7 - 3 - 14									DAT	TE 2-	4-	- j4	(<u>-~</u>		TIMIT }	E) = 2	26			D	ATE		,	TIME

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COMPANY											1A	۱A۱	_YS	SIS	RE	QL	JES	ST							PO# 13017-13
Geoscience Support Service	s			H	I					Π								84						T	TURNAROUND TIME
ADDRESS PO 220	CITY Claremon	t, CA	ZIP CODE 91711													D2937		HYDRAULIC CONDUCTIVITY, EPA9100, API RP40, D5084	464M			127			24 HOURS 5 DAYS 148 HOURS NORMAL 72 HOURS 1
PROJECT MANAGER Brian Villalobos	bvillalob	os@geoso	ience-water.com			GE	3E	E E						Σ		ASTM		, API F	7422/4			<u> </u>			OTHER:
PROJECT NAME MPWSP			PHONE NUMBER 09-451-6650		ш	HYDRAULIC CONDUCTIVITY PACKAGE	PORE FLUID SATURATIONS PACKAGE	TCEQ/TNRCC PROPERTIES PACKAGE		GE	PHOTOLOG: CORE PHOTOGRAPHY	MOISTURE CONTENT, ASTM D2216	0	POROSITY: EFFECTIVE, ASTM D425M)854	BULK DENSITY (DRY), API RP40 or ASTM D2937	40	EPA9100	GRAIN SIZE DISTRIBUTION, ASTM D422/4464M		D4318	brductivity			SAMPLE INTEGRITY (CHECK): INTACT Y ON ICE
PROJECT NUMBER 13017-13		9	FAX NUMBER 09-451-6638	ES	ACKAG	CTIVIT	ATIONS	ERTIES	GE	PACKA	ното	T, AST	PI RP4	VE, AS	ASTM [), API	API RP	TIVITY,	SUTION	쏤	, ASTM	\exists			PTS QUOTE NO.
SITE LOCATION MBARI, Moss Landing				SAMPLES	SOIL PROPERTIES PACKAGE	CONDU	SATUR/	PROPI	CAPILLARITY PACKAGE	FLUID PROPERTIES PACKAGE	CORE F	ONTEN	POROSITY: TOTAL, API RP40	FFECTI	SPECIFIC GRAVITY, ASTM D854	Y (DR)	AIR PERMEABILITY, API RP40	ONDOC	SISTRIE	TOC: WALKLEY-BLACK	ATTERBERG LIMITS, ASTM D4318	Hovizontal			PTS FILE:
SAMPLER SIGNATURE				1 5	ROPEF	VULIC C	FLUID	TNRCC	ARITY	PROPE	JLOG: (URE C	SITY: T	SITY: E	FIC GR	DENSI	RMEA	AULIC C	I SIZE I	WALKL	REERG	120			44073
SAMPLE ID NUMBER	DATE	TIME	DEPTH, FT	NUMBER (SOIL P	HYDR/	PORE	TCEQ/	CAPIL	FLUID	РНОТ	NOIST	PORO	PORO	SPECI	BULK	AIR P	HYDR/	GRAIN	T0C:	ATTE	101			COMMENTS
ML-6 79.5-80	11/19/13	1310	79.5-80	ij		X																X			1 48
ML-6 107.5-108	11/19/13	1320	107.5-108	· Editorial Com-		X																X			
ML-6 167-168.5	11/20/13	0935	167-168.5	**00100*		X																X			
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